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ARTICLE

3D Exact Magneto-Electro-Elastic Static Analysis of Multilayered Plates

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ABSTRACT: This study proposes a three-dimensional (3D) coupled magneto-electro-elastic problem for the static analysis of multilayered plates embedding piezomagnetic and piezoelectric layers by considering both sensor and actuator configurations. The 3D governing equations for the magneto-electro-elastic static behavior of plates are explicitly show that are made by the three 3D equilibrium equations, the 3D divergence equation for magnetic induction, and the 3D divergence equation for the electric displacement. The proposed solution involves the exponential matrix in the thickness direction and primary variables' harmonic forms in the in-plane ones. A closed-form solution is performed considering simply-supported boundary conditions. Interlaminar continuity conditions are imposed for displacements, magnetic potential, electric potential, transverse shear/normal stresses, transverse normal magnetic induction and transverse normal electric displacement. Therefore, a layerwise approach is adopted. The results section is composed of an assessment part, where the present model is compared to past 3D electro-elastic or magneto-elastic formulations and a new benchmark part. Benchmarks consider sensor and actuator plate configurations for the fully coupled magneto-electro-elastic cases for different thickness ratios. Tabular and graphical results are presented for displacements, stresses, magnetic potential, electric potential, transverse normal magnetic induction and transverse normal electric displacement. For each presented benchmark, magneto-electro-elastic coupling and thickness and material layer effects are discussed in depth.

KEYWORDS: Multilayered and smart plates; static analyses; magneto-electro-elastic coupling; exponential matrix method; 3D model; layer-wise approach

1 Introduction

Magneto-Electric (ME) coupling in magnetostrictive-piezoelectric multiferroic structures consent to induce an electric field in the structure due to an applied magnetic field, and on the contrary, a magnetic response consequent to an applied electric field. ME voltage coefficient (the ratio of an induced electric field to an applied magnetic field) is the key parameter to measure ME coupling strength [1–3]. In the case of smart structures (both sensor and actuator configurations), this coupling evaluation is fundamental and for this reason 1D, 2D and 3D numerical/analytical magneto-electro-elastic models have great importance in such investigations.

In the field of 1D models, generally applied to structures where one dimension is predominant with respect to the other two dimensions in the cross-section, several approaches have been proposed in recent years. Milazzo and Orlando [4] developed an elastic equivalent single layer finite element formulation for shear deformable and straight magneto-electro-elastic (MEE) laminated beam. The generalized exp-function method was employed in [5] to investigate the families of solitary wave solutions of one-dimensional

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nonlinear longitudinal wave equations in a MEE circular rod. In [6], an MEE functionally graded Timoshenko microbeam model was developed thanks to both the use of the variational formulation and the extended modified couple stress theory proposed to understand microstructure effects. Plane-strain equations for static deformations of anisotropic layered MEE cylinders were solved in [7] by assuming layers as perfectly bonded at the interfaces and by solving these equations thanks to the separation of variables and eigenfunction expansion. Huang et al. [8] showed both analytical and semi-analytical solutions for anisotropic functionally graded MEE beams under an arbitrary load. The generalized plane stress problem took into account stress functions, electric displacement, and magnetic induction functions.

2D models can be applied in the numerical or analytical form to plates and shells, which are structures where the two dimensions in the in-plane directions are predominant with respect to the dimension through the thickness direction. Chen et al. [9] proposed the state-vector approach to analyze free vibrations of MEE laminated plates, where extended displacements and stresses are split up into in-plane and out-of-plane variables. Phoenix et al. [10] adopted Reissner's mixed variational theorem for static and dynamic analyses of coupled MEE problems in the case of composite/piezoelectric plates. A coupled finite element method was proposed in [11] considering higher-order approximate interpolation displacement, electric potential and magnetic potential shape functions. A fully geometrically nonlinear finite rotation shell element based on Reissner–Mindlin first-order shear deformation theory was proposed by Rao et al. in [12] for static analysis of layered MEE structures. Wang et al. [13] developed an hygrothermo-magneto-electro-elastic coupled and improved enriched finite element formulation to analyze functionally graded MEE structures; quadrilateral elements were used in this study. Carrera et al. [14,15] proposed refined 2D finite elements for MEE plates based on the principle of virtual displacements and on the Reissner's mixed variational theorem, respectively. A closed form solution for MEE bending of rectangular thin plates was developed in [16] using the Kirchhoff thin-plate theory. The large deflection of MEE laminated plates was investigated by Milazzo [17], where the first-order shear deformation theory and the von Karman stress function approach were employed. Alaimo et al. [18,19] developed an isoparametric four-node finite element for multilayered MEE plates, the first order shear deformation theory was employed. Quasi-static behavior investigations were proposed, and then large deflections in MEE multilayered plates were also analyzed. Analytical solutions for general static deformations of spherically anisotropic and multilayered MEE hollow spheres were proposed in [20]. A partial mixed layerwise finite element model for adaptive plate structures was formulated in [21] using transverse stresses, displacement components, electric and magnetic potentials as primary variables. Explicit solutions for Navier's and Lévy's solutions were derived in [22] for unsymmetric MEE composite laminated thin plates. The scaled boundary finite element method was employed in [23] to study the deformation of a MEE plate. The inhomogeneous MEE coupling element-free Galerkin method, showed in [24] by Zhou et al. was used for solving static behaviors of structures where different temperature fields were simulated. A multiphysics plate model for the analysis of MEE composite laminates was shown in [25] by applying the variational asymptotic method, reducing the multiphysically coupled three-dimensional model to a series of two-dimensional plate models. A higher-order thickness-stretched model was proposed in [26] for the electro-elastic analysis of the composite graphene origami-reinforced square plate sandwiched by piezoelectric/piezomagnetic layers subjected to multifield loads (thermal, electric, magnetic and mechanical). Kiarasi et al. [27] investigated the hygrothermal effect on natural frequencies for functionally graded annular plates integrated with piezo-magneto-electro-elastic layers resting on Pasternak foundations. The effects of hygro-thermal environments on smart composite nanoplates were investigated in [28,29] using coupled MEE constitutive and governing equations solved via a strain gradient nonlocal theory and analytical methods. The magneto-electric effect on waves in functionally graded piezoelectric-piezomagnetic fan-shaped cylindrical structures was explored in [30] using the double Legendre orthogonal

polynomial method and the Heaviside function. The nonlocal static analysis using Reddy's high-order shear deformation theory of MEE sandwich micro/nano-plates with functionally graded carbon nanotube core in a hygrothermal environment was studied in [31]. Zhang et al. [32] proposed the scaled boundary finite element method incorporated with the precise integration technique for static and free vibration of multilayered MEE plates. The multi-physics zonal Galerkin free element method was proposed in [33] for static and transient responses of functionally graded MEE structures. The MEE-coupled isogeometric analysis was shown in [34] to understand the behaviour of structures thanks to the use of Non-Uniform Rational B-Spine functions. Tornabene et al. [35,36] proposed refined 2D generalized differential quadrature methods for the thermo-hygro-electro-magneto-elastic analysis of double-curved shells using an equivalent layerwise approach. Ren et al. [37] investigated static magneto-electro-hygro-elastic multi-field coupling problems using a stabilized node-based smoothed radial point interpolation method. Under the assumption of quasi-static electric and magnetic fields, the MEE analysis including the medium and its environment was proposed in [38].

3D analytical/numerical models for the electro-magneto-elastic analysis of multilayered structures are less numerous than 2D models. They can be applied to thick and anisotropic multilayered structures to obtain correct evaluations of elastic, magnetic and electric variables through the thickness direction. The study of isotropic functionally graded MEE circular plate behavior under uniform load was considered in [39]. The analytical solution for a three-dimensional transversely isotropic axisymmetric multilayered MEE circular plate under simply supported boundary conditions was proposed in [40]. In [41], the coupled governing equations for MEE plates were derived and solved via the COMSOL software considering a three-dimensional finite element approach. Pan [42] derived an exact three-dimensional model for anisotropic MEE simply supported multilayered plates under static loads. Derivation of the state vector equations for the three dimensional MEE orthotropic media was presented by Wang et al. in [43] from governing equations and then they were employed for the analysis of multilayered MEE plates. The static response of MEE plates subjected to hygrothermal loads was investigated in [44] using the finite element method derived from the principle of total potential energy. Pan and Heyliger [45] derived analytical solutions for free vibrations of three-dimensional MEE anisotropic multilayered plates under simply supported boundary conditions. A modified Pagano method was developed in [46] for the three-dimensional analysis of functionally graded simply supported rectangular plates subjected to magneto-electro-mechanical loads. The static behavior of doubly curved functionally graded MEE shells under mechanical loads, electric displacements and magnetic fluxes was investigated in [47] via the asymptotic approach.

The 3D exact and coupled electro-magneto-elastic plate model in this study tries to fill the gap of a few works on 3D models in the literature. The governing equations in 3D form are completely coupled and they are solved in in-plane directions using Navier-type solutions and through the thickness utilizing the exponential matrix method. The multilayered approach is layerwise, and equilibrium and compatibility conditions are fully satisfied at each layer interface. The same authors proposed a similar 3D coupled electro-elastic model in [48] and a similar 3D coupled magneto-elastic model in [49]; the first original work for the pure elastic analysis was given in [50]. This study fully couples elastic, magnetic, and electric fields for the first time using the exponential matrix method and the layerwise approach. It proposes several static analyses for multilayered plates in sensor and actuator configurations. Governing, constitutive, and geometrical relations are discussed in Section 2, the solution procedure is developed in Section 3, results (both preliminary assessments and new benchmarks) are discussed in Section 4, and finally, the main conclusions are presented in Section 5.

2 Coupled Magneto-Electro-Elastic 3D Plate Model

This section presents equations for the 3D coupled magneto-electro-elastic plate problem. Each subsection is devoted to equations involved in the present formulation. In the first one, constitutive and geometrical relations are given. In the second one, the 3D equilibrium equations, the 3D divergence equation for the magnetic induction and the 3D divergence equation for the electric displacement are shown for the plate case. The geometry of the plate considered in this study is shown in Fig. 1.

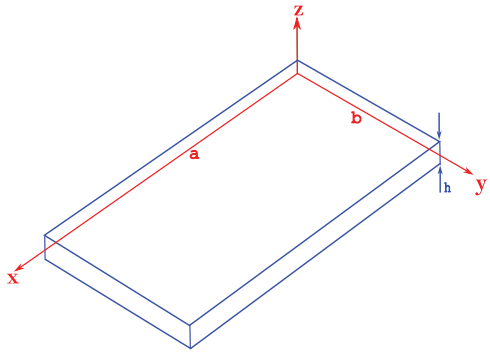


Figure 1: Geometry of the plate

2.1 Constitutive and Geometrical Relations

Constitutive and geometrical relations are utilized to couple magnetic, electric and elastic fields. For the present 3D coupled magneto-electro-elastic problem, constitutive equations can be written in the orthogonal structural reference system (x, y, z) for plates embedding k layers:

$$\boldsymbol{\sigma}^k = \boldsymbol{C}^k\boldsymbol{\varepsilon}^k - \boldsymbol{e}^{kT}\mathcal{E}^k - \boldsymbol{q}^{kT}\mathcal{H}^k, \tag{1a}$$

$$\mathcal{D}^k = \boldsymbol{e}^k\boldsymbol{\varepsilon}^k + \epsilon^k\,\mathcal{E}^k + \boldsymbol{d}^k\mathcal{H}^k, \tag{1b}$$

$$\mathcal{B}^k = \boldsymbol{q}^k\boldsymbol{\varepsilon}^k + \boldsymbol{d}^k\mathcal{E}^k + \boldsymbol{\mu}^k\mathcal{H}^k. \tag{1c}$$

$\boldsymbol{\sigma}^k$ is the 6×1 stress vector, $\boldsymbol{C}^k$ is the 6×6 elastic coefficient matrix, $\boldsymbol{\varepsilon}^k$ is the 6×1 strain vector, $\boldsymbol{e}^k$ is the 3×6 piezoelectric coefficient matrix, $\mathcal{E}^k$ is the 3×1 electric field vector, $\boldsymbol{q}^k$ is the 3×6 piezomagnetic coefficient matrix, $\mathcal{H}^k$ is the 3×1 magnetic field vector, $\mathcal{D}^k$ is the 3×1 electric displacement vector, ϵ^k is the 3×3 electric permittivity matrix, $\boldsymbol{d}^k$ is the 3×3 electro-magnetic coupling coefficient matrix, $\mathcal{B}^k$ is the 3×1 magnetic induction vector and $\boldsymbol{\mu}^k$ is the 3×3 magnetic permittivity matrix. T means the transpose of a vector or a matrix.

All vectors and matrices involved in Eq. (1) are here explicitly written:

$$\boldsymbol{\sigma}^k = \begin{Bmatrix} \sigma^k_{xx} \\ \sigma^k_{yy} \\ \sigma^k_{zz} \\ \sigma^k_{yz} \\ \sigma^k_{xz} \\ \sigma^k_{xy} \end{Bmatrix}, \quad \boldsymbol{C}^k = \begin{bmatrix} C^k_{11} & C^k_{12} & C^k_{13} & 0 & 0 & C^k_{16} \\ C^k_{12} & C^k_{22} & C^k_{23} & 0 & 0 & C^k_{26} \\ C^k_{13} & C^k_{23} & C^k_{33} & 0 & 0 & C^k_{36} \\ 0 & 0 & 0 & C^k_{44} & C^k_{45} & 0 \\ 0 & 0 & 0 & C^k_{45} & C^k_{55} & 0 \\ C^k_{16} & C^k_{26} & C^k_{36} & 0 & 0 & C^k_{66} \end{bmatrix}, \quad \boldsymbol{\varepsilon}^k = \begin{Bmatrix} \varepsilon^k_{xx} \\ \varepsilon^k_{yy} \\ \varepsilon^k_{zz} \\ \gamma^k_{yz} \\ \gamma^k_{xz} \\ \gamma^k_{xy} \end{Bmatrix}, \tag{2a}$$

$$\boldsymbol{e}^k = \begin{bmatrix} 0 & 0 & 0 & e_{14}^k & e_{15}^k & 0 \\ 0 & 0 & 0 & e_{24}^k & e_{25}^k & 0 \\ e_{31}^k & e_{32}^k & e_{33}^k & 0 & 0 & e_{36}^k \end{bmatrix}, \quad \mathcal{E}^k = \begin{Bmatrix} \mathcal{E}_x^k \\ \mathcal{E}_y^k \\ \mathcal{E}_z^k \end{Bmatrix}, \quad \boldsymbol{q}^k = \begin{bmatrix} 0 & 0 & 0 & q_{14}^k & q_{15}^k & 0 \\ 0 & 0 & 0 & q_{24}^k & q_{25}^k & 0 \\ q_{31}^k & q_{32}^k & q_{33}^k & 0 & 0 & q_{36}^k \end{bmatrix}, \tag{2b}$$

$$\mathcal{H}^k = \begin{Bmatrix} \mathcal{H}_x^k \\ \mathcal{H}_y^k \\ \mathcal{H}_z^k \end{Bmatrix}, \quad \mathcal{D}^k = \begin{Bmatrix} \mathcal{D}_x^k \\ \mathcal{D}_y^k \\ \mathcal{D}_z^k \end{Bmatrix}, \quad \epsilon^k = \begin{bmatrix} \epsilon_{11}^k & \epsilon_{12}^k & 0 \\ \epsilon_{12}^k & \epsilon_{22}^k & 0 \\ 0 & 0 & \epsilon_{33}^k \end{bmatrix}, \quad \boldsymbol{d}^k = \begin{bmatrix} d_{11}^k & d_{12}^k & 0 \\ d_{12}^k & d_{22}^k & 0 \\ 0 & 0 & d_{33}^k \end{bmatrix}, \tag{2c}$$

$$\mathcal{B}^k = \begin{Bmatrix} \mathcal{B}_x^k \\ \mathcal{B}_y^k \\ \mathcal{B}_z^k \end{Bmatrix}, \quad \boldsymbol{\mu}^k = \begin{bmatrix} \mu_{11}^k & \mu_{12}^k & 0 \\ \mu_{12}^k & \mu_{22}^k & 0 \\ 0 & 0 & \mu_{33}^k \end{bmatrix}. \tag{2d}$$

Geometrical relations for plates can be written as:

$$\epsilon^k = \boldsymbol{\Delta} \boldsymbol{u}^k, \tag{3a}$$

$$\mathcal{H}^k = -\boldsymbol{\Delta}_{\mathcal{H}} \psi^k, \tag{3b}$$

$$\mathcal{E}^k = -\boldsymbol{\Delta}_{\mathcal{E}} \phi^k, \tag{3c}$$

where $\boldsymbol{\Delta}$ is the 6×3 derivative matrix for the elastic field, $\boldsymbol{\Delta}_{\mathcal{H}}$ is the 3×1 derivative vector for the magnetic field and $\boldsymbol{\Delta}_{\mathcal{E}}$ is the 3×1 derivative vector for the electric field. These derivative matrices and vectors are expressed as:

$$\boldsymbol{\Delta} = \begin{bmatrix} \dfrac{\partial}{\partial x} & 0 & 0 \\ 0 & \dfrac{\partial}{\partial y} & 0 \\ 0 & 0 & \dfrac{\partial}{\partial z} \\ 0 & \dfrac{\partial}{\partial z} & \dfrac{\partial}{\partial y} \\ \dfrac{\partial}{\partial z} & 0 & \dfrac{\partial}{\partial x} \\ \dfrac{\partial}{\partial y} & \dfrac{\partial}{\partial x} & 0 \end{bmatrix}, \qquad \boldsymbol{\Delta}_{\mathcal{H}} = \boldsymbol{\Delta}_{\mathcal{E}} = \begin{bmatrix} \dfrac{\partial}{\partial x} \\ \dfrac{\partial}{\partial y} \\ \dfrac{\partial}{\partial z} \end{bmatrix}. \tag{4}$$

$\frac{\partial}{\partial x}$, $\frac{\partial}{\partial y}$ and $\frac{\partial}{\partial z}$ indicate partial derivatives in x, y and z directions, respectively.

2.2 3D Magneto-Electro-Elastic Governing Equations for Plates

Governing equations for plates include the three 3D equilibrium equations for the elastic field, the 3D divergence equation of the magnetic induction for the magnetic field and the 3D divergence equation of the electric displacement for the electric field. These five equations are coupled in a unique system.

The three 3D equilibrium equations for the plate case written in terms of stresses are:

$$\sigma_{xx,x}^k + \sigma_{xy,y}^k + \sigma_{xz,z}^k = 0, \tag{5a}$$

$$\sigma_{xy,x}^k + \sigma_{yy,y}^k + \sigma_{yz,z}^k = 0, \tag{5b}$$

$$\sigma_{xz,x}^k + \sigma_{yz,y}^k + \sigma_{zz,z}^k = 0, \tag{5c}$$

where stresses σ^k_{xx}, σ^k_{xy}, σ^k_{xz}, σ^k_{xy}, σ^k_{yy}, $\sigma^k_{\beta z}$, σ^k_{zz} are dependent from x, y and z. For this reason, the present formulation has a three-dimensional approach.

The 3D divergence equation of the magnetic induction for plates can be written as:

$$\mathcal{B}^k_{x,x} + \mathcal{B}^k_{y,y} + \mathcal{B}^k_{z,z} = 0. \tag{6}$$

Analogously, the 3D divergence equation of the electric displacement for plates is:

$$\mathcal{D}^k_{x,x} + \mathcal{D}^k_{y,y} + \mathcal{D}^k_{z,z} = 0. \tag{7}$$

Subscripts, x, y and, z indicate partial derivatives with respect to x, y and z directions, respectively.

3 Navier Harmonic Forms and Exponential Matrix Method

The set of equations for the 3D magneto-electro-elastic problem for plates is composed of Eqs. (5)–(7). The resolution method is proposed and discussed in depth.

In order to write the five second-order differential equations in terms of primary variables, geometric and constitutive relations (Eqs. (1) and (3)) have to be introduced into Eqs. (5)–(7). In this way, the 3D governing equations are written in terms of primary variables u^k, v^k, w^k, ψ^k and ϕ^k. In addition, the following terms must be set at zero to have a closed from solution:

$$C^k_{16} = C^k_{26} = C^k_{36} = C^k_{45} = 0, \quad e^k_{14} = e^k_{25} = e^k_{36} = 0, \quad q^k_{14} = q^k_{25} = q^k_{36} = 0, \quad \epsilon^k_{12} = 0, \quad \mu^k_{12} = 0, \quad d^k_{12} = 0. \tag{8}$$

In order to solve the 3D magneto-electro-elastic problem for plates, the first step is the imposition of the Navier harmonic forms in the in-plane directions x and y. These harmonic forms, in the case of simply supported sides, can be explicitly written as:

$$u^k(x,y,z) = U^k(z)\cos(\bar{\alpha}x)\sin(\bar{\beta}y), \tag{9a}$$
$$v^k(x,y,z) = V^k(z)\sin(\bar{\alpha}x)\cos(\bar{\beta}y), \tag{9b}$$
$$w^k(x,y,z) = W^k(z)\sin(\bar{\alpha}x)\sin(\bar{\beta}y), \tag{9c}$$
$$\phi^k(x,y,z) = \Phi^k(z)\sin(\bar{\alpha}x)\sin(\bar{\beta}y), \tag{9d}$$
$$\psi^k(x,y,z) = \Psi^k(z)\sin(\bar{\alpha}x)\sin(\bar{\beta}y), \tag{9e}$$

where $U^k(z)$, $V^k(z)$, $W^k(z)$, $\Phi^k(z)$, $\Psi^k(z)$ are the amplitudes for each primary variable. Terms $\bar{\alpha}$ and $\bar{\beta}$ are written as:

$$\bar{\alpha} = \frac{m\pi}{a}, \qquad \bar{\beta} = \frac{n\pi}{b}, \tag{10}$$

considering m, n the half-wave numbers and a, b the in-plane dimensions of the plate in x and y directions, respectively.

Navier harmonic forms fulfill the boundary conditions for the simply-supported constraints:

$$\begin{aligned} &\phi^k = 0, \quad \psi^k = 0, \quad w^k = 0, \quad v^k = 0, \quad \sigma^k_{xx} = 0, \quad \text{for} \quad x = 0, a, \\ &\phi^k = 0, \quad \psi^k = 0, \quad w^k = 0, \quad u^k = 0, \quad \sigma^k_{yy} = 0, \quad \text{for} \quad y = 0, b. \end{aligned} \tag{11}$$

The imposition of harmonic forms of Eq. (9) permits to get the 3D magneto-electro-elastic set of equations in terms of primary variable amplitudes:

$$\left(-\bar{\alpha}^2 C_{11}^k - \bar{\beta}^2 C_{66}^k\right) U^k + \left(-\bar{\alpha}\bar{\beta} C_{12}^k - \bar{\alpha}\bar{\beta} C_{66}^k\right) V^k + \left(\bar{\alpha} C_{13}^k + \bar{\alpha} C_{55}^k\right) W_{,z}^k + C_{55}^k U_{,zz}^k + \\ + \left(\bar{\alpha} e_{31}^k + \bar{\alpha} e_{15}^k\right) \Phi_{,z}^k + \left(\bar{\alpha} q_{31}^k + \bar{\alpha} q_{15}^k\right) \Psi_{,z}^k = 0, \tag{12a}$$

$$\left(-\bar{\alpha}^2 C_{66}^k - \bar{\beta}^2 C_{22}^k\right) V^k + \left(-\bar{\alpha}\bar{\beta} C_{12}^k - \bar{\alpha}\bar{\beta} C_{66}^k\right) U^k + \left(\bar{\beta} C_{44}^k + \bar{\beta} C_{23}^k\right) W_z^k + C_{44}^k V_{,zz}^k + \\ + \left(\bar{\beta} e_{32}^k + \bar{\beta} e_{24}^k\right) \Phi_{,z}^k + \left(\bar{\beta} q_{32}^k + \bar{\beta} q_{24}^k\right) \Psi_{,z}^k = 0, \tag{12b}$$

$$\left(-\bar{\alpha}^2 C_{55}^k - \bar{\beta}^2 C_{44}^k\right) W^k + \left(-\bar{\alpha} C_{55}^k - \bar{\alpha} C_{13}^k\right) U_{,z}^k + \left(-\bar{\beta} C_{44}^k - \bar{\beta} C_{23}^k\right) V_{,z}^k + C_{33}^k W_{,zz}^k + \\ + \left(-\bar{\alpha}^2 e_{15}^k - \bar{\beta}^2 e_{24}^k\right) \Phi^k + \left(-\bar{\alpha}^2 q_{15}^k - \bar{\beta}^2 q_{24}^k\right) \Psi^k + e_{33}^k \Phi_{,zz}^k + q_{33}^k \Psi_{,zz}^k = 0, \tag{12c}$$

$$\left(-\bar{\alpha}^2 e_{15}^k - \bar{\beta}^2 e_{24}^k\right) W^k + \left(-\bar{\alpha} e_{15}^k - \bar{\alpha} e_{31}^k\right) U_{,z}^k + \left(-\bar{\beta} e_{24}^k - \bar{\beta} e_{32}^k\right) V_{,z}^k + e_{33}^k W_{zz}^k + \\ + \left(\bar{\alpha}^2 \epsilon_{11}^k + \bar{\beta}^2 \epsilon_{22}^k\right) \Phi^k - \epsilon_{33}^k \Phi_{,zz}^k + \left(\bar{\alpha}^2 d_{11}^k + \bar{\beta}^2 d_{22}^k\right) \Psi^k - d_{33}^k \Psi_{,zz}^k = 0, \tag{12d}$$

$$+ \left(-\bar{\alpha}^2 q_{15}^k - \bar{\beta}^2 q_{24}^k\right) W^k + \left(-\bar{\alpha} q_{15}^k - \bar{\alpha} q_{31}^k\right) U_{,z}^k + \left(-\bar{\beta} q_{24}^k - \bar{\beta} q_{32}^k\right) V_{,z}^k + q_{33}^k W_{zz}^k + \\ + \left(\bar{\alpha}^2 d_{11}^k + \bar{\beta}^2 d_{22}^k\right) \Phi^k - d_{33}^k \Phi_{,zz}^k + \left(\bar{\alpha}^2 \mu_{11}^k + \bar{\beta}^2 \mu_{22}^k\right) \Psi^k - \mu_{33}^k \Psi_{,zz}^k = 0. \tag{12e}$$

The exponential matrix method is the approach adopted to solve Eq. (12) along the thickness direction. To get first order differential equations in z starting from the second order differential equations (Eq. (12)), a redoubling procedure must be done. This procedure also duplicates the number of unknowns: $U^k(z)$, $V^k(z)$, $W^k(z)$, $\Phi^k(z)$, $\Psi^k(z)$, $U_{,z}^k(z)$, $V_{,z}^k(z)$, $W_{,z}^k(z)$, $\Phi_{,z}^k(z)$, $\Psi_{,z}^k(z)$. The use of the exponential matrix resolution method allows correct calculations of first derivatives in z because they are now the primary variables of the problem. In this way, the computation of stresses, strains, electric displacement, and magnetic induction along thickness direction is always correct and in three-dimensional form.

Eq. (12) can be written in a compact matrix form as follows:

$$\boldsymbol{D}^k \boldsymbol{X}_{,z}^k = \boldsymbol{A}^k \boldsymbol{X}^k \;\Rightarrow\; \boldsymbol{X}_{,z}^k = \boldsymbol{A}^{*k} \boldsymbol{X}^k \,, \tag{13}$$

where $\boldsymbol{D}^k$ and $\boldsymbol{A}^k$ are 10×10 matrices, $\boldsymbol{X}_{,z}^k$ is the 10×1 vector of unknowns derived in z, $\boldsymbol{X}^k$ is the 10×1 vector of unknowns and $\boldsymbol{A}^{*k} = \boldsymbol{D}^{-1k} \boldsymbol{A}^k$ is a 10×10 matrix. Vector of unknowns $\boldsymbol{X}^k$ is defined as follows:

$$\boldsymbol{X}^k = \{U^k, V^k, W^k, \Phi^k, \Psi^k, U_{,z}^k, V_{,z}^k, W_{,z}^k, \Phi_{,z}^k, \Psi_{,z}^k\}^T. \tag{14}$$

A possible solution of Eq. (13) can be obtained with the exponential matrix method as follows:

$$\boldsymbol{X}^k(h_k) = exp\left(\boldsymbol{A}^{*k} h_k\right) \boldsymbol{X}^k(0) = \left[\sum_{i=0}^{N} \frac{(\boldsymbol{A}^{*k})^i}{i!} h_k^i\right] \boldsymbol{X}^k(0), \tag{15}$$

where $(\boldsymbol{A}^{*k})^0 = \boldsymbol{I}$ is the 10×10 identity matrix, and h_k is the thickness of each k layer. The exponential matrix in Eq. (15) is computed considering the Taylor expansion.

The imposition of the interlaminar continuity between two adjacent k layers permits the layerwise approach. So, these conditions need to be imposed on primary variables, transverse shear stresses, transverse normal stresses, transverse normal electric displacement and transverse normal magnetic induction:

$$u_b^k = u_t^{k-1}, \quad v_b^k = v_t^{k-1}, \quad w_b^k = w_t^{k-1}, \quad \phi_b^k = \phi_t^{k-1}, \quad \psi_b^k = \psi_t^{k-1}, \tag{16a}$$

$$\sigma^k_{xz_b} = \sigma^{k-1}_{xz_t}, \quad \sigma^k_{yz_b} = \sigma^{k-1}_{yz_t}, \quad \sigma^k_{zz_b} = \sigma^{k-1}_{zz_t}, \quad \mathcal{D}^k_{z_b} = \mathcal{D}^{k-1}_{z_t}, \quad \mathcal{B}^k_{z_b} = \mathcal{B}^{k-1}_{z_t}. \tag{16b}$$

t is the *top* of the previous $k-1$ layer, and b is the *bottom* of the adjacent k layer. k goes from 1 to N_L (total number of layers). Introducing Eq. (9) in Eq. (16), interlaminar continuity conditions are:

$$U^k_b = U^{k-1}_t, \tag{17a}$$
$$V^k_b = V^{k-1}_t, \tag{17b}$$
$$W^k_b = W^{k-1}_t, \tag{17c}$$
$$\Phi^k_b = \Phi^{k-1}_t, \tag{17d}$$
$$\Psi^k_b = \Psi^{k-1}_t, \tag{17e}$$
$$C^k_{55}\bar{\alpha}W^k_b + C^k_{55}U^k_{,z_b} + e^k_{15}\bar{\alpha}\Phi^k_b + q^k_{15}\bar{\alpha}\Psi^k_b = C^{k-1}_{55}\bar{\alpha}W^{k-1}_t + C^{k-1}_{55}U^{k-1}_{,z_t} + e^{k-1}_{15}\bar{\alpha}\Phi^{k-1}_t + q^{k-1}_{15}\bar{\alpha}\Psi^{k-1}_t, \tag{17f}$$
$$C^k_{44}\bar{\beta}W^k_b + C^k_{44}V^k_{,z_b} + e^k_{24}\bar{\beta}\Phi^k_b + q^k_{24}\bar{\beta}\Psi^k_b = C^{k-1}_{44}\bar{\beta}W^{k-1}_t + C^{k-1}_{44}V^{k-1}_{,z_t} + e^{k-1}_{25}\bar{\beta}\Phi^{k-1}_t + q^{k-1}_{25}\bar{\beta}\Psi^{k-1}_t, \tag{17g}$$
$$C^k_{13}\bar{\alpha}U^k_b - C^k_{23}\bar{\beta}V^k_b + C^k_{33}W^k_{,z_b} + e^k_{33}\Phi^k_{,z_b} + q^k_{33}\Psi^k_{,z_b} = -C^{k-1}_{13}\bar{\alpha}U^{k-1}_t - C^{k-1}_{23}\bar{\beta}V^{k-1}_t + C^{k-1}_{33}W^{k-1}_{,z_t} + \\ + e^{k-1}_{33}\Phi^{k-1}_{,z_t} + q^{k-1}_{33}\Psi^{k-1}_{,z_t}, \tag{17h}$$
$$-e^k_{31}\bar{\alpha}U^k_b - e^k_{32}\bar{\beta}V^k_b + e^k_{33}W^k_{,z_b} - \epsilon^k_{33}\Phi^k_{,z_b} - d^k_{33}\Psi^k_{,z_b} = -e^{k-1}_{31}\bar{\alpha}U^k_t - e^{k-1}_{32}\bar{\beta}V^k_t + e^{k-1}_{33}W^{k-1}_{,z_t} + \\ - \epsilon^{k-1}_{33}\Phi^{k-1}_{,z_t} - d^{k-1}_{33}\Psi^{k-1}_{,z_t}, \tag{17i}$$
$$-q^k_{31}\bar{\alpha}U^k_b - q^k_{32}\bar{\beta}V^k_b + q^k_{33}W^k_{,z_b} - d^k_{33}\Phi^k_{,z_b} - \mu^k_{33}\Psi^k_{,z_b} = -q^{k-1}_{31}\bar{\alpha}U^k_t - q^{k-1}_{32}\bar{\beta}V^k_t + q^{k-1}_{33}W^{k-1}_{,z_t} + \\ - d^{k-1}_{33}\Phi^{k-1}_{,z_t} - \mu^{k-1}_{33}\Phi^{k-1}_{,z_t}. \tag{17j}$$

All these equations can be compacted in a matrix form as follows:

$$\boldsymbol{X}^k_b = \boldsymbol{T}^{k,k-1}\boldsymbol{X}^{k-1}_t, \tag{18}$$

where $\boldsymbol{T}^{k,k-1}$ is the 10×10 transfer matrix between layer k and layer $k-1$. Terms of matrix $\boldsymbol{T}^{k,k-1}$ include constant coefficients coming from a rearrangement of Eq. (17) in terms of primary variables.

Therefore, the solution along the z direction is possible by considering a recursive substitution as follows:

$$\boldsymbol{X}^{N_L}(h_{N_L}) = \boldsymbol{A}^{**N_L}\boldsymbol{T}^{N_L,N_L-1}\ldots\boldsymbol{T}^{2,1}\boldsymbol{A}^{**1}\boldsymbol{X}^1(0) \Rightarrow \boldsymbol{X}^{N_L}(h_{N_L}) = \boldsymbol{H}_m\boldsymbol{X}^1(0), \tag{19}$$

where $\boldsymbol{H}_m$ is the 10×10 matrix; its terms consider plate dimensions, thickness and material layer configuration of the multilayered plate. The matrix $\boldsymbol{H}_m$ is always a 10×10 matrix, despite the number of layers along the thickness direction and the order$N$ of the exponential matrix.

Load boundary conditions can be imposed on the external surfaces of the plate in terms of mechanical loads, electric potential, and/or magnetic potential. The transverse normal mechanical load has the following harmonic form:

$$p^k_z(x, y, z) = P^k_z(z)\sin(\bar{\alpha}x)\sin(\bar{\beta}y), \tag{20}$$

harmonic forms of electric potential and magnetic potential are already described in Eqs. (9d) and (9e), respectively. $P^k_z(z)$, $\Phi^k(z)$ and $\Psi^k(z)$ are the amplitudes of external mechanical, electric, and magnetic loads. They can be imposed at the bottom (b) of the first layer ($k = 1$) or at the top (t) of the last layer ($k = N_L$).

Load boundary conditions can be written in matrix form as:

$$\begin{bmatrix} B^1_{1_b} & B^1_{2_b} & B^1_{3_b} & 0 & 0 & 0 & 0 & B^1_{4_b} & B^1_{5_b} & B^1_{6_b} \\ 0 & B^1_{7_b} & B^1_{8_b} & B^1_{9_b} & B^1_{10_b} & 0 & B^1_{11_b} & 0 & 0 & 0 \\ B^1_{12_b} & 0 & B^1_{13_b} & B^1_{14_b} & B^1_{15_b} & B^1_{16_b} & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \begin{Bmatrix} U^1_b \\ V^1_b \\ W^1_b \\ \Phi^1_b \\ \Psi^1_b \\ U^1_{,z\,b} \\ V^1_{,z\,b} \\ W^1_{,z\,b} \\ \Phi^1_{,z\,b} \\ \Psi^1_{,z\,b} \end{Bmatrix} = \begin{Bmatrix} P^1_{z_b} \\ 0 \\ 0 \\ \Phi^1_b \\ \Psi^1_b \end{Bmatrix} \quad \text{for } z = -h/2, \tag{21}$$

$$\begin{bmatrix} B^{N_L}_{1_t} & B^{N_L}_{2_t} & B^{N_L}_{3_t} & 0 & 0 & 0 & 0 & B^{N_L}_{4_t} & B^{N_L}_{5_t} & B^{N_L}_{6_t} \\ 0 & B^{N_L}_{7_t} & B^{N_L}_{8_t} & B^{N_L}_{9_t} & B^{N_L}_{10_t} & 0 & B^{N_L}_{11_t} & 0 & 0 & 0 \\ B^{N_L}_{12_t} & 0 & B^{N_L}_{13_t} & B^{N_L}_{14_t} & B^{N_L}_{15_t} & B^{N_L}_{16_t} & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \begin{Bmatrix} U^{N_L}_t \\ V^{N_L}_t \\ W^{N_L}_t \\ \Phi^{N_L}_t \\ \Psi^{N_L}_t \\ U^{N_L}_{,z_t} \\ V^{N_L}_{,z_t} \\ W^{N_L}_{,z_t} \\ \Phi^{N_L}_{,z_t} \\ \Psi^{N_L}_{,z_t} \end{Bmatrix} = \begin{Bmatrix} P^{N_L}_{z_t} \\ 0 \\ 0 \\ \Phi^{N_L}_t \\ \Psi^{N_L}_t \end{Bmatrix} \quad \text{for } z = +h/2, \tag{22}$$

that can be further compacted in the following form:

$$\boldsymbol{B}^1_b \boldsymbol{X}^1_b = \boldsymbol{P}^1_{\,b}, \tag{23a}$$

$$\boldsymbol{B}^{N_L}_t \boldsymbol{X}^{N_L}_t = \boldsymbol{P}^{N_L}_{\,t}, \tag{23b}$$

where $\boldsymbol{B}^1_b$ and $\boldsymbol{B}^{N_L}_t$ are the 5×10 load boundary condition matrix and $\boldsymbol{P}^1_{\,b}$ and $\boldsymbol{P}^{N_L}_{\,t}$ are the 5×1 bottom and top load vectors of the plate, respectively. Considering Eq. (19), it is possible to write Eq. (23) as:

$$\begin{bmatrix} \boldsymbol{B}^1_b \\ \boldsymbol{B}^{N_L}_t \boldsymbol{H}_m \end{bmatrix} \boldsymbol{X}^1_b = \begin{Bmatrix} \boldsymbol{P}^1_{\,b} \\ \boldsymbol{P}^{N_L}_{\,t} \end{Bmatrix} \Rightarrow \boldsymbol{E}\boldsymbol{X}^1_b = \boldsymbol{P}, \tag{24}$$

where $\boldsymbol{E}$ is the 10×10 matrix including the multilayered configuration characteristics.

The present 3D magneto-electro-elastic formulation can analyze both sensor and actuator configurations. The vector of external loads $\boldsymbol{P}$ assumes a slightly different form in the two cases:

$$\boldsymbol{P} = \begin{Bmatrix} P_{z_b}^1 \\ 0 \\ 0 \\ 0 \\ 0 \\ P_{z_t}^{N_L} \\ 0 \\ 0 \\ 0 \\ 0 \end{Bmatrix} \quad \text{for the sensor case,} \tag{25}$$

$$\boldsymbol{P} = \begin{Bmatrix} 0 \\ 0 \\ 0 \\ \Phi_b^1 \\ \Psi_b^1 \\ 0 \\ 0 \\ 0 \\ \Phi_t^{N_L} \\ \Psi_t^{N_L} \end{Bmatrix} \quad \text{for the actuator case.} \tag{26}$$

Due to the resolution of the linear system proposed in Eq. (24) and considering the recursive use of Eqs. (15) and (18), trends of primary variables along the thickness direction can be evaluated. The presented analytical formulation is simple and elegant, permitting the correct results for each thickness ratio of the plate. Matlab code (done with Matlab R2022a version) runs analysis in a few seconds, as the heavier computation cost regards iterative matrix multiplications of 10×10 matrices.

4 Results

The present section is divided into an assessment subsection and a new benchmark subsection. In the assessment subsection, the present magneto-electro-elastic 3D-u-ϕ-ψ model is compared to the 3D electro-elastic (3D-u-ϕ) model developed in [48], with the 3D magneto-elastic (3D-u-ψ) model developed in [49] and with the 3D magneto-electro-elastic model developed by Pan [42]. The acronym 3D-u-ϕ-ψ summarizes the main peculiarities of the model: three-dimensional formulation where primary variables are displacements and their derivatives in z (stated as u), electric potential and its derivative in z (indicated with ϕ) and magnetic potential and its derivative in z (indicated with ψ). In the benchmark subsection, a new multilayered square plate in both sensor and actuator configurations is proposed considering different a/h thickness ratios (from thick to thin plates). As far as the authors know, magnetic permittivity coefficients μ_1 and μ_2 can be found in literature mainly with the negative sign ($\mu_1 = \mu_2 = -590\,10^3$ nH/m), as assessed and validated in [51], but also with a positive sign ($\mu_1 = \mu_2 = 590\,10^3$ nH/m) [52]. For this time, the proposed benchmark case is provided considering μ_1 and μ_2 with both signs to overcome this discrepancy. The new benchmark subsection is useful for those scientists and researchers interested in the development of 3D/2D numerical or analytical models for magneto-electro-elastic structures.

4.1 Assessments

This section presents a simply supported multilayered square plate. Different thickness ratios are considered, from thick (a/h = 4) to thin (a/h = 100) plates for both sensor and actuator configurations. The present 3D magneto-electro-elastic model (3D-u-ϕ-ψ) is compared to the 3D electro-elastic model (3D-u-ϕ) [48], with the 3D magneto-elastic model (3D-u-ψ) [49] and with the 3D magneto-electro-elastic plate model (3D) by Pan [42]. In this way, the magneto-electro-elastic coupling is first validated separately and then fully coupled. The opportune choice of the order$N$ for the exponential matrix was deeply discussed in [53] for different thickness ratios, geometries and lamination schemes. In the case of multilayered plate structures with an evident transverse anisotropy, an order N = 9 always gives correct results even if the plate is very thick. This order$N$ can be reduced if opportune mathematical layers$M$ are applied, but they are not necessary for plate geometries and homogeneous materials.

The first assessment (A1) is devoted to a simply supported multilayered square plate in the sensor (A1-S) and actuator (A1-A) configurations. The considered multilayered plate lamination is PZT-4/Al2024/Foam/Al2024/PZT-4 where $h_{PZT-4} = h_{Al2024} = 0.1h$ and $h_{Foam} = 0.6h$ where h is the total thickness of the plate. Geometrical data and load conditions are in Table 1 and material properties are collected in Table 2. Elastic properties reported in Table 2 are computed with relations explicitly written for orthotropic materials in [54], starting from the elastic coefficients of the material. The reference solution is the 3D electro-elastic model (3D-u-ϕ model) proposed in [48]. Tables 3 and 4 show comparisons between the present 3D-u-ϕ-ψ model and the 3D-u-ϕ model [48] for both sensor and actuator configurations in terms of displacements, stresses, electric potential, and electric displacement. The accordance between the results is good for each thickness ratio and for each variable proposed. The perfect accordance of results is visible for both primary variables (u, w, ϕ) and secondary variables (σ_{xx}, σ_{zz}, D_z), certifying the correct computation of each kind of variable. Therefore, this assessment permits validation of the electro-elastic coupling and the thickness and material layer effects in multilayered piezoelectric plates.

Table 1: Geometrical data and load conditions for assessment (A) and benchmark (B) cases. "-S" indicates the "sensor" configuration and "-A" indicates the "actuator" configuration. "/" means "not included in the model"

	A1-S	**A1-A**	**A2-S**	**A2-A**	**A3-S**	**B-S**	**B-A**
a [m]	1	1	1	1	1	1	1
b [m]	1	1	1	1	1	1	1
h [m]	variable	variable	variable	variable	0.3	variable	variable
m	1	1	1	1	1	1	1
n	1	1	1	1	1	1	1
P_{z_t} [Pa]	10000	0	10000	0	1	10000	0
P_{z_b} [Pa]	0	0	0	0	1	0	0
ϕ_t [V]	0	100	/	/	free	0	10
ϕ_b [V]	0	0	/	/	free	0	0
ψ_t [A]	/	/	0	10	free	0	15
ψ_b [A]	/	/	0	0	free	0	0

Table 2: Elastic, electric and magnetic characteristics for materials involved in assessment and benchmark cases

	Al2024 [48]	**PZT-4** [48]	**Foam** [48]	$CoFe_2O_4$ [49]	$BaTiO_3$ [42]	**Adaptive wood** [51]	**Composite** [49]
E_1 [GPa]	73	81.3	0.180	154.32	116.33	154.32	172.37
E_2 [GPa]	73	81.3	0.180	154.32	116.33	154.32	6.895
E_3 [GPa]	73	64.5	0.180	142.83	111.93	142.83	6.895
ν_{12}	0.3	0.329	0.37	0.36564	0.30709	0.36564	0.25
ν_{13}	0.3	0.432	0.37	0.40133	0.33362	0.40133	0.25
ν_{23}	0.3	0.432	0.37	0.40133	0.33362	0.40133	0.25
G_{12} [GPa]	28.077	30.6	0.65693	56.5	44.5	56.5	3.447
G_{13} [GPa]	28.077	25.6	0.65693	45.3	43	45.3	3.447
G_{23} [GPa]	28.077	25.6	0.65693	45.3	43	45.3	1.379
e_{15} [C/m^2]	0	12.72	0	0	11.6	11.6	0
e_{24} [C/m^2]	0	12.72	0	0	11.6	11.6	0
e_{31} [C/m^2]	0	−5.20	0	0	−4.4	−4.4	0
e_{32} [C/m^2]	0	−5.20	0	0	−4.4	−4.4	0
e_{33} [C/m^2]	0	15.08	0	0	18.6	18.6	0
ϵ_1 [nF/m]	0.008854	0.008854	13.06	0.08	11.2	0.08	0.008854
ϵ_2 [nF/m]	0.008854	0.008854	13.06	0.08	11.2	0.08	0.008854
ϵ_3 [nF/m]	0.008854	0.008854	11.51	0.093	12.6	0.093	0.008854
q_{15} [T]	0	0	0	550	0	560	0
q_{24} [T]	0	0	0	550	0	560	0
q_{31} [T]	0	0	0	580.3	0	580	0
q_{32} [T]	0	0	0	580.3	0	580	0
q_{33} [T]	0	0	0	699.7	0	700	0
μ_1 [nH/m]	$4\pi \cdot 10^2$	$4\pi \cdot 10^2$	$4\pi \cdot 10^2$	$-590 \cdot 10^3$	$5 \cdot 10^3$	variable	$4\pi \cdot 10^2$
μ_2 [nH/m]	$4\pi \cdot 10^2$	$4\pi \cdot 10^2$	$4\pi \cdot 10^2$	$-590 \cdot 10^3$	$5 \cdot 10^3$	variable	$4\pi \cdot 10^2$
μ_3 [nH/m]	$4\pi \cdot 10^2$	$4\pi \cdot 10^2$	$4\pi \cdot 10^2$	$157 \cdot 10^3$	$10 \cdot 10^3$	$157 \cdot 10^3$	$4\pi \cdot 10^2$
d_1 [Ns/VC]	0	0	0	0	0	$3 \cdot 10^{-12}$	0
d_2 [Ns/VC]	0	0	0	0	0	$3 \cdot 10^{-12}$	0
d_3 [Ns/VC]	0	0	0	0	0	$3 \cdot 10^{-12}$	0

Table 3: Assessment A1-S, simply supported multilayered electro-elastic square plate in sensor configuration

a/h	**4**	**10**	**20**	**50**	**100**
		$u\,[10^{-7}\ \mathrm{m}](\tilde{z} = 0.75h)$			
3D-u-ϕ [48]	8.6313	12.619	6.2546	−59.111	−296.59
3D-u-ϕ-ψ	8.6313	12.619	6.2547	−59.111	−296.59
		$w\,[10^{-6}\ \mathrm{m}](\tilde{z} = 0.5h)$			
3D-u-ϕ [48]	8.9184	54.445	156.24	835.45	4703.4
3D-u-ϕ-ψ	8.9184	54.445	156.24	835.45	4703.4
		$\sigma_{xx}\,[10^3\ \mathrm{Pa}](\tilde{z} = 0.75h)$			
3D-u-ϕ [48]	2.5461	3.1429	4.0125	9.9881	31.321
3D-u-ϕ-ψ	2.5460	3.1429	4.0124	9.9881	31.321
		$\sigma_{zz}\,[10^3\ \mathrm{Pa}](\tilde{z} = 0.95h)$			
3D-u-ϕ [48]	9.3376	9.7171	9.8427	9.8884	9.8954
3D-u-ϕ-ψ	9.3376	9.7171	9.8427	9.8884	9.8954

(Continued)

Table 3 (continued)

a/h	4	10	20	50	100
		$\phi\,[\mathrm{V}](\tilde{z}=0.15h)$			
3D-u-ϕ [48]	51.426	77.653	102.79	208.25	401.46
3D-u-ϕ-ψ	51.426	77.653	102.79	208.25	401.46
		$\mathcal{D}_z\,[10^{-9}\,\mathrm{C/m^2}](\tilde{z}=0.85h)$			
3D-u-ϕ [48]	−1.1991	−0.2870	−0.0552	0.0235	0.0354
3D-u-ϕ-ψ	−1.1991	−0.2870	−0.0552	0.0235	0.0354

Table 4: Assessment A1-A, simply supported multilayered electro-elastic square plate in actuator configuration

a/h	4	10	20	50	100
		$u\,[10^{-11}\,\mathrm{m}](\tilde{z}=0.75h)$			
3D-u-ϕ [48]	6.8261	16.335	8.4438	−0.70485	−8.0823
3D-u-ϕ-ψ	6.8259	16.335	8.4438	−0.70485	−8.0823
		$w\,[10^{-9}\,\mathrm{m}](\tilde{z}=0.5h)$			
3D-u-ϕ [48]	−5.4491	−2.7851	−1.6696	−1.2583	−1.1948
3D-u-ϕ-ψ	−5.4491	−2.7851	−1.6696	−1.2583	−1.1948
		$\sigma_{xx}\,[10^{3}\,\mathrm{Pa}](\tilde{z}=0.75h)$			
3D-u-ϕ [48]	−1.9234	−0.29305	−0.09300	0.00623	0.07299
3D-u-ϕ-ψ	−1.9234	−0.29305	−0.09300	0.00623	0.07299
		$\sigma_{zz}\,[10^{-5}\,\mathrm{Pa}](\tilde{z}=0.95h)$			
3D-u-ϕ [48]	−92196	−7080.2	−887.69	−36.241	5.1601
3D-u-ϕ-ψ	−92196	−7080.2	−887.69	−36.241	5.1601
		$\phi\,[\mathrm{V}](\tilde{z}=0.15h)$			
3D-u-ϕ [48]	5.4381	6.1172	6.2215	6.2509	6.2552
3D-u-ϕ-ψ	5.4381	6.1172	6.2215	6.2509	6.2552
		$\mathcal{D}_z\,[10^{-9}\,\mathrm{C/m^2}](\tilde{z}=0.85h)$			
3D-u-ϕ [48]	−5.2884	−11.431	−22.316	−55.403	−110.70
3D-u-ϕ-ψ	−5.2884	−11.431	−22.316	−55.403	−110.70

In the second assessment (A2), a multilayered square plate is proposed in both sensor (A2-S) and actuator (A2-A) configurations. In this case, the multilayered plate lamination is $CoFe_2O_4$/Al2024/Foam/Al2024/$CoFe_2O_4$ where $h_{CoFe_2O_4} = h_{Al2024} = 0.1h$ and $h_{Foam} = 0.6h$ where h is the total thickness of the plate. Geometrical data and load conditions are listed in Table 1. Material properties in terms of magnetic, electric, and mechanical coefficients are detailed in Table 2. The reference solution for both configurations is the 3D-u-ψ magneto-elastic model in [49]. Tables 5 and 6 show results in terms of displacements v and w, stresses σ_{xx} and σ_{zz}, magnetic potential ψ and magnetic induction $\mathcal{B}_z$ for different thickness locations. A perfect agreement between the 3D-u-ψ-ϕ model and the reference solution is possible to observe for each proposed variable and thickness ratio. Even in A2-S and A2-A cases, the perfect match involves primary variables (v, w, ψ) and secondary variables (σ_{xx}, σ_{zz}, B_z). The present assessment is useful to validate the magneto-elastic coupling and the thickness and material layer effects in multilayered piezomagnetic plates.

Table 5: Assessment A2-S, simply supported multilayered magneto-elastic square plate in sensor configuration

a/h	4	10	20	50	100
		$v\,[10^{-6}\,\mathrm{m}](\tilde{z}=0.75h)$			
3D-u-ψ [49]	0.4325	1.4974	3.0988	12.380	45.150
3D-u-ϕ-ψ	0.4325	1.4974	3.0988	12.380	45.150
		$w\,[10^{-4}\,\mathrm{m}](\tilde{z}=0.5h)$			
3D-u-ψ [49]	0.0893	0.4930	1.3875	6.6144	34.151
3D-u-ϕ-ψ	0.0893	0.4930	1.3875	6.6144	34.151
		$\sigma_{xx}\,[10^{3}\,\mathrm{Pa}](\tilde{z}=0.75h)$			
3D-u-ψ [49]	2.4439	2.9747	3.5577	7.6673	22.366
3D-u-ϕ-ψ	2.4439	2.9747	3.5577	7.6673	22.366
		$\sigma_{zz}\,[10^{3}\,\mathrm{Pa}](\tilde{z}=0.95h)$			
3D-u-ψ [49]	4.6605	5.0316	5.0109	5.0019	5.0005
3D-u-ϕ-ψ	4.6605	5.0316	5.0109	5.0019	5.0005
		$\psi\,[\mathrm{A}](\tilde{z}=0.15h)$			
3D-u-ψ [49]	−0.0285	−0.0404	−0.0549	−0.1122	−0.2167
3D-u-ϕ-ψ	−0.0285	−0.0404	−0.0549	−0.1122	−0.2167
		$\mathcal{B}_z\,[10^{-8}\,\mathrm{T}](\tilde{z}=0.85h)$			
3D-u-ψ [49]	5.7606	1.9062	1.2871	1.1143	1.0905
3D-u-ϕ-ψ	5.7606	1.9062	1.2871	1.1143	1.0905

Table 6: Assessment A2-A, simply supported multilayered magneto-elastic square plate in actuator configuration

a/h	4	10	20	50	100
		$v\,[10^{-10}\,\mathrm{m}](\tilde{z}=0.75h)$			
3D-u-ψ [49]	−11.020	−2.1426	0.6612	3.8437	8.1866
3D-u-ϕ-ψ	−11.020	−2.1426	0.6612	3.8437	8.1866
		$w\,[10^{-9}\,\mathrm{m}](\tilde{z}=0.5h)$			
3D-u-ψ [49]	−22.134	−10.247	−6.1126	−4.5503	−4.3069
3D-u-ϕ-ψ	−22.134	−10.247	−6.1126	−4.5503	−4.3069
		$\sigma_{xx}\,[\mathrm{Pa}](\tilde{z}=0.75h)$			
3D-u-ψ [49]	−7.9920	−1.3076	−0.6029	−0.5376	−0.8293
3D-u-ϕ-ψ	−7.9920	−1.3076	−0.6029	−0.5376	−0.8293
		$\sigma_{zz}\,[\mathrm{Pa}](\tilde{z}=0.95h)$			
3D-u-ψ [49]	−11.809	−0.8745	−0.1406	−0.0233	−0.0093
3D-u-ϕ-ψ	−11.809	−0.8745	−0.1406	−0.0233	−0.0093
		$\psi\,[\mathrm{A}](\tilde{z}=0.15h)$			
3D-u-ψ [49]	7.9550	8.0902	8.1116	8.1177	8.1185
3D-u-ϕ-ψ	7.9550	8.0902	8.1116	8.1177	8.1185
		$\mathcal{B}_z\,[10^{-4}\,\mathrm{T}](\tilde{z}=0.85h)$			
3D-u-ψ [49]	−0.6208	−1.5651	−3.1341	−7.8380	−15.677
3D-u-ϕ-ψ	−0.6208	−1.5651	−3.1341	−7.8380	−15.677

The third assessment (A3) is devoted to a multilayered square plate involving a piezoelectric lamina $BaTiO_3$ and a magnetostrictive lamina $CoFe_2O_4$. The first assessed stacking sequence is $BaTiO_3/CoFe_2O_4/BaTiO_3$ and the second one is $CoFe_2O_4/BaTiO_3/CoFe_2O_4$ in sensor configuration (A3-S). For both cases, each lamina of the multilayered plate is $0.1m$ thick. Geometrical data and load boundary conditions are explicitly written in Table 1, while the material properties of the two constituents are listed in Table 2. The reference solution adopted is the 3D magneto-electro-elastic plate model by Pan [42]. Tabular results with four significant digits listed in Tables 7 and 8 were derived from graphical trends proposed in the work [42]. Comparisons for this assessment are presented for ϕ, ψ, $\mathcal{D}_x$, $\mathcal{D}_z$, $\mathcal{B}_x$, $\mathcal{B}_z$ and σ_{zz} variables for both $BaTiO_3/CoFe_2O_4/BaTiO_3$ and $CoFe_2O_4/BaTiO_3/CoFe_2O_4$ layered configurations. Tables 7 and 8 exhibit a good match for both stacking sequences between 3D-u-ϕ-ψ model results and the reference ones. Differences in the last digit probably arise from converting in tabular form the results from a graphical trend. Both primary (ϕ, ψ) and secondary ($\mathcal{D}_x$, $\mathcal{D}_z$, $\mathcal{B}_x$, $\mathcal{B}_z$ and σ_{zz}) variables are in accordance with the reference results. This assessment is useful to validate the present 3D-u-ϕ-ψ model with a completely different 3D magneto-electro-elastic multilayered plate theory and to validate the fully coupled magneto-electro-elastic effect.

Table 7: Assessment A3-S, simply supported multilayered ($BaTiO_3/CoFe_2O_4/BaTiO_3$) magneto-electro-elastic square plate in sensor configuration

$\phi[10^{-3}\,\mathrm{V}]\ (\tilde{z}=0.5h)$	
3D [42]	1.413
3D-u-ϕ-ψ	1.416
$\psi\,[10^{-6}\,\mathrm{A}]\ (\tilde{z}=\frac{5}{6}h)$	
3D [42]	−2.215
3D-u-ϕ-ψ	−2.221
$\mathcal{D}_x\,[10^{-11}\,\mathrm{C/m^2}]\ (\tilde{z}=0)$	
3D [42]	3.500
3D-u-ϕ-ψ	3.526
$\mathcal{D}_z\,[10^{-12}\,\mathrm{C/m^2}]\ (\tilde{z}=\frac{1}{6}h)$	
3D [42]	−4.400
3D-u-ϕ-ψ	−4.414
$\mathcal{B}_x\,[10^{-9}\,\mathrm{T}]\ (\tilde{z}=h)$	
3D [42]	−0.038
3D-u-ϕ-ψ	−0.035
$\mathcal{B}_z\,[10^{-10}\,\mathrm{T}]\ (\tilde{z}=\frac{5}{6}h)$	
3D [42]	−0.100
3D-u-ϕ-ψ	−0.109
$\sigma_{zz}\,[\mathrm{Pa}]\ (\tilde{z}=0.5h)$	
3D [42]	0.2499
3D-u-ϕ-ψ	0.2499

Table 8: Assessment A3-S, simply supported multilayered ($CoFe_2O_4/BaTiO_3/CoFe_2O_4$) magneto-electro-elastic square plate in sensor configuration

$\phi[10^{-3}\,\mathrm{V}]\ (\tilde{z} = 0.5h)$	
3D [42]	2.243
3D-u-ϕ-ψ	2.246
$\psi\,[10^{-6}\,\mathrm{A}]\ (\tilde{z} = \frac{5}{6}h)$	
3D [42]	−1.490
3D-u-ϕ-ψ	−1.496
$\mathcal{D}_x\,[10^{-11}\,\mathrm{C/m^2}]\ (\tilde{z} = 0)$	
3D [42]	0.050
3D-u-ϕ-ψ	0.048
$\mathcal{D}_z\,[10^{-12}\,\mathrm{C/m^2}]\ (\tilde{z} = \frac{1}{6}h)$	
3D [42]	−0.150
3D-u-ϕ-ψ	−0.152
$\mathcal{B}_x\,[10^{-9}\,\mathrm{T}]\ (\tilde{z} = h)$	
3D [42]	1.600
3D-u-ϕ-ψ	1.585
$\mathcal{B}_z\,[10^{-10}\,\mathrm{T}]\ (\tilde{z} = \frac{5}{6}h)$	
3D [42]	2.175
3D-u-ϕ-ψ	2.171
$\sigma_{zz}\,[\mathrm{Pa}]\ (\tilde{z} = 0.5h)$	
3D [42]	0.246
3D-u-ϕ-ψ	0.247

4.2 Benchmarks

This section proposes a new multilayered square plate in both sensor and actuator configurations to evaluate the magneto-electro-elastic coupling effects. The magneto-elastic effects and the electro-elastic effects have already been investigated separately in the assessment part to validate the model. Eight different values for specific $\tilde{z}/h$ locations are presented for variables w, ϕ, ψ, σ_{xx}, σ_{yy}, σ_{zz}, $\mathcal{D}_z$, and $\mathcal{B}_z$ in tabular forms. z goes from $-h/2$ to $+h/2$ and $\tilde{z}$ goes from 0 to h. Each variable is proposed for different thickness ratios, from thick ($a/h = 4$) to thin ($a/h = 100$) structures. The same eight variables are also presented in graphical forms along the thickness direction for a moderately thick plate ($a/h = 10$).

This new benchmark considers two different load boundary conditions: sensor configuration (B-S) and the actuator configuration (B-A). From bottom to top, the lamination scheme is Adaptive Wood/0°/90°/0°/Adaptive Wood. Each layer is $h_{Adaptive\ Wood} = 0.05h$ e $h_{Composite} = 0.3h$. h is the total thickness. Geometrical and load conditions are listed in Table 1, and material properties are collected in Table 2. Since in the literature the sign of the magnetic permittivity coefficients μ_1 and μ_2 are stated as both negative [51] and positive [52], this benchmark is duplicated by considering the two possibilities. So, B-S and B-A are proposed with both $\mu_1 = \mu_2 = -590 \cdot 10^3$ nH/m and $\mu_1 = \mu_2 = 590 \cdot 10^3$ nH/m. In Tables 9–12, variables w, ϕ, ψ, σ_{xx}, σ_{yy}, σ_{zz}, $\mathcal{D}_z$ and $\mathcal{B}_z$ are proposed at different $\tilde{z}/h$ thickness positions and for different a/h thickness ratios for both sensor and actuator cases. Tables 9 and 11 indicate the effect of the sign on permittivity coefficients μ_1 and μ_2 for the sensor case: slight differences in results onto the electric and magnetic variables (ϕ, $\mathcal{D}_z$, ψ and $\mathcal{B}_z$) are present. Tables 10 and 12 demonstrate that greater differences

in all the proposed variables occur in both thick and thin plates for the actuator configuration due to the different signs of the permittivity coefficients μ_1 and μ_2. Figs. 2 and 3 depict trends along the thickness direction of the proposed tabular variables, considering negative μ_1 and μ_2 for the sensor and actuator case, respectively. Figs. 4 and 5 indicate that the same trends are reported considering positive magnetic permittivity coefficients. Both sensor and actuator configurations exhibit that the correct imposition of the load boundary conditions (for the sensor case, $\sigma_{zzt} = P_{z_t} = 10000$ Pa and $\sigma_{zzb} = P_{z_b} = 0$ Pa, $\phi_t = \phi_b = 0$ V, $\psi_t = \psi_b = 0$ A; for the actuator case, $\sigma_{zzt} = \sigma_{zzb} = P_{z_t} = P_{z_b} = 0$ Pa, $\phi_t = 10$ V and $\phi_b = 0$ V, $\psi_t = 15$ A and $\psi_b = 0$ A). In addition, it is clear the perfect depiction of the magneto-electro-elastic coupling for both sensor and actuator cases: in B-S case, the presence of a transverse normal load at the top surface creates a ϕ electric potential and a ψ magnetic potential in the thickness of the plate, in the B-A case, the ϕ electric potential trend and the ψ magnetic potential trend in the thickness of the plate generates a σ_{zz} non-zero trend along the thickness direction. For each presented variable, the zigzag effect is shown as a multilayered structure is analyzed. The zigzag effect is apparent for both configurations as the slope drastically changes in correspondence with the physical interfaces of the plate. For variables w, ϕ, ψ, σ_{zz}, $\mathcal{D}_z$, and $\mathcal{B}_z$ trends are continuous along the thickness direction owning to the correct imposition of interlaminar continuity conditions at each interface between two adjacent k layers. For variables σ_{xx} and σ_{yy}, trends are discontinuous as no interlaminar continuity conditions are imposed. For the sensor configuration, the sign of the magnetic permittivity coefficients μ_1 and μ_2 only affects the $\mathcal{B}_z$ trend (Figs. 2 and 4). In the case of the actuator configuration, different trends are due to the different signs of the magnetic permittivity regarding the w displacement, the σ_{xx} and σ_{yy} stresses and the $\mathcal{B}_z$ transverse magnetic induction (Figs. 3 and 5). The sign of μ_1 and μ_2 coefficients does not affect any of the previously described peculiarities related to the model (load boundary conditions, magneto-electro-elastic coupling effect, zigzag effect and interlaminar continuity conditions).

Table 9: B-S, simply supported multilayered electro-magneto-elastic square plate in sensor configuration. $\mu_1 = -590 \cdot 10^3$ nH/m, $\mu_2 = -590 \cdot 10^3$ nH/m. Results obtained via the new 3D-u-ϕ-ψ model

a/h	4	10	20	50	100
		$w\,[10^{-6}\,\mathrm{m}](\tilde{z} = 0.5h)$			
	1.1408	4.9505	23.567	295.98	2284.5
		$\phi\,[10^{1}\,\mathrm{V}](\tilde{z} = 0.75h)$			
	5.0115	12.996	25.496	63.095	125.97
		$\psi\,[10^{-2}\mathrm{A}](\tilde{z} = 0.25h)$			
	−2.0197	−4.9894	−9.6587	−23.794	−47.475
		$\sigma_{xx}\,[10^{5}\,\mathrm{Pa}](\tilde{z} = h)$			
	1.8042	7.7687	28.840	176.03	701.62
		$\sigma_{yy}\,[10^{5}\,\mathrm{Pa}](\tilde{z} = 0)$			
	−1.5823	−7.9167	−29.160	−176.41	−702.02
		$\sigma_{zz}\,[10^{3}\,\mathrm{Pa}](\tilde{z} = 0.5h)$			
	4.9271	5.0065	5.0031	5.0006	5.0001
		$\mathcal{D}_z\,[10^{-10}\,\mathrm{C/m^2}](\tilde{z} = 0.5h)$			
	1.6460	3.4245	3.9899	4.1837	4.2130
		$\mathcal{B}_z\,[10^{-9}\,\mathrm{T}](\tilde{z} = 0.5h)$			
	4.5506	−4.4506	−7.4005	−8.4166	−8.5691

Table 10: B-A, simply supported multilayered electro-magneto-elastic square plate in actuator configuration. $\mu_1 = -590 \cdot 10^3$ nH/m, $\mu_2 = -590 \cdot 10^3$ nH/m. Results obtained via the new 3D-u-ϕ-ψ model

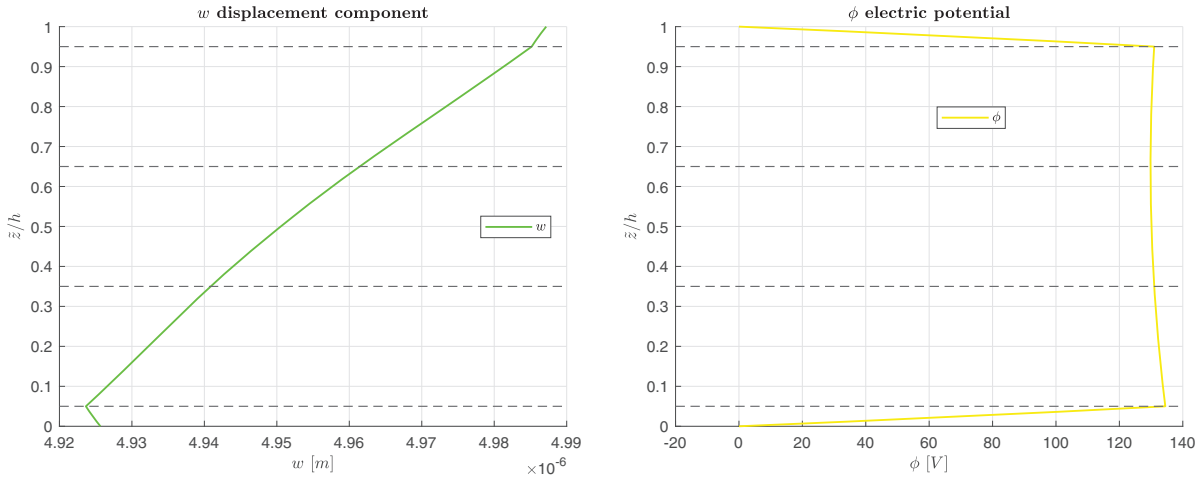
a/h	4	10	20	50	100
		$w\,[10^{-10}\,\mathrm{m}](\tilde{z} = 0.5h)$			
	−3.9516	−3.4755	−3.3060	−3.2417	−3.2317
		$\phi\,[\mathrm{V}](\tilde{z} = 0.75h)$			
	5.7736	7.5134	7.7774	7.8520	7.8627
		$\psi\,[\mathrm{A}](\tilde{z} = 0.25h)$			
	2.8789	3.2568	3.3167	3.3338	3.3362
		$\sigma_{xx}\,[10^2\,\mathrm{Pa}](\tilde{z} = h)$			
	−16.743	−1.8880	7.6162	27.030	56.344
		$\sigma_{yy}\,[10^2\,\mathrm{Pa}](\tilde{z} = 0)$			
	1.5251	4.7650	10.328	26.558	53.345
		$\sigma_{zz}\,[10^{-1}\,\mathrm{Pa}](\tilde{z} = 0.5h)$			
	−25.418	−12.087	−6.4263	−2.6252	−1.3168
		$\mathcal{D}_z\,[10^{-10}\,\mathrm{C/m^2}](\tilde{z} = 0.5h)$			
	−3.0421	−9.7255	−20.088	−50.670	−101.47
		$\mathcal{B}_z\,[10^{-5}\,\mathrm{T}](\tilde{z} = 0.5h)$			
	−8.0769	−20.805	−41.791	−104.60	−209.24

Table 11: B-S, simply supported multilayered electro-magneto-elastic square plate in sensor configuration. $\mu_1 = 590 \cdot 10^3$ nH/m, $\mu_2 = 590 \cdot 10^3$ nH/m. Results obtained via the new 3D-u-ϕ-ψ model

a/h	4	10	20	50	100
		$w\,[10^{-6}\,\mathrm{m}](\tilde{z} = 0.5h)$			
3D-u-ϕ-ψ	1.1408	4.9506	23.567	295.98	2284.5
		$\phi\,[10^{1}\,\mathrm{V}](\tilde{z} = 0.75h)$			
3D-u-ϕ-ψ	5.0113	12.996	25.496	63.095	125.97
		$\psi\,[10^{-2}\,\mathrm{A}](\tilde{z} = 0.25h)$			
3D-u-ϕ-ψ	−2.0029	−4.9832	−9.6557	−23.793	−47.474
		$\sigma_{xx}\,[10^{5}\,\mathrm{Pa}](\tilde{z} = h)$			
3D-u-ϕ-ψ	1.8041	7.7686	28.840	176.03	701.62
		$\sigma_{yy}\,[10^{5}\,\mathrm{Pa}](\tilde{z} = 0)$			
3D-u-ϕ-ψ	−1.5822	−7.9166	−29.160	−176.41	−702.02
		$\sigma_{zz}\,[10^{3}\,\mathrm{Pa}](\tilde{z} = 0.5h)$			
3D-u-ϕ-ψ	4.9271	5.0065	5.0031	5.0006	5.0001
		$\mathcal{D}_z\,[10^{-10}\,\mathrm{C/m^2}](\tilde{z} = 0.5h)$			
3D-u-ϕ-ψ	1.6461	3.4245	3.9899	4.1837	4.2130
		$\mathcal{B}_z\,[10^{-9}\,\mathrm{T}](\tilde{z} = 0.5h)$			
3D-u-ϕ-ψ	4.5063	−4.4453	−7.3982	−8.4161	−8.5689

Table 12: B-A, simply supported multilayered electro-magneto-elastic square plate in sensor configuration. $\mu_1 = 590 \cdot 10^3$ nH/m, $\mu_2 = 590 \cdot 10^3$ nH/m. Results obtained via the new 3D-u-ϕ-ψ model

a/h	4	10	20	50	100
		$w\,[10^{-9}\ \mathrm{m}](\tilde{z} = 0.5h)$			
3D-u-ϕ-ψ	−5.8195	−4.9277	−4.6583	−4.5594	−4.5441
		$\phi\,[\mathrm{V}](\tilde{z} = 0.75h)$			
3D-u-ϕ-ψ	7.8864	7.9198	7.8849	7.8696	7.8671
		$\psi\,[\mathrm{A}](\tilde{z} = 0.25h)$			
3D-u-ϕ-ψ	2.8461	3.2509	3.3152	3.3335	3.3361
		$\sigma_{xx}\,[10^3\ \mathrm{Pa}](\tilde{z} = h)$			
3D-u-ϕ-ψ	11.493	5.4200	3.6225	3.8554	6.2112
		$\sigma_{yy}\,[10^2\ \mathrm{Pa}](\tilde{z} = 0)$			
3D-u-ϕ-ψ	8.4150	9.1190	12.674	27.511	53.822
		$\sigma_{zz}\,[10^{-1}\ \mathrm{Pa}](\tilde{z} = 0.5h)$			
3D-u-ϕ-ψ	−221.29	−35.942	−9.8989	−2.8584	−1.3461
		$\mathcal{D}_z\,[10^{-10}\ \mathrm{C/m^2}](\tilde{z} = 0.5h)$			
3D-u-ϕ-ψ	−4.2523	−10.333	−20.411	−50.802	−101.54
		$\mathcal{B}_z\,[10^{-5}\ \mathrm{T}](\tilde{z} = 0.5h)$			
3D-u-ϕ-ψ	−7.9845	−20.767	−41.771	−104.60	−209.24



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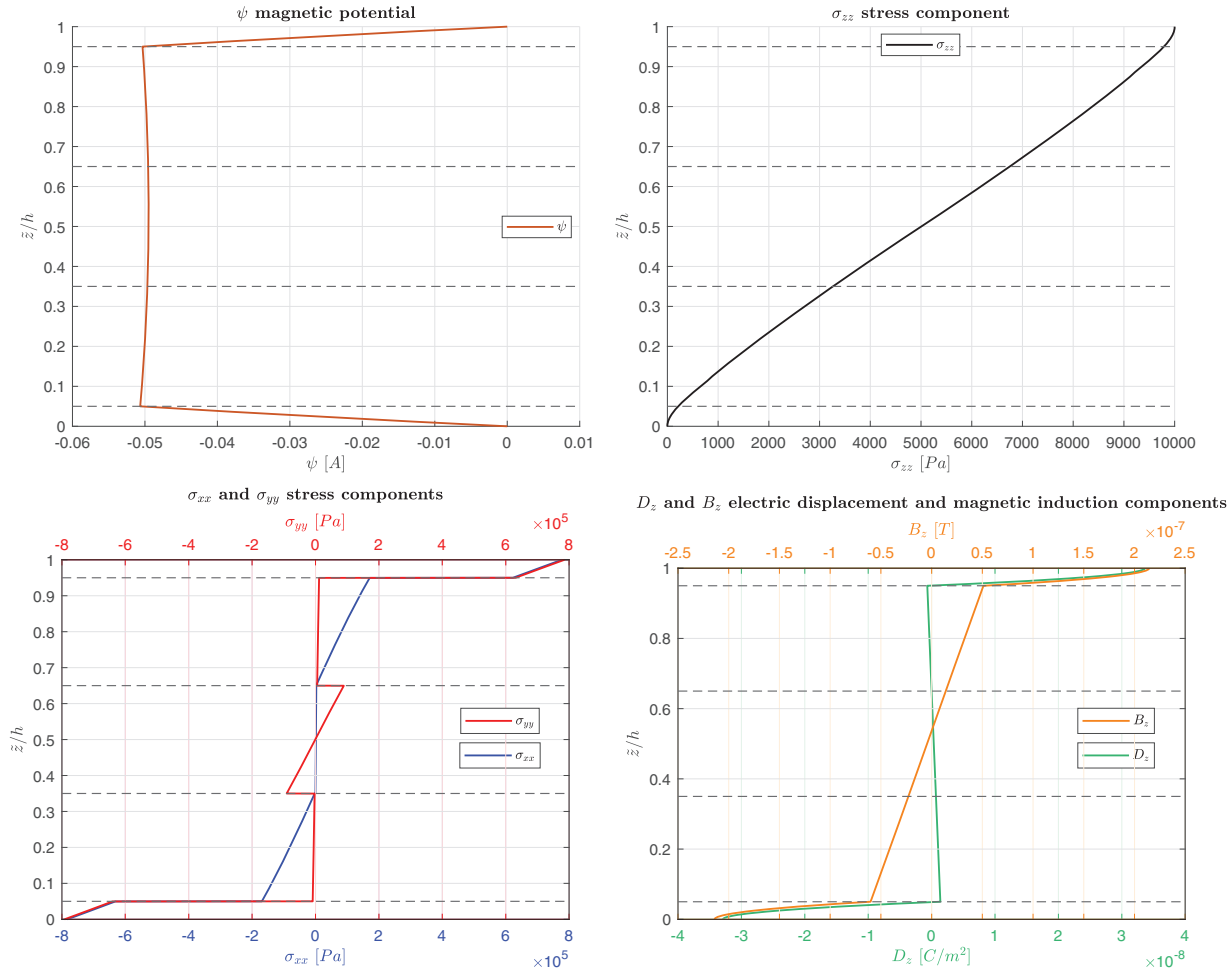
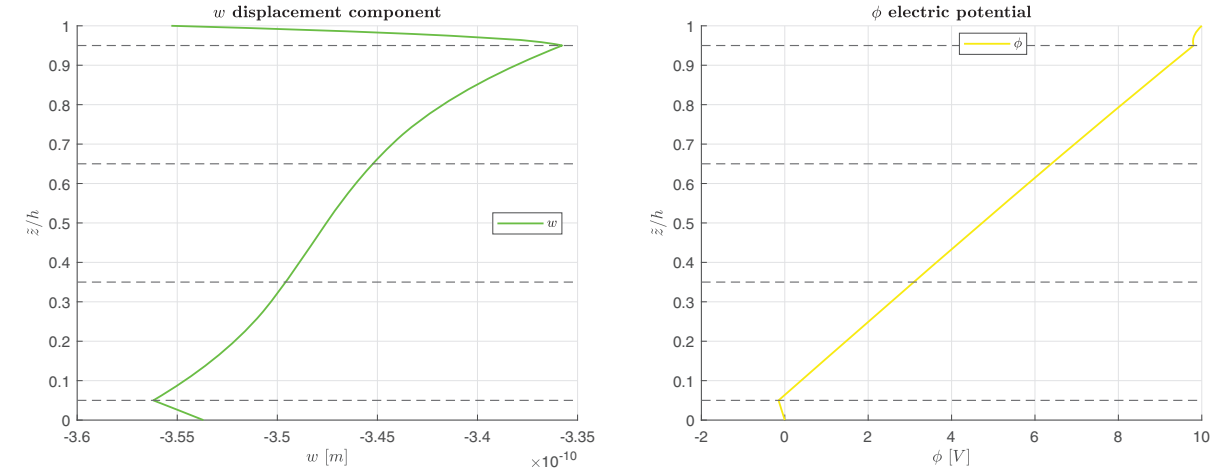


Figure 2: B-S, simply-supported multilayered electro-magneto-elastic square plate in sensor configuration. $\mu_1 = -590 \cdot 10^3$ nH/m, $\mu_2 = -590 \cdot 10^3$ nH/m. Results obtained via the new 3D-u-ϕ-ψ model for thickness ratio $a/h = 10$



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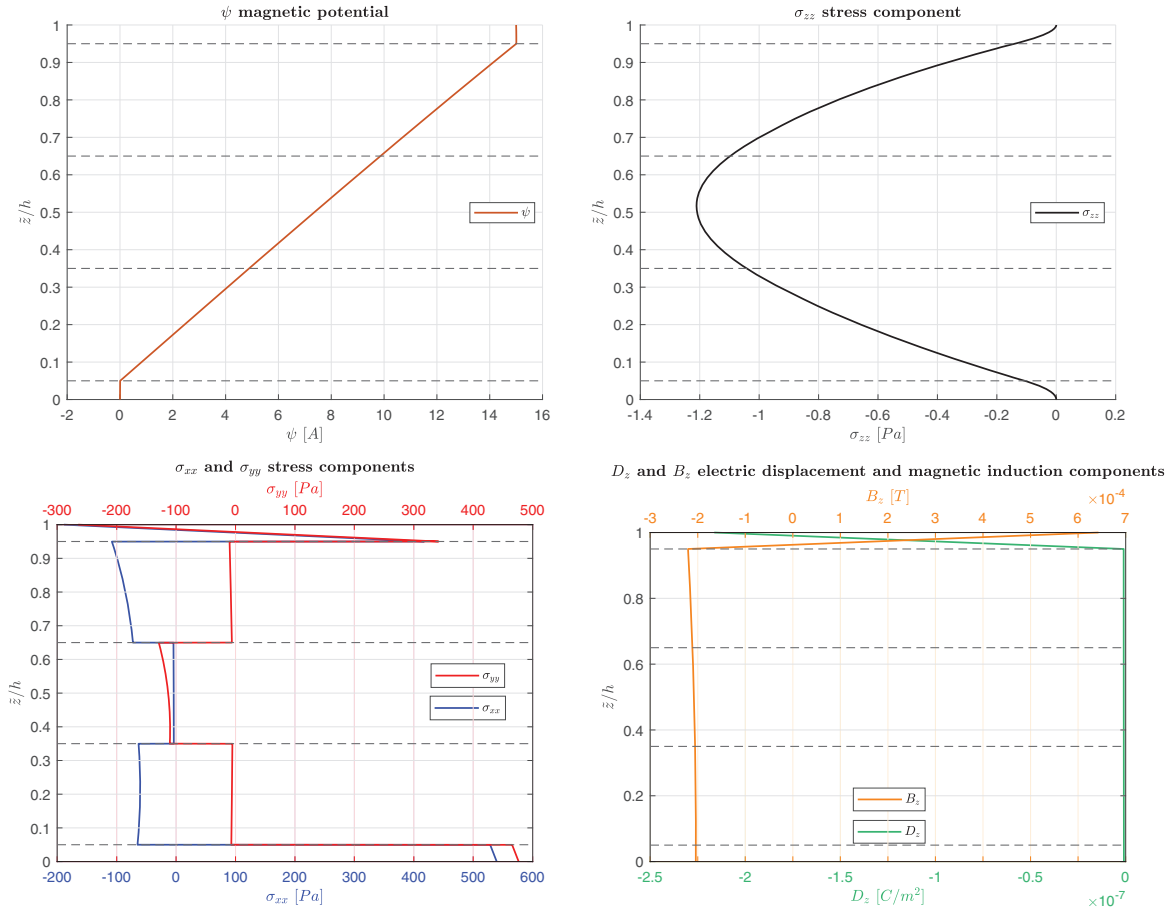
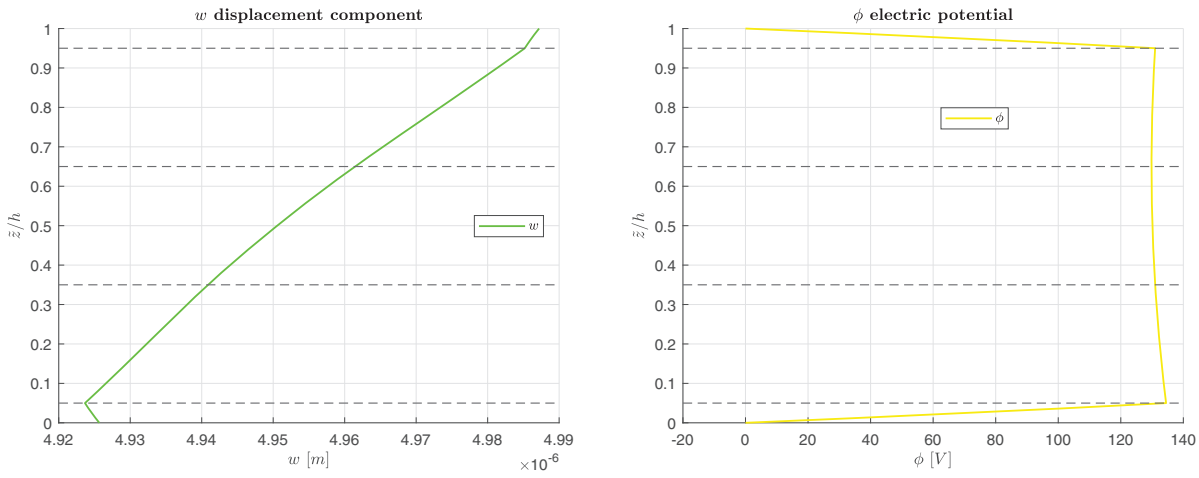


Figure 3: B-A, simply-supported multilayered electro-magneto-elastic square plate in actuator configuration. $\mu_1 = -590 \cdot 10^3$ nH/m, $\mu_2 = -590 \cdot 10^3$ nH/m. Results obtained via the new 3D-u-ϕ-ψ model for thickness ratio $a/h = 10$



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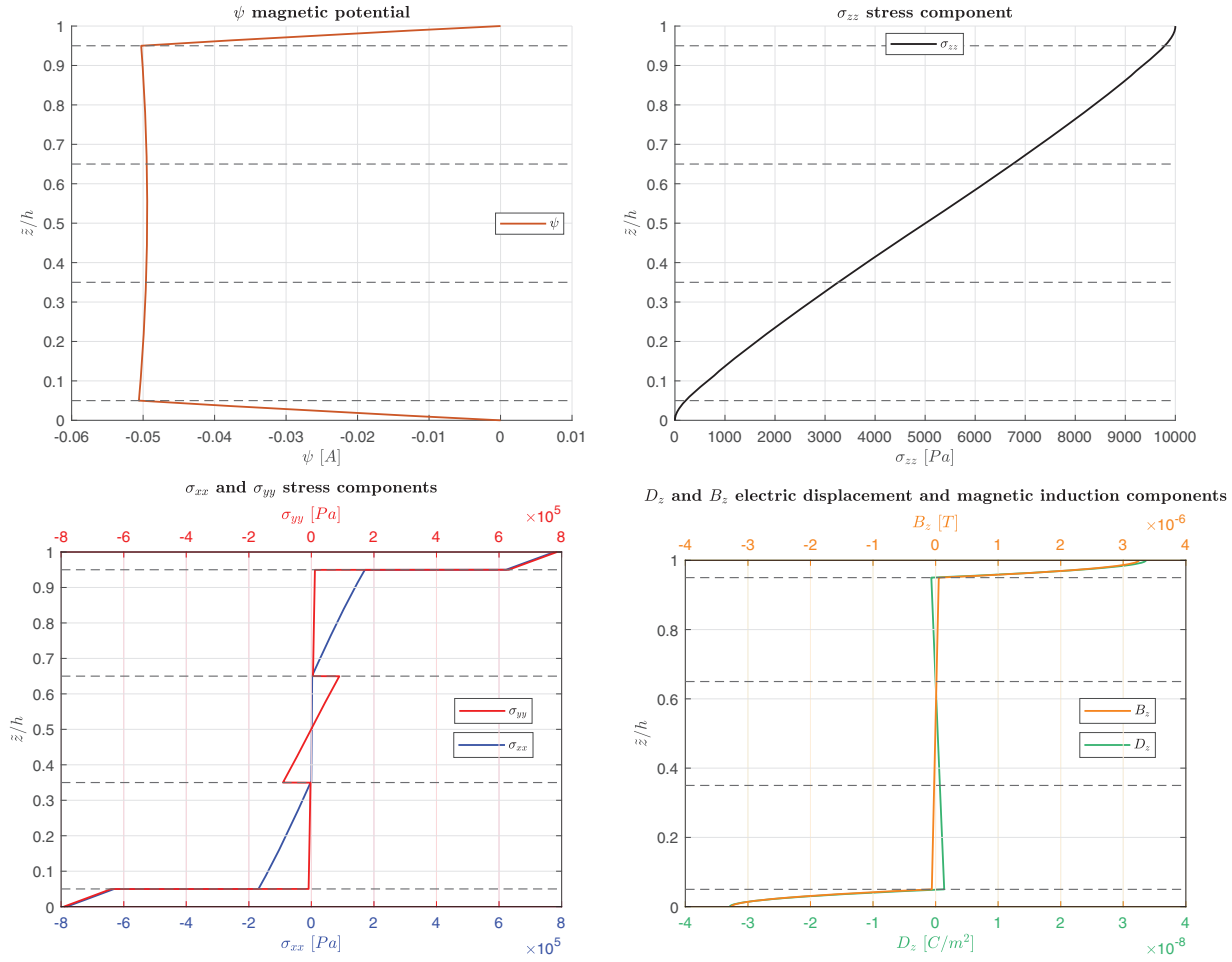
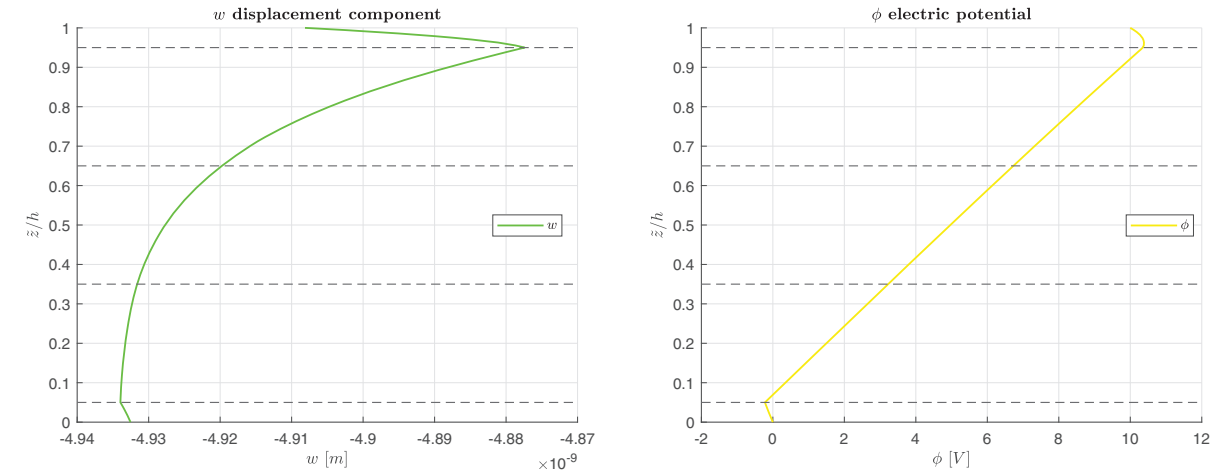


Figure 4: B-S, simply-supported multilayered electro-magneto-elastic square plate in sensor configuration. $\mu_1 = 590 \cdot 10^3$ nH/m, $\mu_2 = 590 \cdot 10^3$ nH/m. Results obtained via the new 3D-u-ϕ-ψ model for thickness ratio $a/h = 10$



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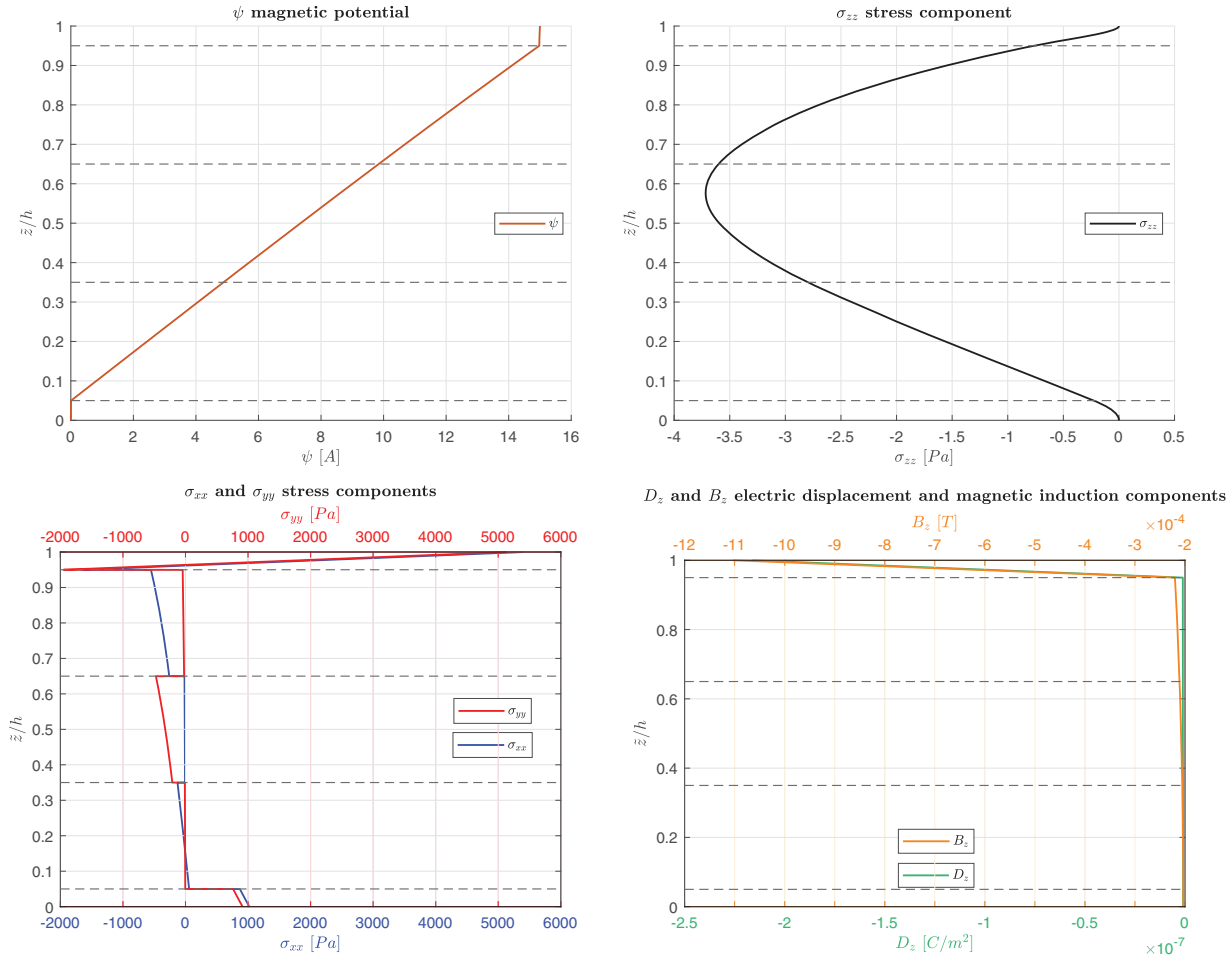

Figure 5: B-A, simply-supported multilayered electro-magneto-elastic square plate in actuator configuration. $\mu_1 = 590 \cdot 10^3$ nH/m, $\mu_2 = 590 \cdot 10^3$ nH/m. Results obtained via the new 3D-u-ϕ-ψ model for thickness ratio $a/h = 10$

5 Conclusions

This study proposes an exact 3D, fully coupled magneto-electro-elastic model for multilayered plates where the three 3D equilibrium equations, the 3D divergence equation for magnetic induction, and the 3D divergence equation for electric induction are the 3D governing equation of the magneto-electro-elastic model. Solution methodology considers Navier harmonic forms in the in-plane directions and the exponential matrix method in the thickness direction. A closed form solution is performed, and only simply supported boundary conditions are possible. In addition, only orthotropic laminae involving piezoelectric and/or piezomagnetic characteristics can be considered. Due to the imposition of the interlaminar continuity conditions between two adjacent layers, the layerwise approach is adopted. In the assessment subsection, the present model is validated with other 3D plate models involving magneto-elastic or electro-elastic effects in a separate way. In the second part, new results are presented in sensor and actuator configurations for different thickness ratios in the case of full coupling between electric, magnetic, and elastic fields. The benchmark case is proposed firstly considering both coefficients with a positive sign and then with a negative sign, to overcome the literature misunderstanding about the proper sign of the magnetic permittivity coefficients μ_1 and μ_2. The present 3D magneto-electro-elastic model correctly depicts the magneto-electro-elastic coupling, the thickness and material layer effects and the load conditions for all thickness ratios considered.

Load boundary conditions are correctly implemented for both sensor and actuator configurations. The present 3D magneto-electro-elastic model can be utilized to understand the behavior of smart multilayered plates embedding piezoelectric and piezomagnetic materials.

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Ethics Approval: Not applicable.

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