

Infrared Thermography for Real-Time Assessment of the Effectiveness of Scoliosis Braces

Original

Infrared Thermography for Real-Time Assessment of the Effectiveness of Scoliosis Braces / Angrisani, Leopoldo; De Benedetto, Egidio; Duraccio, Luigi; Lo Regio, Fabrizio; Ruggiero, Roberto; Tedesco, Annarita. - In: SENSORS. - ISSN 1424-8220. - ELETTRONICO. - 23:19(2023). [10.3390/s23198037]

Availability:

This version is available at: 11583/2982504 since: 2023-09-27T07:25:11Z

Publisher:

MDPI

Published

DOI:10.3390/s23198037

Terms of use:

This article is made available under terms and conditions as specified in the corresponding bibliographic description in the repository

Publisher copyright

(Article begins on next page)

Infrared Thermography for Real-Time Assessment of the Effectiveness of Scoliosis Braces

Leopoldo Angrisani ¹ , Egidio De Benedetto ^{1*} , Luigi Duraccio ² , Fabrizio Lo Regio ¹ , Roberto Ruggiero ³ and Annarita Tedesco ⁴ 

¹ Department of Electrical Engineering and Information Technology - University of Naples Federico II, Naples, Italy

² Department of Electronics and Telecommunications - Polytechnic University of Turin, Turin, Italy

³ Ortopedia Ruggiero SRL, Cardito, Naples, Italy

⁴ Department of Chemistry, University of Naples Federico II, Naples, Italy

* Correspondence: egidio.debenedetto@unina.it (E.D.B.)

Abstract: This work proposes an innovative method, based on the use of low-cost infrared thermography (IRT) instrumentation, to assess in real time the effectiveness of scoliosis braces.

Establishing the effectiveness of scoliosis braces means to decide whether the pressure exerted by the brace on the patient's back is adequate for the intended therapeutic purpose. Traditionally, the evaluation of brace effectiveness relies on empirical, qualitative assessments carried out by orthopedists during routine follow-up examinations. Hence, it heavily depends on the expertise of the orthopedists involved. At the state of the art, the only objective methods to confirm the orthopedists' opinion are based on the evaluation of how scoliosis progresses over time, often exposing people to ionizing radiations. To overcome these limitations, the method proposed in this work aims to provide a real-time, objective assessment of the effectiveness of scoliosis braces in a non-harmful way. This is achieved by exploiting the thermoelastic effect and correlating temperature changes on the patients' backs due to the mechanical pressure exerted by the braces. A system based on this method was implemented and validated through an experimental study on 21 patients conducted at an accredited orthopedic center. The experimental results demonstrate a classification accuracy slightly below 70% in discriminating *adequate* from *inadequate* pressure, which is an encouraging result for further advancement in view of clinical use of such systems in orthopedic centers.

Keywords: Health 4.0; Biomedical applications; Instrumentation; Real-time measurements; Real-time Monitoring; Scoliosis Braces; Infrared Thermal Imaging

Citation: Angrisani, L.; De Benedetto, E.; Duraccio, L.; Lo Regio, F.; Ruggiero, R.; Tedesco, Annarita. Infrared Thermography for Real-Time Assessment of the Effectiveness of Scoliosis Braces. *Sensors* **2023**, *1*, 0. <https://doi.org/>

Received:

Revised:

Accepted:

Published:

Copyright: © 2023 by the authors. Submitted to *Sensors* for possible open access publication under the terms and conditions of the Creative Commons Attribution (CC BY) license (<https://creativecommons.org/licenses/by/4.0/>).

1. Introduction

Scoliosis is defined as a complex deformity of the backbone and the torso that occurs in three dimensions [1,2] and consists of a lateral curvature with a vertebral rotation [3]. The standard screening test for scoliosis is the forward bending test [3], during which the patient is asked to bend forward with straight knees, while the examiner observes the back for any signs of asymmetry. If the results of the test, along with the patient's medical history, raise suspicion of scoliosis, radiography becomes crucial for further evaluation [4]. Once radiography is acquired, scoliosis is identified by means of the measurement of the Cobb angle, which quantifies the degree of spinal curvature by measuring the angle between the two most inclined vertebrae at the top and at the bottom of the curve [5,6]. In particular, scoliosis is diagnosed when this angle exceeds 10° [7]. Among the different types of scoliosis, idiopathic scoliosis represents the majority of cases since it is identified as a multi-factor spinal deformity with unknown etiology [8]. In addition to the significant cosmetic deformity, idiopathic scoliosis poses risks including cardiac and pulmonary impairments [9]. Based on the patient's age, scoliosis is categorized as infantile (0-3 years), juvenile (4-10 years), and adolescent (older than 10 years) [3]. Other classification systems consider the number of curves and the type of deformity [10].

With regards to the treatments, they include various approaches such as observation, physiotherapy, bracing, and, in extreme cases, surgery [11]. While surgery is needed for Cobb angles greater than 50° [12], scoliosis braces represent the most widely adopted treatment for patients with incomplete bone growth and Cobb angles ranging between 25° and 50° [4,12]. In this particular scenario, patients wear a rigid or semi-rigid corset-like device, whose model differs in *Milwaukee*, *Lyonnaise*, *Cheneau*, *Sforzesco*, *Boston*, and others [4], based on the patient's bone maturity, Cobb angle, and backbone deformation [4]. The design of this corset is tailored to suit the individual patient's torso, considering the asymmetry caused by scoliosis, while the primary objective is to realign the patient and correct the curvature of the backbone. To achieve this, the corset applies external pressure specifically to the regions of the backbone that are affected by the curvature.

During the treatment, regular follow-up examinations are necessary to evaluate brace compliance and adjust the corset according to the changes in the patient's body [13], ensuring proper pressure application. However, currently, there is no consensus in the literature on the implementation of these brace corrections [12], as well as there is a lack of agreement on the mechanical principles of brace design and manufacturing [8,14]. As a result, the evaluation of the effectiveness of the brace, that means deciding whether the pressure exerted by the brace is considered *adequate* or *inadequate*, relies entirely on the expertise of the orthopedist [2,15]. Hence, the more reliable measure to confirm the orthopedist's opinion is the assessment of curve progression, typically achieved by comparing the Cobb angle measured through radiographic images taken over a specific period of time [16]. As it can be deduced, this approach requires a certain time interval between two measurements of the Cobb angle. In addition, when using radiographic imaging, the potential risks associated with ionizing radiation exposure constitute a limitation for repeated acquisitions over time. If alternative radiation-free methods, such as Moiré topography [17] or 3D scanning [18], are employed to assess the curve progression and evaluate the effectiveness of the brace, the time horizon between two acquisitions could be considerably shortened. Nevertheless, immediate evaluation remains not feasible, as the gradual reduction of spinal curvature can be achieved only with the prolonged wearing of the brace by the patient. Moreover, another crucial aspect is that failure to wear the corset correctly by the patients could result in a deterioration of scoliosis, even if the corset has been properly designed. Therefore, a comparison between two measurements over time may not accurately reflect the effectiveness of the corset if it is not consistently and correctly worn as prescribed. Consequently, orthopedists still currently lack an objective means of monitoring the effectiveness of corsets in real-time, which would enable prompt adjustments to be made. A first attempt for enabling real-time evaluation was introduced in [10], where the considered technique involved the monitoring of the mechanical pressure exerted by the brace by using pressure sensors positioned between the brace and the patient's backbone. Nevertheless, measuring the pressure between these two surfaces, while consistently moving the sensor, without compromising the accuracy of the measurement, proved to be a challenging task. Therefore, ensuring reliability, repeatability, and cost-effectiveness for widespread implementation in healthcare facilities posed additional complexities.

Starting from these considerations, this study presents an innovative, non-invasive, and cost-effective approach to evaluate the effectiveness of scoliosis braces in real-time. The proposed method utilizes low-cost infrared thermography (IRT) instrumentation to acquire the skin temperature of the patients' backs, right after removing the braces.

By processing the acquired temperature data, the developed system is able to determine whether the mechanical pressure applied by the corset was *adequate* or *inadequate* according to the orthopedic prescription and design of the brace. In practical application, this method can provide orthopedists with a reliable and objective assessment, allowing them to promptly identify the need for adjustments to the corset and enhance the scoliosis treatment process. This could represent a possible alternative to reduce the prescription of x-rays.

The paper is organized as follows. Section 2 provides a background on IRT technology, with a focus on relevant application scenarios in healthcare. Therefore, Section 3 describes the proposed method in detail. The experimental validation is reported in Section 4, along with the obtained results. Finally, conclusions are drawn and future works are outlined.

2. Background

IRT is a non-invasive technology that relies on the detection and registration of emitted radiation energy at wavelengths ranging from 2 to 15 μm [19]. This is achieved through an array of detectors that convert the energy E into a thermal image [20], which displays the temperature T of the observed objects as per the Stefan-Boltzmann law $E = \varepsilon \sigma T^4$, where ε represents the emissivity of the objects, which is defined as the ratio between the amount of infrared energy emitted by the object and that emitted by an ideal black body at the same wavelength and temperature [21], and σ is the Stefan-Boltzmann constant.

The amount of energy emitted by an object is influenced by multiple factors, not only including emissivity but also wavelength and surface temperature. As emissivity values vary among different objects, they can emit the same amount of thermal energy even though at different temperatures. Moreover, when utilizing infrared detectors to measure the infrared energy emitted by a specific object, the measured value may not solely reflect the energy emitted by the object itself. As a matter of fact, it is also influenced by the energy absorbed, reflected, and emitted by the surrounding environment [20]. In addition, the measure also depends on the distance of the surface from the camera [22].

IRT technology has experienced widespread adoption across diverse fields, including electrical engineering [23], mechanical engineering [24], agriculture [25], veterinary medicine [26], and healthcare [27]. With specific regards to the healthcare sector, this technology has made significant strides over the years, benefiting from advancements in detector sensitivity, cost reductions [22,28], and suitable integration within the broader context of the 4.0 digital transition, which leverages enabling technologies like Augmented Reality [29], Internet of Things [30], Cloud Computing [31], and Artificial Intelligence [32,33]. As a matter of fact, these advancements are resulting in the development of attached-to-smartphones infrared cameras, which offer improved portability, connectivity, and ease of use without compromising performance compared to traditional devices [34]. This paved the way for the rise of decision-support systems able to furnish healthcare professionals with fast, reliable, and objective results in diverse scenarios, including the evaluation of inflammatory processes [35,36], detection of infections, [37] diagnosis of carpal tunnel syndrome [38], monitoring of diabetes-related conditions [39], and assessment of eye diseases [40]. In the field of rehabilitation and orthopedics, these systems are used for ergonomic evaluations [41], injury prevention and assessments [42,43], scoliosis diagnosis [44,45], and brace manufacturing [46]. In Figure 1, some of the aforementioned healthcare-related scenarios are illustrated.

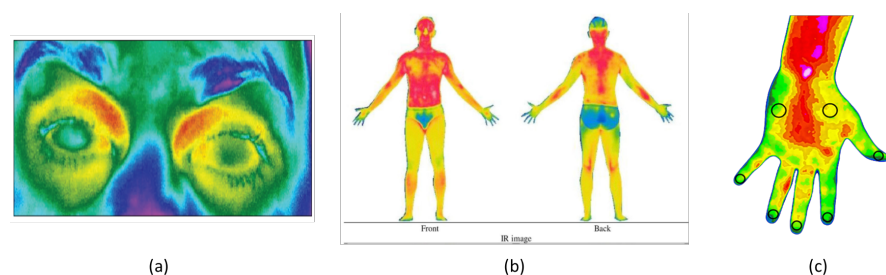


Figure 1. Examples of adoption of IRT in the framework of (a) evaluation of ocular inflammation [36], (b) ergonomics assessment [41], and (c) diagnosis of carpal tunnel syndrome [38].

All these scenarios require advanced knowledge of the relationship between the human body and the relative emitted thermal energy. Human skin has a constant emissivity in the range 3-15 μm of about 0.97 ± 0.05 , close to that of the black body [22], while the

contribution to the heat supply emitted by the human body can be mainly related to blood perfusion, metabolism, and external sources [27,47], such as electromagnetic fields, or mechanical loading [27]. In this latter case, the relationship between mechanical loading and emitted thermal energy allows to use of IRT in order to evaluate the stress imposed on a body. The involved analysis is known as Thermoelastic Stress Analysis (TSA) and is based on the thermoelastic effect, which refers to the linear correlation between changes in body temperature (and thus emitted thermal energy) and stress states on the surface of the body, assuming local adiabatic conditions [27]. More in detail, mechanical loading is related to the skin temperature variations on the patients' backs according to (1) [48]:

$$\Delta T = \frac{T}{\rho C_\epsilon} \sum \frac{\partial \sigma_{ij}}{\partial T} \epsilon_{ij} + \frac{Q}{\rho C_\epsilon} \quad (1)$$

where T is the absolute temperature of the body, C_ϵ is the specific heat at constant strain, ρ is the density, Q is the heat input, and σ_{ij} and ϵ_{ij} are respectively the stress and strain change tensors in the three dimensions, for $i, j = \{1, 2, 3\}$.

Taking all these factors into account, it becomes clear that, in the framework of the evaluation of the effectiveness of scoliosis corsets, TSA could represent a robust fundament that can be exploited to assess, by means of suitable acquisition and processing of the thermal images of patients' backs, whether the pressure applied by the corset is adequate.

3. Proposal

Based on the considerations outlined in Section 1 and Section 2, this study proposes a method that leverages the relationship between skin temperature variations and applied mechanical pressure in order to evaluate if the pressure applied by scoliosis corsets on the patients' backs is *adequate* or *inadequate*, thus facilitating orthopedists' clinical decision-making. The proposed method represents *workaround* to the problem of directly measuring the pressure exerted by the brace, which is a task associated with several difficulties, as reported in [10]. Figure 2 schematizes the pipeline of the method. This consists of three major modules, namely *Regions of Interest (ROIs) preparation*, *ROIs processing*, and *Decision*.

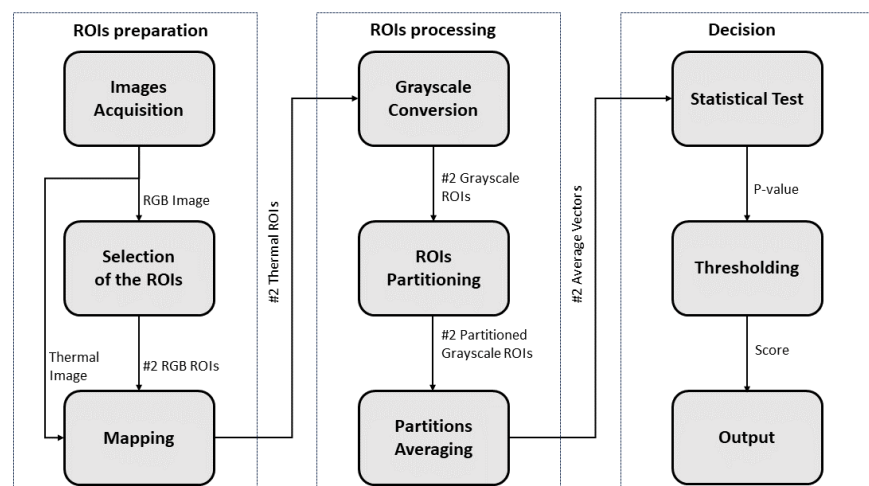


Figure 2. Conceptual description of the proposed method

1. The *ROIs preparation* module consists of three blocks. The first block, named *Images Acquisition*, captures the thermal and corresponding RGB images from the dorsum of the patients, right after removing the braces. It is noteworthy that the patient's dorsum remains uncovered during this stage. To ensure that the bracing effect remains visible, it is recommended to wait no more than one minute between the patient removing the scoliosis corset and the start of image capture. In fact, the duration of the corset's pressure effect on skin temperature

variation after its removal can be influenced by several factors, such as the duration of brace usage, the intensity of applied pressure, patients' metabolism, sweating, and ambient temperature. This effect may gradually dissipate within a few minutes or persist for an extended period, ranging from several minutes to tens of minutes [49,50]. Hence, a waiting time of less than one minute can be considered as a time to ensure adequate stability in the short term.

In the second block, referred to as the *Selection of the ROIs*, the orthopedic specialist selects on his/her computer (with the help of cursors) two ROIs from the acquired RGB image: the first ROI corresponds to the area in which the thrust is exerted by the brace, while the second ROI is selected symmetrically to the first ROI with respect to the backbone. It should be pointed out that this selection is guided by the patient's clinical history: the orthopedic specialist has access to the patient's radiography, has knowledge of the diagnosis, knows the type of corset worn, and has the related prescription. As a result, he/she possesses the necessary information to identify the specific region of the back where the corset needs to exert its effect. Nevertheless, to avoid confirmation bias, the selection of the ROIs is not performed directly on the thermal image but rather on the RGB one.

Finally, the third block (*Mapping*) is responsible for mapping the selected regions from the RGB image onto the thermal image.

2. Also the *ROIs processing* module is divided into three blocks.

The first block, named *Grayscale Conversion*, handles the conversion of the thermal ROIs from the RGB color space to grayscale so that the white color is associated with the maximum value of temperature, and the black color with the minimum one. Consequently, each ROI undergoes a transformation from three dimensions (red, green, and blue channels) to one dimension (grayscale) to save computational effort. Then, in the *ROIs Partitioning* block, each ROI converted in grayscale is divided by performing both horizontal and vertical slicing. As a result, each ROI is segmented into $N \times M$ subregions, where N represents the number of horizontal slices and M represents the number of vertical slices.

In this way, the last block, called *Partitions Averaging*, allows performing an average assessment on each of the $N \times M$ subregions within the partitioned grayscale ROIs. This process generates two vectors, each with dimensions $[N \times M, 1]$, corresponding to the averaged values of the temperature for each ROI subregion.

3. These two vectors are compared by means of the *Decision* module.

In particular, a *Statistical Test* is performed between the two vectors in order to evaluate whether there is a statistically significant difference between the means of the two groups represented by the vectors. The output of such a Test is the p-value, which indicates the probability of obtaining test results at least as extreme as the result actually observed, under the assumption that the null hypothesis is correct. In this context, the null hypothesis implies no significant difference between the two vectors, suggesting inadequate scoliosis brace pressure. For this reason, the lower the p-value, the lower the probability of erroneously rejecting the null hypothesis. The utilization of a statistically derived score affords independence from absolute temperature (and consequently, pressure) values measured on the patient's back, which significantly vary among different patients and corsets, given the anatomical distinctions inherent to each individual. As a matter of fact, typical pressure values range from 7 to 10 kPa [51], but these values are subject to significant variability both inter-subject and intra-subject. The resulting p-value is compared with a *Threshold* in order to associate it with an *Output* that can indicate whether the scoliosis brace is functioning adequately. More specifically, if the obtained p-value is found to be lower than the threshold value, and if the average temperature of ROI #1 (region where brace pressure is supposed) is greater than that of ROI #2 (region where brace pressure is not supposed), the pressure of the scoliosis corset is indicated as adequate. Conversely, if the p-value exceeds the threshold value, it is indicated as inadequate. The identification of this threshold can

follow an *a priori* model, which is based on prior information, or models based on learning from newly acquired data. 216
217

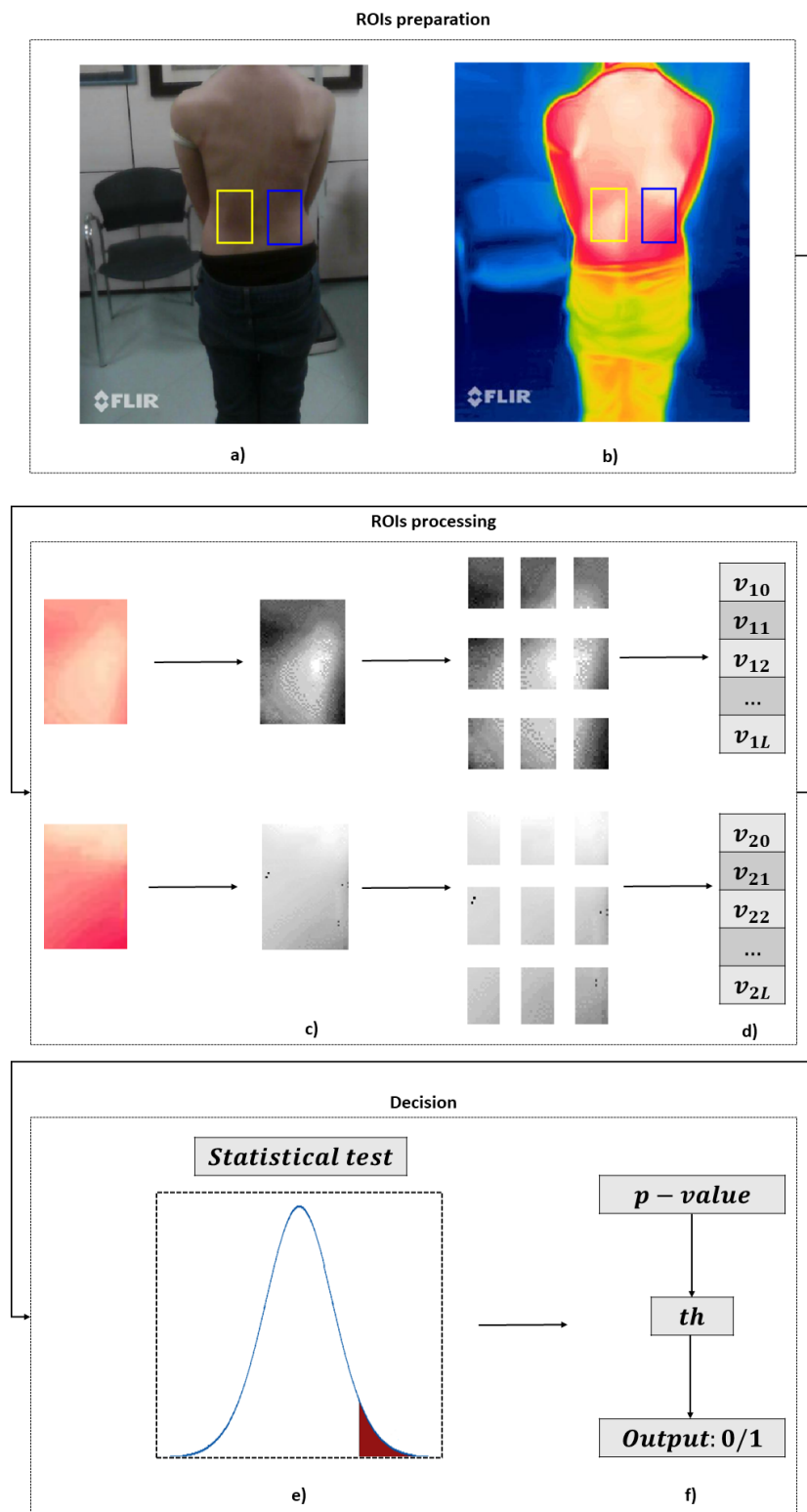


Figure 3. Graphical representation of the proposed method: a) Selection of the ROIs; b) Mapping; c) ROIs Partitioning and Grayscale Conversion; d) Partitions Averaging; e) Statistical test; f) Thresholding and Output.

A graphical representation of the proposed method is shown in Figure 3. The three modules (*ROIs preparation*, *ROIs processing*, and *Decision*) are highlighted along with the inner blocks related to: the selection of the ROIs (a), the mapping onto the thermal image (b), the partitioning and grayscale conversion (c), the averaging of the partitions (d) which provides two vectors v of length $L = N \times M$, the t-test (e), and, finally, the thresholding and output assessment (f), which is 0 if the corset pressure is inadequate, and 1 otherwise.

4. Experimental Validation

This section describes the experimental validation of a system developed on the basis of the proposed IRT-based method. More in detail, first, the experimental setup is described, along with the conducted experimental study on patients. Then, the performance of the developed system was evaluated by means of suitable validation strategies.

4.1. Experimental Setup

The acquisition of the thermal images was performed by using the *FLIR ONE Pro* thermal imaging camera [52], a low-cost attached-to-smartphone camera. The cost of this camera is approximately 450 USD. In terms of metrological performance, the camera provides an accuracy of 3 °C when operated within a temperature range of 15 to 35 °C, and when measuring object temperatures ranging from 0 to 120 °C. The thermal sensitivity is equal to 100 mK. The thermal sensor of the camera operates within a spectral range of 8 to 14 μm , encompassing the range of interest from 8 to 12 μm . The acquired data are stored directly on the smartphone as an image with dimensions of 1440 \times 1080 pixels, while the thermal resolution of the camera is 160 \times 120 pixels. In accordance with the methodology outlined in [41,42], each patient was positioned at a specified distance from the camera. A marked spot on the floor, situated 1 m away from the IR camera, was designated as the reference point. This approach was employed to ensure the repeatability and reproducibility of measurements, as it allowed to guarantee the same camera's performance in terms of resolution and minimized interference from objects near the patients throughout the entire study. All possible obstacles between the IR camera and the patient's back were carefully avoided. For the sake of completeness, a sketch of the acquisition system is shown in Figure 4.

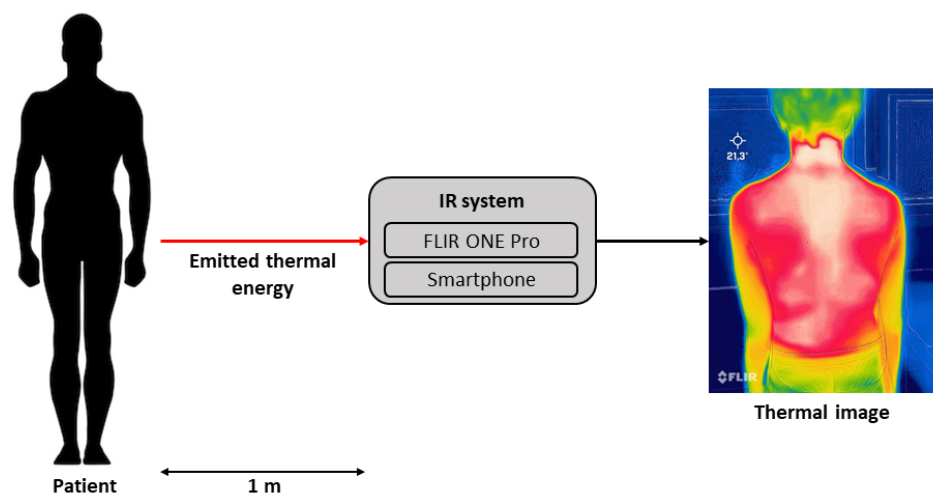


Figure 4. Sketch of the acquisition system.

4.2. Experimental Study

The experimental study was conducted at *Ortopedia Ruggiero*, site in Cardito (Naples, Italy), and included a cohort of 21 patients categorized as juvenile and adolescent, of which fourteen were females. This patients' distribution reflects the evidence that idiopathic

scoliosis is more prevalent in women [53]. All the patients were affected by idiopathic scoliosis and subjected to bracing treatment, hence not under consideration for surgery, with different braces according to the specialist's prescription. For the sake of example, in Figure 5, braces of different models are shown while they are worn by patients. Six patients were affected by dorsal or lumbar scoliosis, and the remaining fifteen suffered from dorso-lumbar scoliosis with a double curve of the backbone. Furthermore, no patient was affected by chronic or acute health conditions that cause temperature changes in the skin surface. Overall, nineteen patients participate in the experimentation once, while two patients were acquired twice during the course of the study.

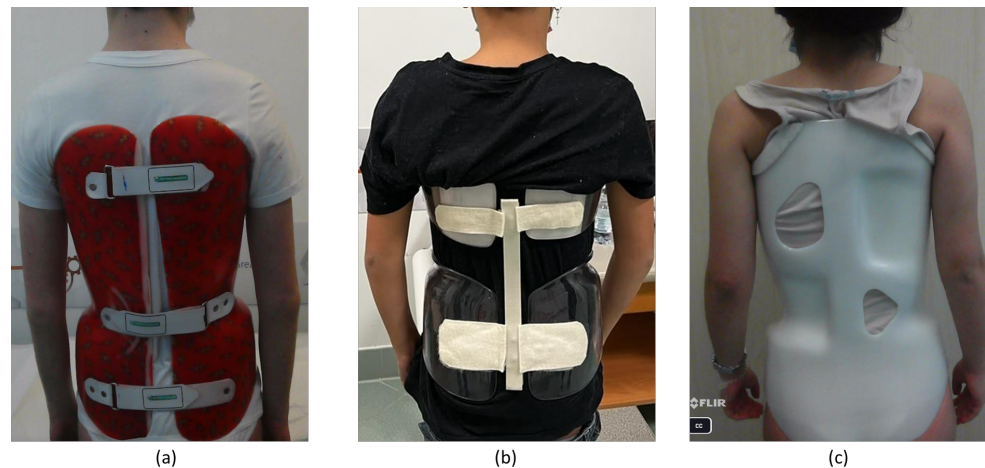


Figure 5. Example of different braces models, (a) *Boston*, (b) *Sforzesco*, and (c) *Cheneau*, worn by three subjects involved in the experimental study.

Before the IR acquisition, the patients were asked to avoid stimulant beverages, physical activity, body creams, and wearing jewelry. The experimental study was carried out in a conditioned room, with non-direct airflow at the patients, with a temperature ranging from 19 °C to 23 °C as it is representative of real operating conditions.

Upon patients' arrival at the facility, their radiographs and orthopedist prescriptions were obtained. Subsequently, they were instructed to rest in a designated room for approximately fifteen minutes to acclimate. During this time, the orthopedist conducted a standard examination of the patient, including an assessment of the brace's compliance based on manual procedures.

After acclimatization, patients were instructed to undress and remove the brace, allowing for thermal images of their back to be captured. This step ensured that any obstruction caused by the brace material was eliminated, enabling clear visualization of the thermal effects resulting from the brace's applied pressure.

At the end of the experimental study, a total of 21 pairs of RGB/thermal images were obtained (one for each patient). For each RGB image, the medical team selected the ROIs as described in Sec. 3. With regards to the patients who suffered from scoliosis with a single curve of the backbone, only a pair of ROIs was selected. Instead, for those suffering from scoliosis with a double curve, two pairs of ROIs were selected.

Overall, the medical team selected 36 pairs of ROIs and assigned a label Y_i to each of them in order to indicate the pressure applied by the brace as (*adequate/1* or *inadequate/0*). The labeling process followed a majority rule to minimize subjective evaluations from a single operator, thus avoiding biasing phenomena.

4.3. Performance Evaluation

The acquired 36 pairs of ROIs were processed in MATLAB environment as described in the *ROIs processing* module shown in Figure 2. After confirming that the data belonged to a normal distribution (by means of a χ^2 test), the statistical test chosen to provide the scores associated with each pair of ROIS was the Student's t-test. Therefore, the dataset to

be analyzed was composed of 36 scores X_i , each one associated with the label Y_i . In order to evaluate the performance of the developed system in terms of classification accuracy (defined as the percentage of instances X correctly classified) and generalization capability (overfitting prevention), a leave-one-out cross-validation (LOOCV) strategy was applied. LOOCV is a common method used to assess the performance and generalization ability of a classifier in a dataset: it is a form of k -fold cross-validation, where k is equal to the number of instances in the dataset. In LOOCV, the dataset is divided into k subsets or folds, where each fold contains only one instance. The model is trained on $k - 1$ folds and then tested on the remaining fold. This process is repeated k times, with each instance serving as the test set once.

In this study, the training was performed by leveraging a grid search between 1000 different values of the threshold th , ranging from 0.005 to 0.500. For each iteration, the threshold value th_{max} that maximized the classification accuracy on the $k - 1$ training folds was used on the test fold k . At the end of the LOOCV process, the classification accuracies obtained from each iteration (defined as the percentage of instances correctly classified) were averaged to obtain a final evaluation of the model's performance. This average performance serves as an estimate of how well the model is likely to perform on unseen data.

However, due to the significant class imbalance in the dataset, with only 10 instances labeled as *inadequate/0* pressure and 26 instances labeled as *adequate/1* pressure, a balancing procedure was conducted prior to the application of leave-one-out cross-validation (LOOCV). Specifically, ten random subsets were created from the original dataset, ensuring that each subset consisted of 20 balanced instances, with half of them labeled as 0 and the remaining half labeled as 1. The procedure for creating each of the ten random subsets was based on randomly selecting 10 instances of the dataset out of the 26 labeled as 1 (changing the seed each time), to which the 10 instances of the dataset labeled as 0 were added. Therefore, LOOCV was applied for each of the ten subsets, thus obtaining ten different values of averaged classification accuracy and related standard uncertainty (evaluated as type-A uncertainty [54]). In this way, the overall mean value and uncertainty extracted provide a robust indication of the system performance on unseen data. Figure 6 provides an illustration of the conducted evaluation of the system performance. The accuracy A and

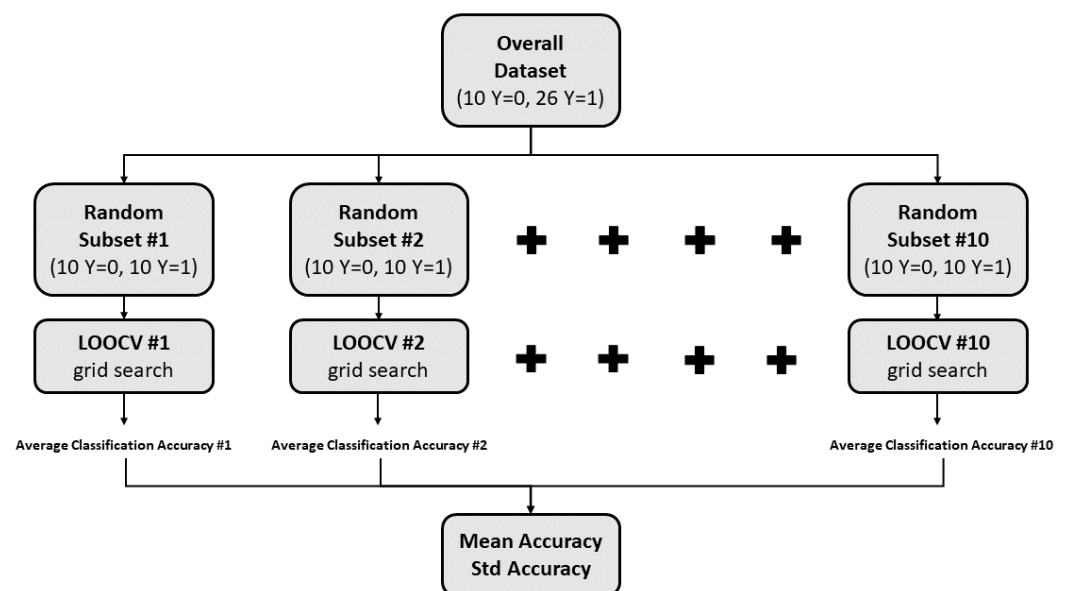


Figure 6. Description of the evaluation of the system performance.

the corresponding standard uncertainty u , obtained for each subset and then averaged, are shown in Table 1, expressed as percentages.

As visible, the overall mean accuracy A_m is equal to 65.5%, while the overall standard uncertainty u_m , evaluated using the first-order law of propagation of uncertainty [54], is

Table 1. Accuracy (A) and corresponding standard uncertainty (u) obtained for each subset and averaged.

Metric	Set #1	Set #2	Set #3	Set #4	Set #5	Set #6	Set #7	Set #8	Set #9	Set #10	Mean
A (%)	70.0	55.0	65.0	75.0	65.0	70.0	60.0	65.0	65.0	65.0	65.5
u (%)	10.5	11.4	10.9	9.9	10.9	10.5	11.2	10.9	10.9	10.9	3.4

found to be equal to 3.4 %. Assuming a normal distribution and a confidence interval of 95 %, a coverage factor $k = 2$ is applied to obtain the expanded uncertainty $U_m = k \cdot u_m$ and express the measurement results as (65.5 ± 6.8) %.

Taking into consideration the employed instrumentation and the approach used in the experimental study, intentionally designed to simulate real-case scenarios, this result proves to be promising regarding further enhancements and potential clinical applications of the system in orthopedic centers.. By utilizing such a system to assess the effectiveness of scoliosis braces, orthopedic specialists would have an objective support that can significantly contribute to the decision-making process. This could lead to further enhancements in the practice of brace-based treatments, eliminating the need to solely rely on the evaluation of curve progression over time before making decisions regarding necessary brace adjustments.

5. Conclusion

This work proposed a method based on low-cost infrared thermography instrumentation for the real-time evaluation of the effectiveness of scoliosis braces. The proposed method leverages the thermoelastic effect to correlate changes in brace pressure with temperature variations on the patient's back. An experimental study at an accredited orthopedic center was conducted on 21 patients of juvenile and adolescent age, simulating real operational conditions and acquiring 36 Region of Interest, each of which was labeled by the medical team. A dedicated algorithm incorporating a typical Machine Learning validation technique was implemented to ensure generalization to unseen data. The experimental results demonstrated a classification accuracy of slightly below 70 %, which represents a promising value considering the use of low-cost instrumentation and intentionally non-ideal experimental conditions.

This study represents a pioneering effort in utilizing systems based on this method for clinical applications. By employing such systems to assess the effectiveness of scoliosis braces, orthopedic specialists can have objective support that significantly contributes to the decision-making process. These findings have the potential to drive further advancements in brace-based treatments, reducing the sole reliance on evaluating curve progression over time before making brace adjustments. Future research will focus on enhancing performance through the implementation of more advanced instrumentation, gathering additional data such as temperature decay curves when patients remove their braces, improving the ROI selection (eventually by means of marker-based approaches), and adopting more sophisticated algorithms to enhance the reliability of this method for orthopedic centers. This also paves the way for new evaluations of the effectiveness of the therapy, based on the observation of the compensation of asymmetric skin temperature distribution along the paravertebral areas over time.

Author Contributions: Conceptualization, L.A.; Methodology, L.A., E.D.B. and A.T.; Software, L.D. and F.L.R.; Validation, L.D. and F.L.R.; Formal Analysis, L.D., E.D.B., F.L.R., and A.T.; Investigation, L.D., F.L.R., and R.R.; Resources, R.R.; Data Curation, L.D., F.L.R., and A.T.; Writing – Original Draft Preparation, L.D. and F.L.R.; Writing – Review & Editing, E.D.B. and A.T.; Visualization, L.D., F.L.R.; Supervision, E.D.B. and A.T.; Project Administration, L.A.; Funding Acquisition, L.A.

Funding: This work was financially supported by the Italian Ministry of University and Research (MUR) through the project "RESearch and innovation on future Telecommunications systems and networks - RESTART" (D.D. MUR no. 341, 15 March 2022) (CUP E63C22002040007).

Informed Consent Statement: The study was carried out following the guidelines of the Declaration of Helsinki. Approval from the institutional review committee was not necessary since the data for this study were collected during regular clinical practice. Informed consent from parents or legal guardians of each patient was not required as the data were anonymized in compliance with GDPR regulations, ensuring they no longer pertain to identifiable individuals. Furthermore, the study did not alter or disrupt the physician's clinical practices for the patients in any manner.

Conflicts of Interest: The authors declare no conflict of interest.

References

1. Trobisch, P.; Suess, O.; Schwab, F. Idiopathic scoliosis. *Deutsches Ärzteblatt International* **2010**, *107*, 875.
2. Negrini, S.; Aulisa, A.G.; Cerny, P.; de Mauroy, J.C.; McAviney, J.; Mills, A.; Donzelli, S.; Grivas, T.B.; Hresko, M.T.; Kotwicki, T.; et al. The classification of scoliosis braces developed by SOSORT with SRS, ISPO, and POSNA and approved by ESPRM. *European Spine Journal* **2022**, *31*, 980–989.
3. Janicki, J.A.; Alman, B. Scoliosis: Review of diagnosis and treatment. *Paediatrics & child health* **2007**, *12*, 771–776.
4. Zaina, F.; De Mauroy, J.; Grivas, T.; Hresko, M.; Kotwizki, T.; Maruyama, T.; Price, N.; Rigo, M.; Stikeleather, L.; Wynne, J.; et al. Bracing for scoliosis in 2014: state of the art. *European journal of physical and rehabilitation medicine* **2014**, *50*, 93–110.
5. Carman, D.; Browne, R.; Birch, J. Measurement of scoliosis and kyphosis radiographs. Intraobserver and interobserver variation. *JBJS* **1990**, *72*, 328–333.
6. Horng, M.H.; Kuok, C.P.; Fu, M.J.; Lin, C.J.; Sun, Y.N.; et al. Cobb angle measurement of spine from X-ray images using convolutional neural network. *Computational and mathematical methods in medicine* **2019**, 2019.
7. Weinstein, S.L.; Dolan, L.A.; Cheng, J.C.; Danielsson, A.; Morcuende, J.A. Adolescent idiopathic scoliosis. *The lancet* **2008**, *371*, 1527–1537.
8. Rigo, M.D.; Villagrasa, M.; Gallo, D. A specific scoliosis classification correlating with brace treatment: description and reliability. *Scoliosis* **2010**, *5*, 1–11.
9. Tsiligiannis, T.; Grivas, T. Pulmonary function in children with idiopathic scoliosis. *Scoliosis* **2012**, *7*, 7.
10. Bignardi, C. Usefulness of Measuring the Pressure Exerted by Orthopedic Braces. *International Journal of Engineering Research and Technology* **2019**, *12*, 2903–2909.
11. Negrini, S.; Donzelli, S.; Aulisa, A.G.; Czaprowski, D.; Schreiber, S.; de Mauroy, J.C.; Diers, H.; Grivas, T.B.; Knott, P.; Kotwicki, T.; et al. 2016 SOSORT guidelines: orthopaedic and rehabilitation treatment of idiopathic scoliosis during growth. *Scoliosis and spinal disorders* **2018**, *13*, 1–48.
12. Richards, B.S.; Bernstein, R.M.; D'Amato, C.R.; Thompson, G.H. Standardization of criteria for adolescent idiopathic scoliosis brace studies: SRS Committee on Bracing and Nonoperative Management. *Spine* **2005**, *30*, 2068–2075.
13. Negrini, S.; Di Felice, F.; Negrini, F.; Rebagliati, G.; Zaina, F.; Donzelli, S. Predicting final results of brace treatment of adolescents with idiopathic scoliosis: First out-of-brace radiograph is better than in-brace radiograph—SOSORT 2020 award winner. *European Spine Journal* **2022**, *31*, 3519–3526.
14. Grazioso, S.; Selvaggio, M.; Di Gironimo, G.; Ruggiero, R. INBODY: Instant Photogrammetric 3D Body Scanner. In Proceedings of the Proceedings of the 7th International Conference on 3D Body Scanning Technologies, Lugano, Switzerland, 30 Nov–1 Dec, 2016, pp. 296–301.
15. Negrini, S.; Grivas, T.B.; Kotwicki, T.; Rigo, M.; Zaina, F.; international Society on Scoliosis Orthopaedic.; stefano. negrini@isico.it, R.T.S. Guidelines on "Standards of management of idiopathic scoliosis with corrective braces in everyday clinics and in clinical research": SOSORT Consensus 2008. *Scoliosis* **2009**, *4*, 1–14.
16. Knott, P.; Pappo, E.; Cameron, M.; deMauroy, J.C.; Rivard, C.; Kotwicki, T.; Zaina, F.; Wynne, J.; Stikeleather, L.; Bettany-Saltikov, J.; et al. SOSORT 2012 consensus paper: reducing x-ray exposure in pediatric patients with scoliosis. *Scoliosis* **2014**, *9*, 4.
17. Daruwalla, J.; Balasubramaniam, P. Moiré topography in scoliosis. Its accuracy in detecting the site and size of the curve. *The Journal of Bone and Joint Surgery. British volume* **1985**, *67*, 211–213.
18. Sudo, H.; Kokabu, T.; Abe, Y.; Iwata, A.; Yamada, K.; Ito, Y.M.; Iwasaki, N.; Kanai, S. Automated noninvasive detection of idiopathic scoliosis in children and adolescents: A principle validation study. *Scientific reports* **2018**, *8*, 1–10.
19. Gaussorgues, G.; Chomet, S. *Infrared thermography*; Vol. 5, Springer Science & Business Media, 1993.
20. Meola, C.; Carlomagno, G.M. Recent advances in the use of infrared thermography. *Measurement science and technology* **2004**, *15*, R27.
21. Bernard, V.; Staffa, E.; Mornstein, V.; Bourek, A. Infrared camera assessment of skin surface temperature—effect of emissivity. *Physica Medica* **2013**, *29*, 583–591.
22. Jones, B.F.; Plassmann, P. Digital infrared thermal imaging of human skin. *IEEE engineering in medicine and biology magazine* **2002**, *21*, 41–48.
23. Osornio-Rios, R.A.; Antonino-Daviu, J.A.; de Jesus Romero-Troncoso, R. Recent industrial applications of infrared thermography: A review. *IEEE transactions on industrial informatics* **2018**, *15*, 615–625.
24. Chrysochoos, A. Infrared thermography applied to the analysis of material behavior: a brief overview. *Quantitative InfraRed Thermography Journal* **2012**, *9*, 193–208.

25. Ishimwe, R.; Abutaleb, K.; Ahmed, F.; et al. Applications of thermal imaging in agriculture—A review. *Advances in remote Sensing* **2014**, *3*, 128. 424
26. Rekant, S.I.; Lyons, M.A.; Pacheco, J.M.; Arzt, J.; Rodriguez, L.L. Veterinary applications of infrared thermography. *American journal of veterinary research* **2016**, *77*, 98–107. 426
27. McBride, A.; Bargmann, S.; Pond, D.; Limbert, G. Thermoelastic modelling of the skin at finite deformations. *Journal of thermal biology* **2016**, *62*, 201–209. 428
28. Faust, O.; Acharya, U.R.; Ng, E.; Hong, T.J.; Yu, W. Application of infrared thermography in computer aided diagnosis. *Infrared Physics & Technology* **2014**, *66*, 160–175. 430
29. Angrisani, L.; Arpaia, P.; De Benedetto, E.; Duraccio, L.; Lo Regio, F.; Tedesco, A. Wearable Brain-Computer Interfaces based on Steady-State Visually Evoked Potentials and Augmented Reality: a Review. *IEEE Sensors Journal* **2023**, pp. 1–1. <https://doi.org/10.1109/JSEN.2023.3287983>. 432
30. Georgios, L.; Kerstin, S.; Theofylaktos, A. Internet of things in the context of industry 4.0: An overview **2019**. 435
31. Hayashi, S.; Kawanishi, K.; Ujike, I.; Chun, P.J. Development of Cloud Computing System for Concrete Structure Inspection by Deep Learning Based Infrared Thermography Method. In Proceedings of the ISARC. Proceedings of the International Symposium on Automation and Robotics in Construction. IAARC Publications, 2020, Vol. 37, pp. 927–934. 436
32. Papež, B.J.; Palfy, M.; Turk, Z. Infrared thermography based on artificial intelligence for carpal tunnel syndrome diagnosis. *Journal of International Medical Research* **2008**, *36*, 1363–1370. 439
33. Apicella, A.; Arpaia, P.; De Benedetto, E.; Donato, N.; Duraccio, L.; Giugliano, S.; Prevede, R. Employment of Domain Adaptation techniques in SSVEP-based Brain-Computer Interfaces. *IEEE Access* **2023**. 441
34. Germi, J.; Mensah-Brown, K.; Chen, H.; Schuster, J. Use of smartphone-integrated infrared thermography to monitor sympathetic dysfunction as a surgical complication. *Interdisciplinary Neurosurgery* **2022**, *28*, 101475. 443
35. Romanò, C.; Logoluso, N.; Dell’Oro, F.; Elia, A.; Drago, L. Telethermographic findings after uncomplicated and septic total knee replacement. *The Knee* **2012**, *19*, 193–197. 446
36. Kawali, A.A. Thermography in ocular inflammation. *Indian Journal of Radiology and Imaging* **2013**, *23*, 281–283. 447
37. Scheidt, S.; Rüwald, J.; Schildberg, F.A.; Mahlein, A.K.; Seuser, A.; Wirtz, D.C.; Jacobs, C. A systematic review on the value of infrared thermography in the early detection of periprosthetic joint infections. *Zeitschrift für Orthopädie und Unfallchirurgie* **2020**, *158*, 397–405. 448
38. Park, D.; Kim, B.H.; Lee, S.E.; Kim, D.Y.; Eom, Y.S.; Cho, J.M.; Yang, J.W.; Kim, M.; Kwon, H.D.; Lee, J.W. Application of digital infrared thermography for carpal tunnel syndrome evaluation. *Scientific reports* **2021**, *11*, 21963. 451
39. Bagavathiappan, S.; Philip, J.; Jayakumar, T.; Raj, B.; Rao, P.N.S.; Varalakshmi, M.; Mohan, V. Correlation between plantar foot temperature and diabetic neuropathy: a case study by using an infrared thermal imaging technique. *Journal of diabetes science and technology* **2010**, *4*, 1386–1392. 453
40. Tan, J.H.; Ng, E.; Acharya, U.R.; Chee, C. Infrared thermography on ocular surface temperature: a review. *Infrared physics & technology* **2009**, *52*, 97–108. 456
41. Luximon, A.; Chao, H.; Goonetilleke, R.S.; Luximon, Y. Theory and applications of InfraRed and thermal image analysis in ergonomics research. *Frontiers in Computer Science* **2022**, *4*, 990290. 458
42. Marzano-Felisatti, J.M.; Martinez-Amaya, A.; Priego-Quesada, J.I. Preliminary Analysis of Skin Temperature Asymmetries in Elite Young Tennis Players. *Applied Sciences* **2023**, *13*, 628. 460
43. Gómez-Carmona, P.; Fernández-Cuevas, I.; Sillero-Quintana, M.; Arnaiz-Lastras, J.; Navandar, A. Infrared thermography protocol on reducing the incidence of soccer injuries. *Journal of sport rehabilitation* **2020**, *29*, 1222–1227. 462
44. Lubkowska, A.; Gajewska, E. Temperature distribution of selected body surfaces in scoliosis based on static infrared thermography. *International Journal of Environmental Research and Public Health* **2020**, *17*, 8913. 464
45. Kwok, G.; Yip, J.; Yick, K.L.; Cheung, M.C.; Tse, C.Y.; Ng, S.P.; Luximon, A. Postural screening for adolescent idiopathic scoliosis with infrared thermography. *Scientific reports* **2017**, *7*, 1–8. 466
46. Redaelli, D.F.; Abbate, V.; Storm, F.A.; Ronca, A.; Sorrentino, A.; De Capitani, C.; Biffi, E.; Ambrosio, L.; Colombo, G.; Frascini, P. 3D printing orthopedic scoliosis braces: a test comparing FDM with thermoforming. *The International Journal of Advanced Manufacturing Technology* **2020**, *111*, 1707–1720. 469
47. Shen, W.; Zhang, J.; Yang, F. Modeling and numerical simulation of bioheat transfer and biomechanics in soft tissue. *Mathematical and Computer Modelling* **2005**, *41*, 1251–1265. 471
48. Dulieu-Barton, J. Introduction to thermoelastic stress analysis. *Strain* **1999**, *35*, 35–39. 473
49. Gulyaev, Y.V.; Markov, A.; Koreneva, L.; Zakharov, P. Dynamical infrared thermography in humans. *IEEE Engineering in Medicine and Biology Magazine* **1995**, *14*, 766–771. 474
50. Hart, J.; Owens Jr, E.F. Stability of paraspinal thermal patterns during acclimation. *Journal of manipulative and physiological therapeutics* **2004**, *27*, 109–117. 476
51. Pham, V.; Houilliez, A.; Schill, A.; Carpentier, A.; Herbaux, B.; Thevenon, A. Study of the pressures applied by a Chêneau brace for correction of adolescent idiopathic scoliosis. *Prosthetics and orthotics international* **2008**, *32*, 345–355. 478
52. FLIR ONE Pro - iOS. <https://www.flir.it/products/flir-one-pro/?vertical=condition+monitoring&segment=solutions>. Accessed: 2023-07-08. 480

-
53. Mitsiaki, I.; Thirios, A.; Panagouli, E.; Bacopoulou, F.; Pasparakis, D.; Psaltopoulou, T.; Sergentanis, T.N.; Tsitsika, A. Adolescent idiopathic scoliosis and mental health disorders: a narrative review of the literature. *Children* **2022**, *9*, 597. 482
483
54. BIPM, I.; IFCC, I.; ISO, I.; IUPAP, O. Guide to the expression of uncertainty in measurement JCGM 100: 2008. *JCGM* **2008**, *101*, 2008. 484
485

Disclaimer/Publisher's Note: The statements, opinions and data contained in all publications are solely those of the individual author(s) and contributor(s) and not of MDPI and/or the editor(s). MDPI and/or the editor(s) disclaim responsibility for any injury to people or property resulting from any ideas, methods, instructions or products referred to in the content. 486
487
488