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Modelling coherent emission in transverse coupled cavity VCSELs

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Abstract—Transverse coupled cavity (TCC)-VCSELs are promising candidates for the next generation of high-speed direct modulation devices. We present a comprehensive framework for their investigation based on the dynamical solution of the scalar wave equation and compare it with recent experimental results.

Index Terms—Transverse coupled cavity, VCSELs, coherent emission

I. INTRODUCTION

TCC VCSELs [1] are promising candidates for a number of different applications, such as direct modulation [2], beam steering and terahertz generation [3]. The potential of these devices lies on the presence of two nearly frequency-degenerate (super)-modes [4], which however implies a critical thermal management and impact of technological variations. In this work we present a model based on the dynamical solution of the scalar wave equation. The model naturally handles particular dynamical states for which two modes are coherently phase-locked [2]. Such effects can be observed by adding cross-coupling terms to the standard rate equation model, which are derived from the scalar wave equation [4] and arise from the variations of the refractive index due to gain, self-heating or unwanted variations on the nominal structure.

We consider the structure manufactured in [5], consisting in a standard 850 nm VCSEL with *bow-tie* oxide aperture, comprising two circular cavities of radius $R_{R,L}$, connected by a rectangular region denoted as *bridge*. It is reasonable to assume that, due to the oxidation process, one of the two apertures is slightly bigger than the other ($R_R < R_L$ in this case). We assume that the two cavities are electrically isolated, as done in [6], and that we can pump them separately with currents $I_{R,L}$, respectively. Fig.1 shows a sketch of the oxide aperture together with a cut of the first two optical modes, computed with our in-house VCSEL modal solver. The two modes are nearly degenerate in frequency and threshold gain.

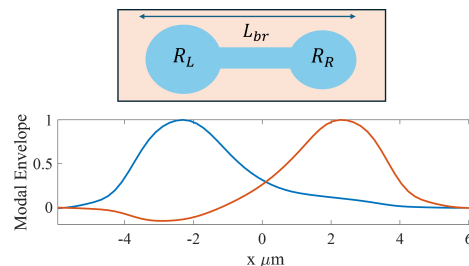


Fig. 1. Sketch of the oxide aperture under investigation together with the first two optical modes. $L_{br} = 4\mu\text{m}$ in this work.

II. THEORY AND RESULTS

By representing the electric field in the quantum well as a sum of the optical modes (*cold-cavity modes*), we obtain a set of dynamical equations for the i -th modal amplitude E_i , reading:

$$\partial_t E_i = (i\omega_i - L_i)E_i + \sum_j k_{ij}E_j, \quad (1)$$

where L_i and ω_i are the i -th modal losses and frequency offset with respect to an arbitrary reference ω_0 , and k_{ij} is given by the following integral on the active region (AR):

$$k_{ij}(t) = \frac{v_g \Gamma_z}{2} \iint_{\text{AR}} \Psi_i^* \Psi_j g(x, y) dx dy, \quad (2)$$

where v_g is the group velocity, Γ_z is the optical confinement factor and $g(x, y)$ is a generalized definition of gain accounting for thermal effects, defined by:

$$g = \underbrace{(1 + i\alpha_h)[G_d(N(x, y) - n_{tr})]}_{\text{carriers}} - i \underbrace{\frac{\Gamma_{th}}{\Gamma_z} \frac{4\pi}{\lambda_0} \frac{dn}{dT} \Delta T(x, y)}_{\text{temperature}} \quad (3)$$

where n_{tr} is the transparency carrier density, G_d is the differential gain, α_h is the linewidth enhancement factor, $\frac{dn}{dT}$ is a

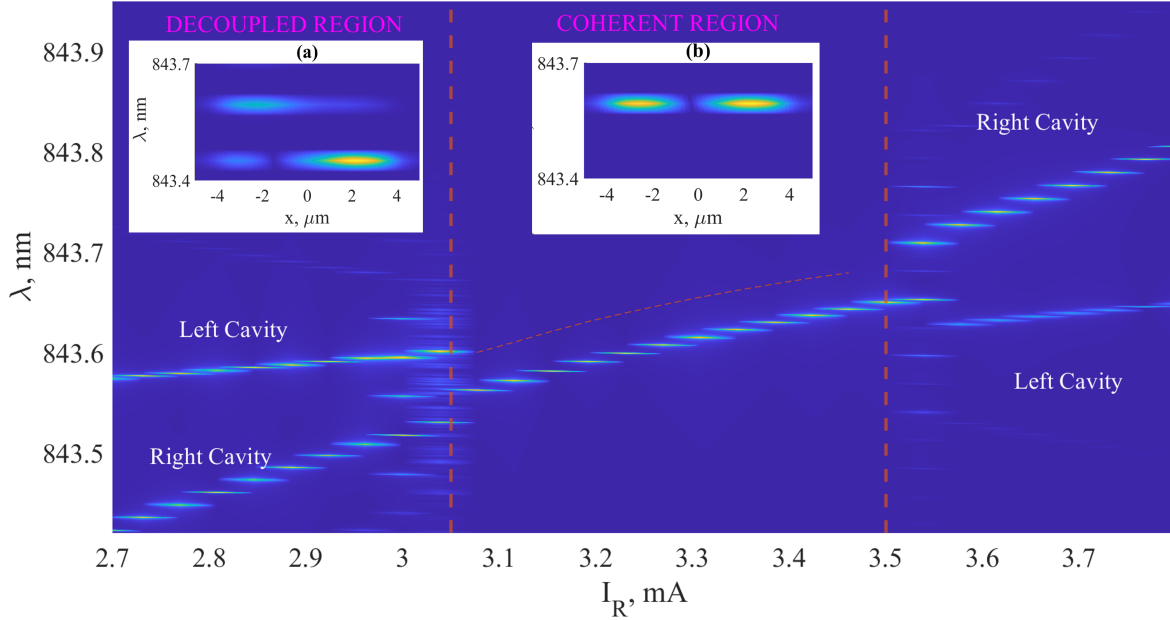


Fig. 2. Simulated optical spectrum for varying I_r for fixed $I_l = 3mA$. The vertical lines denote the boundaries of the coherent region. Insets: wavelength resolved near field for (a) 2.8 mA and (b) 3.2 mA. The dashed line is the emission wavelength of the below-threshold supermode in the coherent range, computed by finding the eigenvalues of the matrix k_{ij} .

phenomenological coefficient describing the variation of the refractive index with respect to the temperature, λ_0 is the reference wavelength associated to ω_0 , Γ_{th} is a phenomenological coefficient to describe the overlap of the standing wave with the longitudinal temperature profile, set to 1 in this work, ΔT is the self-heating temperature variation profile. In this work, we assume ΔT as a superposition of two *gaussians* centered in the two apertures, whose peak values are proportional to the currents $I_{R,L}$, with a coefficient of $7.5 \frac{K}{mA}$. Other material parameters can be found in [4]. The model is closed with the self-consistent solution of the carrier diffusion equation by means of a finite-element discretization, as carried out in [2].

We solve the dynamical equations fixing I_L and varying I_R , using the first four modes as basis. Fig. 2 shows the resulting optical spectra. At low I_R , each cavity emits at a distinct wavelength, with a large frequency separation due to the temperature difference between the apertures. As I_R increases and approaches I_L , a coherent regime emerges where both cavities emit at the same frequency, which tends toward the lower-wavelength mode. The plot is asymmetric with respect to $I_R = I_L$, reflecting the structural asymmetry of the device. In particular, the coupling occurs when the smaller cavity is hotter. The two insets display the wavelength-resolved near-field, highlighting the considerations made so far. Given a certain gain and temperature profile, we can interpret as *pumped-cavity* modes the combination of *cold-cavity* modes that diagonalize the matrix k_{ij} , where the imaginary part of the correspondent eigenvalues represents the emission frequency. In this way, we can highlight the presence of a below-threshold

supermode in the coherent range, which is responsible for photon-photon-resonance [4], denoted with the dashed line.

The simulated behaviour aligns well with recent experimental results [7] [6]. Evidence of coherent emission has been also recently observed in [2], showing theoretically and experimentally an enhancement of the bandwidth modulation.

III. ACKNOWLEDGEMENT

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