

Solving Nonlinear MPC Problems in the Koopman Lifted Space: The Case Study of Mobile Robot Navigation in Cluttered Environments

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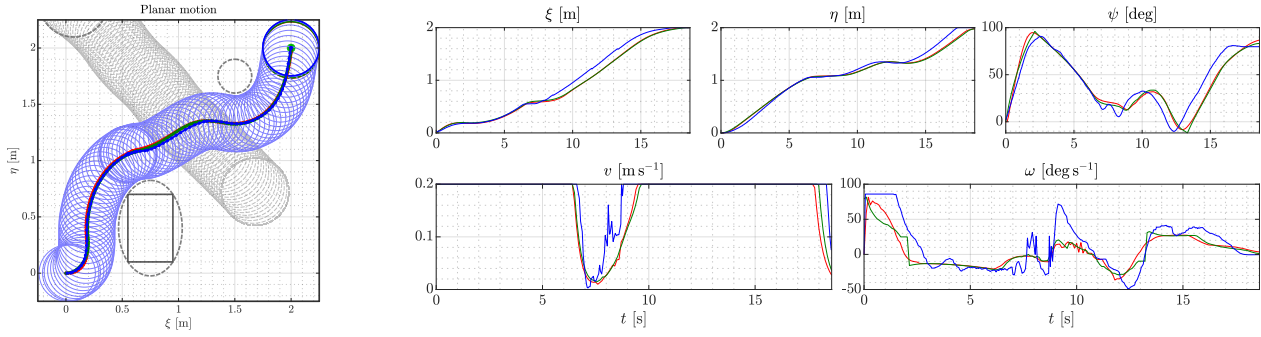


Fig. 2. Planar motion and closed-loop trajectories of the ego robot within the cluttered environment: NMPC — green —; K-NMPC (simulation) — red —; K-NMPC (real) — blue —.

III. KOOPMAN NMPC: LIFTING NONLINEAR MPC INTO THE LINEAR KOOPMAN SPACE

In the following, we extend the Koopman operator framework to optimization problems. Specifically, we transform a generic NMPC problem in the state x – comprising nonlinear prediction model and nonlinear state constraints – into an equivalent quadratic program (QP) in the lifted state z (K-NMPC) [1].

The NMPC problem is formulated as follows, for each $k \geq 0$:

$$\min_{\hat{x}, \hat{u}} J(\hat{x}, \hat{u}) \quad (8a)$$

$$\text{s.t. } \hat{x}_0 = x_k, \quad \hat{x}_{i+1} = f^d(\hat{x}_i, \hat{u}_i), \quad (8b)$$

$$\hat{u}_i \in \mathcal{U}, \quad \hat{x}_i \in \mathcal{X}, \quad h_i^d(\hat{x}_i, c_k, \nu_k) \leq 0, \quad (8c)$$

$$i = 0, \dots, N_p - 1,$$

$$J(\hat{x}, \hat{u}) = \sum_{i=0}^{N_p-1} \|\hat{x}_i - x_{r,k+i}\|_Q^2 + \|\hat{u}_i\|_R^2 + \sum_{i=1}^{N_p-1} \|\hat{x}_i - \hat{x}_{i-1}\|_{Q_\Delta}^2 + \|\hat{u}_i - \hat{u}_{i-1}\|_{R_\Delta}^2. \quad (8d)$$

In the following, we shall focus on the practical case study of mobile robot navigation in cluttered environments (Fig. 1).

A. Nonlinear Prediction Model: Mobile Robot

As prediction model of plant (1) (i.e., the ego mobile robot), we employ the kinematic unicycle model, i.e.,

$$\dot{x}(t) = f(x(t), u(t)) = [v(t) \cos \psi(t), v(t) \sin \psi(t), \omega(t)]^\top, \quad (9)$$

where $x = [\xi, \eta, \psi]^\top$ and $u = [v, \omega]^\top$, being (ξ, η) the robot planar position, ψ the heading angle, v the linear velocity, and ω the angular velocity. Eq. (8b) is the discrete-time version of model (9).

B. Nonlinear State Constraints and Observables Generation: Cluttered Environment

Nonlinear state constraints are given by the obstacles – either stationary or moving – that the ego robot has to avoid. We assume that each j -th obstacle can be fully enclosed in a safety ellipsoid, yielding the following constraints:

$$1 - \frac{(\xi - c_{\xi,j}(t) - \nu_{\xi,j}(t)\tau)^2}{(l_{\xi,j} + \alpha_j r)^2} - \frac{(\eta - c_{\eta,j}(t) - \nu_{\eta,j}(t)\tau)^2}{(l_{\eta,j} + \alpha_j r)^2} \leq 0 \\ \Rightarrow h_{j,\tau}(x, c_j(t), \nu_j(t)) \leq 0, \quad j = 1, \dots, N_{\text{obst}}, \quad (10)$$

where N_{obst} is the number of obstacles; $c_j(t) = [c_{\xi,j}(t), c_{\eta,j}(t)]^\top$ and $(l_{\xi,j}, l_{\eta,j})$ are the j -th ellipsoid center and semi-axes, respectively; $\nu_j(t) = \dot{c}_j(t)$; r is the radius of the ego robot; α_j is a safety margin. Eq. (8c) is the discrete-time version of constraints (10).

From Eqs. (9) and (10), we can define the initial set of observables $\Phi_{\text{in}} = \{\xi, \eta, \psi, \xi^2, \eta^2\}$, which includes the system states and the nonlinear terms $([\xi^2, \eta^2]^\top = \sigma(x))$ introduced by Eq. (10).

The complete basis Φ is generated from Φ_{in} through [1, Algorithm 1], obtaining a finite-dimensional basis of 14 observables,

$$\Phi = \Phi_{\text{in}} \cup \{c_\psi, s_\psi, \xi c_\psi, \eta s_\psi, c_\psi^2, \xi s_\psi, s_\psi^2, \eta c_\psi, c_\psi s_\psi\}, \quad (11)$$

where $c_\psi = \cos \psi$ and $s_\psi = \sin \psi$. Thus, system (9) with constraints (10) admits an exact finite-dimensional Koopman lifted system, with dimension $n_z = |\Phi| = 14$, and lifted state $z = [z_x^\top, z_\sigma^\top, \dots]^\top = \phi(x) = [x^\top, \sigma(x)^\top, \dots]^\top$.

C. Lifted System Reduction and Linearization

The Koopman lifted system arising from Eqs. (9)-(11) can be further reduced in dimension (so to have a less complex K-NMPC problem) as in Sec. II-B. Also, its bilinearity (7) is linearized around $(\bar{z}, \bar{u}) = (z_k, \hat{u}_{1|k-1}^*)$ to obtain a discrete-time linear parameter-varying prediction model, i.e., $z_{k+1} = A_d(\bar{z}, \bar{u})z_k + B_d(\bar{z}, \bar{u})u_k + b_d(\bar{z}, \bar{u}) = A_{d,k}z_k + B_{d,k}u_k + b_{d,k}$.

D. Koopman NMPC Formulation

The resulting K-NMPC optimal control problem is given by

$$\min_{\hat{z}, \hat{u}} J(\hat{z}, \hat{u}) \quad (12a)$$

$$\text{s.t. } \hat{z}_0 = \phi(x_k), \quad \hat{z}_{i+1} = A_{d,k}\hat{z}_i + B_{d,k}\hat{u}_i + b_{d,k}, \quad (12b)$$

$$\hat{u}_i \in \mathcal{U}, \quad \hat{z}_{x,i} \in \mathcal{X}, \quad C_i(c_k, \nu_k)\hat{z}_{\sigma,i} \leq d_i(c_k, \nu_k), \quad (12c)$$

$$i = 0, 1, \dots, N_p - 1,$$

where the prediction model (12b) and constraints (12c) are linear thanks to the Koopman lifting. The obtained QP-MPC (12) is equivalent to NMPC (8) (albeit with the relaxations introduced in Sec. II-B and III-C) through the map $z = \phi(x)$.

IV. EXPERIMENTAL RESULTS

Our K-NMPC approach is validated through hardware-in-the-loop experiments on a real differential wheeled mobile robot, tasked to reach a target position within a cluttered environment, populated by stationary and moving obstacles (Fig. 1).

Results are reported in Fig. 2, showing that K-NMPC manages to successfully attain the control task, effectively avoiding all the obstacles, with remarkably similar trajectories to NMPC. K-NMPC execution time is within [1.54, 3.57] ms (average: 2.26 ms), while NMPC achieves [20.03, 55.29] ms (average: 27.92 ms); thus, K-NMPC outperforms NMPC by over an order of magnitude.

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