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# Solar-driven integrated Carbon Capture and Utilization: Coupling CO<sub>2</sub> electroreduction toward CO with capture or photovoltaic systems

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## Abstract

Electrochemical processes have emerged as intriguing strategies for both CO<sub>2</sub> capture and valorization, which are needed to combat global warming and climate change. Among other advantages over competing technologies, electrochemical systems can be powered by renewable sources, including solar energy. This review aims at collecting and analyzing the main works proposed in the literature that study the coupling of electrochemical reactors for the conversion of CO<sub>2</sub> into carbon monoxide with 1) electrochemical capture systems or 2) solar cells to power them. In addition to the critical analysis of these articles, a brief discussion of future research directions in this field is proposed.

**Keywords:** CO<sub>2</sub> capture and conversion; solar cells; carbon monoxide; electrochemistry.

## 1. Introduction

As the 21<sup>st</sup> century progresses, the problem of global warming becomes more and more pressing on our planet. This phenomenon is represented by the average rise in terrestrial temperatures (and a corresponding reduction of rainfall), leading to an increase, both in frequency and intensity, of phenomena such as hurricanes, fires and floods as well as the growth of sea level caused by the melting of glaciers and the desertification of places. This causes problem for biodiversity, due to abnormal migrations, food shortages and hard living conditions [1]. It can be undoubtedly affirmed that this situation has been largely caused by the human activities [2]. Since the industrial revolution, large amounts of greenhouse gases (GHGs) have been emitted in the atmosphere, substantially contributing to the rise in temperatures and to the problems mentioned above. Among the GHGs, carbon dioxide (CO<sub>2</sub>) is the one with the largest concentration in the environment and the longest residence time, thus representing the most impacting climate-altering substance [3]. Moreover, its concentration had the greatest increase from the pre-industrial age up to now. To face the global warming issues, different policies have been established in the recent years. In 2015, the COP21 was held and the Paris agreement was signed. With this agreement, the goal was to keep the temperature increase (compared to the pre-industrial era) to a maximum of 2 °C [4]. In 2020, the EU published the 'European Green Deal', which sets the goal, within 2030, of reducing emissions by 55% (compared to 1990) [5]. This target was revised in 2021 following COP26 in Glasgow, with the main objective to keep the temperature increase within 1.5 °C [6].

To reduce the CO<sub>2</sub> emissions and its accumulation in the atmosphere, carbon capture and utilization (CCU) technologies have been proposed as effective solutions [7-10]. Indeed, some CCU pilot plants were already established all over the world [11-13] and additional ones are planned to be built in the next years [14-16], witnessing the disruptive potential that these technologies can offer. In particular, different strategies can be adopted for carbon capture and separation from flue gas (in order to have more details on this class of

technologies, the reader is invited to have a look on other recently published reviews [17-19]). Among them, the one which is widely adopted is the absorption process using chemical solvents like amines [20]. However, amines are toxic substances, and the energetic costs for their regeneration is not negligible [21, 22]. For what concerns the CO<sub>2</sub> conversion, also in this case different technologies have been proposed in the literature, including, biochemical, enzymatic, photochemical, electrochemical and thermochemical routes [23-25]. The latter represent the most employed one, mainly due to the high efficiency and the capability of obtain large variety of output molecules [26], even though relatively high temperatures are needed to carry out the conversion [27, 28].

In this framework, electrochemical processes demonstrated to be intriguing strategies for both CO<sub>2</sub> capture [29-31] and valorization [32-34]. Indeed, electrochemical routes can guarantee many advantages over the remaining technologies: the processes are repeatable and controllable and can be carried out at mild conditions; it is possible to use green chemicals as reagent and/or supporting electrolytes; the employed reactors are easily up-scalable and compact [35]. Moreover, being both capture and valorization electrochemically-based, the coupling of the two processes become easier, thus providing additional advantages, such as reduced costs for CO<sub>2</sub> transport and potential downstream apparatuses [36, 37]. Finally, another fascinating characteristic is the possibility for electrochemical systems to be powered by renewable sources, in particular by the Sun [38, 39]. This can be seen as a sustainable route for store the excess solar energy that is not put in the electric grid [40], globally allowing a carbon neutral (or even negative) path [41].

Among the different products obtainable from the electrochemical CO<sub>2</sub> reduction reaction (CO<sub>2</sub>RR), techno-economic analyses showed that carbon monoxide (CO) is the one with the highest profitability [42, 43]. In fact, CO can be easily produced at relatively low overpotentials through a 2 electron-reduction pathway [44], and it is widely employed in the chemical industry, representing the most significant and versatile C1-building block [45]. As an example, it used at large industrial scales in the Monsanto/Cativa acetic acid synthesis [46] and, together with hydrogen (H<sub>2</sub>) forms then synthesis gas (syngas) [47], which is exploited in the Fischer-Tropsch synthesis of hydrocarbons [48], and in internal combustion engines [49]. This represent a plus for the electrochemical CO<sub>2</sub>RR (eCO<sub>2</sub>RR) to CO, since usually the hydrogen evolution reaction (HER) is seen as a competing reaction in water-based electrolytes, while in this case CO<sub>2</sub>RR and HER can be carried out simultaneously to obtain syngas with tunable composition [50].

Based on all these premises, it is clear that an all-electrochemical system, consisting of the coupling of (i) a CO<sub>2</sub> separation and capture module and (ii) a conversion module, powered by solar energy, is of crucial interest in order to face the global warming issue. To this end, the aim of this review is to critically analyze the solutions proposed in the literature, which, to the best of our knowledge, do not include a single integrated system. Therefore, after a brief introduction on eCO<sub>2</sub>RR in Section 2, the coupled capture-conversion approaches are reviewed in Section 3, while in Section 4 the solar-driven conversion systems are discussed. Finally, Section 5 will present the future perspectives, suggesting some strategies that are not yet explored by the scientific community.

## 2. Electrochemical CO<sub>2</sub> reduction reaction

The eCO<sub>2</sub>RR is a mechanism for which carbon dioxide is converted in value-added molecules, usually in aqueous electrolytes. Thanks to Proton-Coupled Electron multi-Transfer (PCET), in fact, multi-electron transfer occurs between the electrode and the CO<sub>2</sub> molecules (which can be dissolved in the electrolyte or in a gaseous stream), thus reducing them. This electron transfer, enabling the reduction of the CO<sub>2</sub>, occurs at the cathode, while protons (H<sup>+</sup>) and electrons are provided by an oxidation reaction occurring at the anode (such as the oxygen evolution reaction, OER). Relations (1-4) summarize the main reactions occurring at the anodic (1 and 2) and cathodic (3 and 4) compartments of the electrochemical cell for the CO production (3) and HER (4).



The latter is a competitive reaction with respect to CO<sub>2</sub>RR (relation 3), and often reduces the selectivity toward the carbon products. In this framework, an important parameter for quantifying the selectivity of the device toward the different products of the electroreduction is the Faradaic Efficiency (FE). This parameter describes the efficiency of the electric charge to participate to a particular electrochemical reaction (for example, formation of CO), and is calculated as the total charge involved in the product formation over the total charge passing through the system:

$$FE = \frac{\chi n F}{Q} \quad (5)$$

where  $\chi$  is the number of moles of the product of interest,  $n$  the number of electrons transferred per mole of product,  $F$  the Faradaic constant, and  $Q$  the total charge flowing through the electrodes. Unless otherwise specified, all the FE values reported in this review refer to CO.

The CO<sub>2</sub>RR is favored by the presence of a catalyst, which is the key component for the selectivity of the final product. The catalytic activity towards a specific product, in fact, is governed by the binding strength towards certain intermediates, and the ability of binding CO<sub>2</sub> molecules on the vacant coordination sites on the reduced catalyst surface [51]. It is well demonstrated in literature that the final product formation is determined by carbon-bound intermediates: for the conversion of CO<sub>2</sub> in CO, the reaction pathway is determined by the initial formation of adsorbed hydrogenated reaction intermediates, such as \*COOH or \*OCHO [52]. For further details, interesting *in-situ* techniques have been exploited to study the process of adsorbed intermediate formation and the catalytic reaction mechanisms [53].

While the catalyst governs the reaction kinetics and the final product selectivity, the overall performance of the electrochemical cell is influenced on a series of factors: type of electrolyte and molar concentration [54], pH [55-57], pressure [58], temperature [59] and eventual poisoning of the catalyst [60-62]. Lastly, there exist different electrolyzer designs (as shown in Figure 1), which lead to different operational conditions and electrochemical performance. The single-type cell (Figure 1a) is the simplest configuration, in which both anode and cathode are immersed in the same electrolyte without separation. In the H-type cell (Figure 1b) an ion exchange membrane divides the cathodic and anodic compartments: the membrane adds an ohmic loss, but it allows for a physical separation between the electrodes, such that liquid products do not cross-over from catholyte to anolyte. In the flow cell (Figure 1c), Gas Diffusion Layers (GDLs) allows the transport of gaseous CO<sub>2</sub> molecules to the electrode, thus reducing mass transport limitations. Lastly, in the zero-gap cell (Figure 1d), no distance is present between the catalysts (both cathodic and anodic ones) and the membrane, thus further improving the mass transport. For more detailed information regarding the different cell types, some reviews are proposed to the reader taken from literature [63-65].

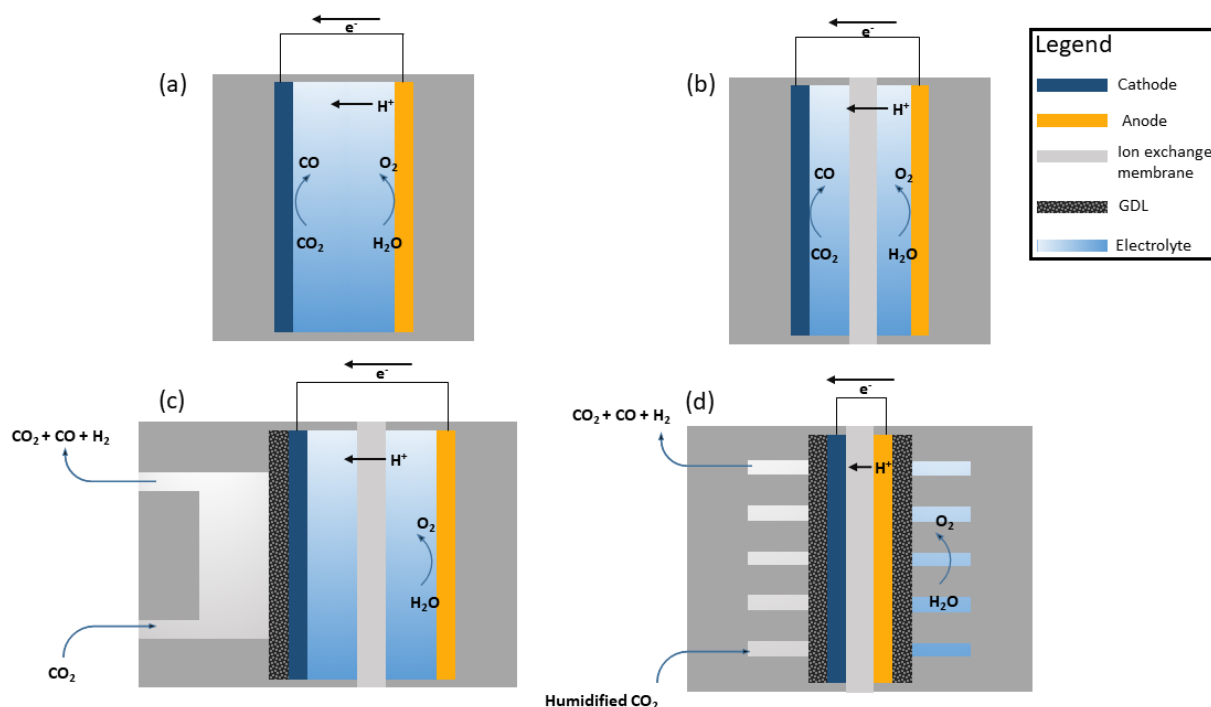


Figure 1 Schematic representation of typical electrochemical reactors for CO<sub>2</sub> reduction: a) single cell, b) H-type cell, c) flow cell, d) zero-gap cell.

### 3. Electrochemical carbon capture and valorization systems

Techniques for the electrochemical conversion of CO<sub>2</sub> have evolved very rapidly in last years. In this framework, there is a growing interest in looking for suitable carbon capture methods that separate the CO<sub>2</sub> from flue gases, and convert it into added-value chemicals. Among the many capture technologies already studied [66, 67], a deep investigation is needed to understand which are actually appropriate to match with a CO<sub>2</sub>RR reactor in terms of optimal working condition. In this framework, it is important to highlight the difference between coupled and integrated systems. In a coupled system (Figure 2a), the separation of gaseous CO<sub>2</sub> from the flue gas occurs in a dedicated device whose outlet is sent to the reactor responsible for the electrochemical conversion. On the other hand, an integrated system (Figure 2b) is able to capture and convert CO<sub>2</sub> in a single device using a novel technique that receive as inlet a flue gas and delivers as outlet the eCO<sub>2</sub>RR products. In the next paragraphs some electrochemical capture technologies that could potentially be coupled/integrated with a typical CO<sub>2</sub>RR reactor [68] are presented.

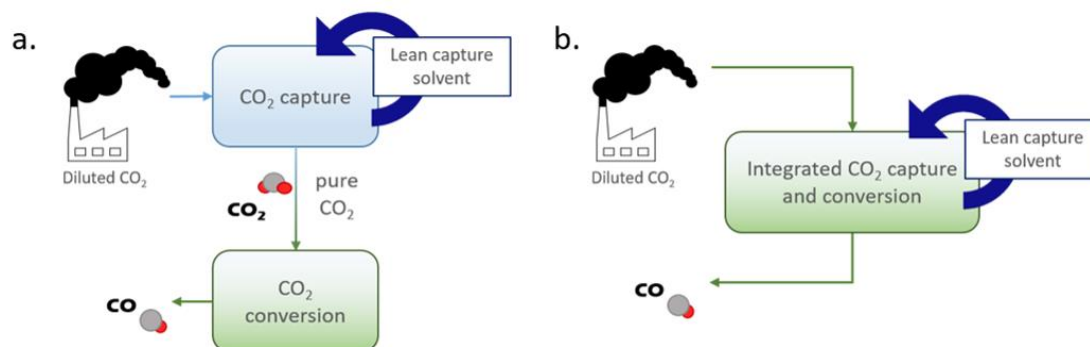


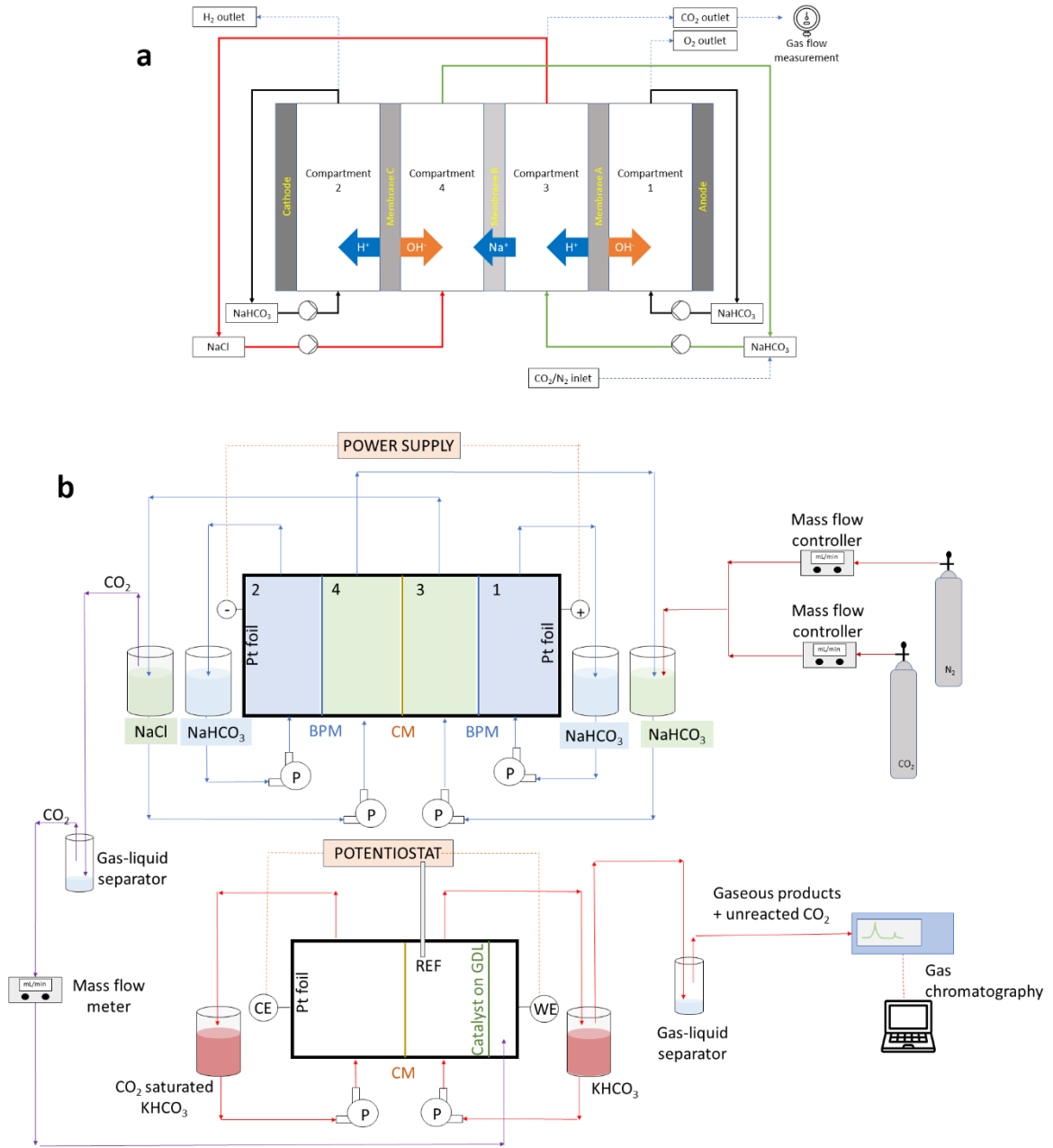
Figure 2 Schematic illustration for a CCU system with (a) coupled capture and conversion and (b) integrated capture and conversion.

### 3.1 Coupled systems

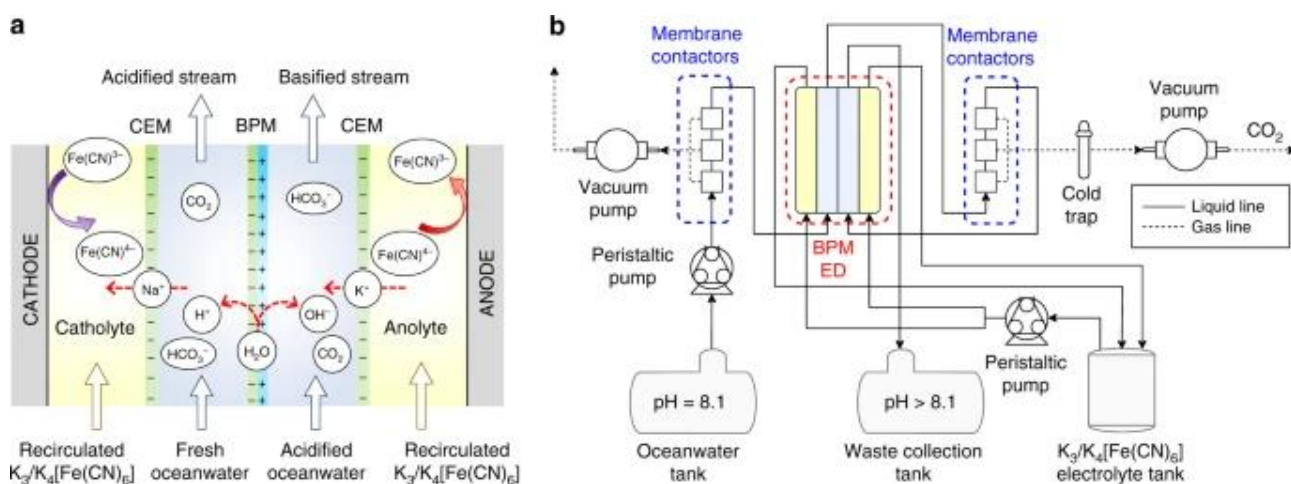
Electrochemical CO<sub>2</sub> capture technologies from point sources have attracted strong interest, since they eliminate the need for thermal energy necessary for the CO<sub>2</sub> stripping from the sorbent solution that is present in amine-based capture methods [69]. The utilization of a pH-swing for the CO<sub>2</sub> absorption and release, implemented by ions exchange membranes and electro dialysis of alkaline carbonate solution, is reported in several works [29, 70]. Sequences of bipolar, cation and/or anion exchange membranes are used to create a pH difference between the compartments of the electrochemical cell, allowing for release and regeneration of the sorbent solution. This system can reach high CO<sub>2</sub> removal rate increasing the current density by keeping a high voltage. However, above 1.23 V vs Reversible Hydrogen Energy (RHE), water splitting occurs producing H<sub>2</sub> and O<sub>2</sub>, thus reducing the global efficiency. Mezza *et al.* [36] showed that it is possible to couple such a system (Figure 3) with an eCO<sub>2</sub>RR cell. CO<sub>2</sub> was successfully filtered from the flue gas through wet scrubbing in NaOH and released into a conversion reactor based on a nanostructured ZnO catalyst on gas diffusion electrode [48] that converted it into CO. Xiang *et al.* [71] reported a proof-of-concept of an electrochemical system exploiting a bipolar membrane electro dialysis cell and a CO<sub>2</sub> reduction cell to extract and convert CO<sub>2</sub> from ocean water. In this last work, catholyte and anolyte contain a reversible redox-couple solution, hence avoiding the water splitting reactions (Figure 4) and increasing the extraction efficiency.

Other techniques are currently being developed [67, 72] to perform CO<sub>2</sub> capture at low energy and they could potentially be useful to build an efficient electrochemical platform. The pH-swing can be enabled by proton carriers undergoing redox reactions whose energy requirement is smaller with respect to electro dialysis mechanisms mentioned above. CO<sub>2</sub> is captured forming an alkaline solution obtained via the reduction of the redox molecule, then it is released through acidification by re-oxidation. This idea has been implemented by Xie *et al.* [73] using riboflavin 5'-monophosphate sodium salt hydrate, and by Kwabi *et al.* [74] using sodium 3,30-(phenazine-2,3-diylbis(oxy))bis(propane-1-sulfonate), as redox proton carriers, respectively. The first one allowed a very low energy dispersion (9.8 kJ per mole of CO<sub>2</sub> desorbed), in addition to have a biological low cost redox-active species. Although these systems are potentially suitable to have eco-friendly closed carbon cycle, they have several practical problems. Firstly, they are vulnerable to oxidizing gases and O<sub>2</sub> is a component of flue gasses. Moreover, the poor cycle performance and the very low release rate make these technologies still underdeveloped to be used in an operative CO<sub>2</sub> capture and conversion system.

In addition to the intrinsic problems of these technologies, several practical issues occur when the capture and the conversion modules are coupled. For instance, the release of CO<sub>2</sub> from an aqueous solution does not ensure a good, pressurized carbon dioxide stream able to feed the CO<sub>2</sub>RR reactor. Moreover contamination of other gasses arising from the capture cell (e.g. O<sub>2</sub>) strongly affects the FE for CO [75].



**Figure 3** CO<sub>2</sub> capture and conversion reported by Mezza et al. a) Electrolysis cell made by two bipolar membranes and two cationic exchange membranes. b) Schematic representation of the process flow including CO<sub>2</sub> capture by wet scrubbing in sodium hydroxide, CO<sub>2</sub> recovery in the electrolysysis cell and conversion into CO in CO<sub>2</sub>RR reactor with ZnO on gas diffusion layer. Reprinted with permission from [36].



**Figure 4**  $\text{CO}_2$  recovery from oceanwater reported by Xiang *et al.* a) Electrodesalination cell made by a bipolar membrane and two cationic exchange membranes. The redox couple  $\text{Fe}(\text{CN})_3^-/\text{Fe}(\text{CN})_4^-$  is used to avoid HER and OER at cathode and anode. b) Schematic representation of the process flow to get a  $\text{CO}_2$  stream from ocean water to feed the conversion reactor. Reprinted with permission from [71].

### 3.2 Integrated systems

The integration of carbon capture and utilization (CCU) permits to solve some of the problems mentioned above. As already shown in Figure 2b, the idea consists in combining the processes employed in CCU using the captured media as an electrolyte inside the electrochemical reactor for the valorization. One way is to release gaseous  $\text{CO}_2$  from the capture media directly near the electrocatalyst responsible for the conversion. The other road is to avoid the energy-intensive  $\text{CO}_2$  desorption from the sorbent agent, performing the electroreduction directly on  $\text{CO}_2$ -loaded capture agents. This implies that the reactor is always fed by high concentration of  $\text{CO}_2$ , decreasing the mass transfer limitation present in  $\text{CO}_2$ RR performed in classic batch cell due to the poor solubility of  $\text{CO}_2$  in aqueous solutions (34 mM). This is a critical step for the Faradaic efficiency of the conversion [76].

For all these reasons, especially if powered by renewable energy, ICCU makes the whole process capture-valorisation more economically advantageous [77, 78]. However it has been calculated that, from an energy perspective, an integrated conversion system must work below 1000  $\text{kJ/mol}_{\text{CO}_2}$  to guarantee a minimum energetic benefit of 44% with respect systems performing sequential capture and conversion present in the state-of-the-art [79].

In the following, the most promising methods for electrochemical ICCU are reported, focusing on CO as product.

#### 3.2.1 Amine-based integration

Nowadays, most part of commercial capture systems exploit amine-based technologies since they are well known for the reversible reactions with  $\text{CO}_2$  [69]. The first trials to integrate capture with conversion used an amine compounds as electrolyte for the electrochemical conversion of  $\text{CO}_2$  [80-82]. The most utilized capture solvents for  $\text{CO}_2$  are monoethanolamine (MEA) [83] and of 2-amino-2-methyl-1-propanol (AMP) [84], that are thermally regenerable.  $\text{CO}_2$  reacts with these substances forming carbamate species [85].

Pérez-Gallent *et al.* [82] carried out the  $\text{CO}_2$  electroreduction in a mixture of AMP and propylene carbonate (PC). The solvent with the carbamate-species is sent to the cathodic compartment of a  $\text{CO}_2$ RR reactor.  $\text{CO}_2$  is desorbed near the electrode as a result of the equilibrium reactions (8) for the carbamate formation:

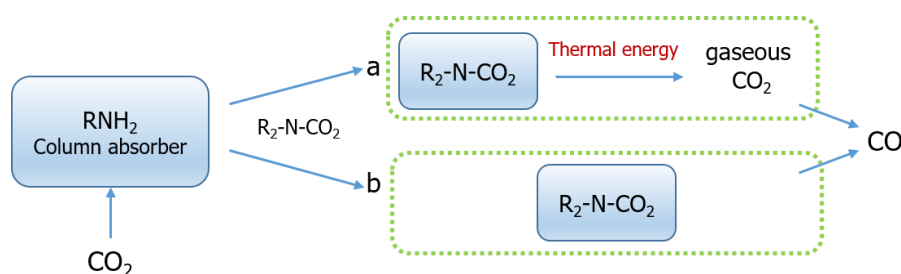


The temperature is kept around 75  $^\circ\text{C}$  in order to reverse (6) and promote the release of  $\text{CO}_2$ , which is then electrochemically reduced. This temperature is easily reached exploiting the Ohmic losses, that usually are a

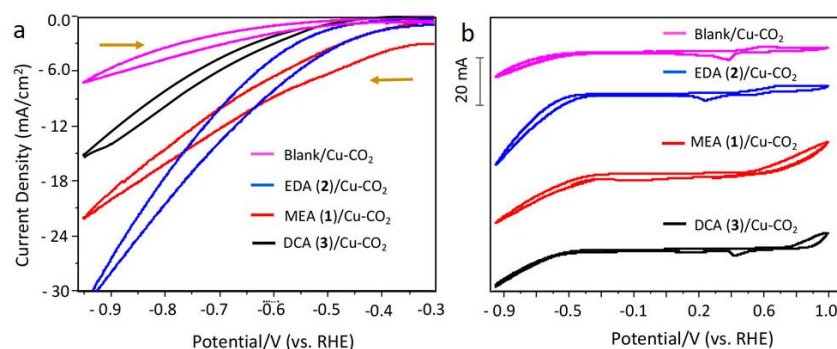


drawback, in standard industrial electrolyzer [86]. This procedure is the one denoted as route (a) in Figure 5. This system, working in a flow cell with AMP 1 M in PC with Au as catalyst at 75 °C, reached a FE of 45% for CO with cathode potential of -1.6 V vs Ag/AgCl and 15 mA/cm<sup>2</sup>.

Except for this example, the main road followed by the research focused on the integration through amine-based processes, is based on the direct electro-reduction (route (b) in Figure 5) of CO<sub>2</sub>-loaded adduct (i.e. RNHCOO<sup>-</sup>) obtained by purging the amine compounds with CO<sub>2</sub>, avoiding high temperature for the release of gaseous CO<sub>2</sub> in the cathodic chamber [87-90]. This permits to have gaseous products (e.g. CO and H<sub>2</sub>) that are not diluted with unreacted CO<sub>2</sub>. Hence, amines and catalyst has started to be studied in recent works to make them suitable for the reduction of carbamates at high FEs. Abdinejad *et al.* [91] studied the electrocatalytic activities of some commercial amine compounds on Cu electrodes. In particular three different compounds has been tested: MEA [83], that form carbamates salts in viscous form, ethylenediamine (EDA) [92] and decylamine (DCA) [93], forming white solid carbamate salts. As reported in Figure 6, EDA-CO<sub>2</sub> provides the highest current density for Cu electrodes (in Figure 6b the peak pair of Cu oxidation can be observed). In particular, it has been performed a chronoamperometry at -0.78 V vs RHE with a current density of 18 mA/cm<sup>2</sup> furnishing a FE for CO of 58%.



**Figure 5** The two roads to implement ICCU through ammine-based processes: a) gaseous CO<sub>2</sub> is released from the CO<sub>2</sub>-rich solvent in proximity of the cathodic catalyst in order to be converted into CO; b) the electroreduction is directly performed on the CO<sub>2</sub>-loaded adduct (i.e. carbamate).



**Figure 6** Cyclic voltammetry of different CO<sub>2</sub>-loaded commercial amine compounds on Cu electrodes in electrochemical H-cell: a) focus on the cathodic potentials, b) full potential range. Reprinted with permission from [91].

The direct electrolysis of carbamates offers an advantageous approach; however, FEs are poorer than classical systems for eCO<sub>2</sub>RR. Lee *et al.* [94], using MEA as electrolyte, got a FE of 5% toward CO with an Ag electrocatalyst, a good and well known material for CO<sub>2</sub> electroreduction. They suggested that this is due to the inefficiency of electron transfer between the electrode and the carbamate molecule; therefore, they deeply investigated the charge transfer between the surface and species in the electrochemical double layer (EDL). The EDL is formed by ethanolammonium and carbamate (since carbamate ions are anions they could be repelled by the cathode surface). The introduction of properly sized electrolyte ions can disrupt the undesired charge-blocking layer, suppressing the hydrogen evolution by minimizing surface coverage of protonated amines and achieving the desired electron transfer to carbamate [79]. Adding KCl (2 M) in 30 wt% aqueous MEA solution, the FE<sub>CO</sub> increased up to 72% at 50 mA/cm<sup>2</sup> and -0.8 V vs RHE. However, this result has been obtained still heating the catholyte at 60 °C, in order to make the N-C bond weaker and promote the carbamate

electroreduction. It should be mentioned that including alkali cations destabilizes the formation of carbamate, affecting the absorption capacity of MEA [95], therefore a trade-off is necessary to favour the carbamate conversion at the lowest possible cost on CO<sub>2</sub> capture.

### 3.2.2 CO<sub>2</sub> electro-reduction from (bi)carbonate aqueous solution

Most recent works on CO<sub>2</sub>RR reached good current densities and high FEs, especially toward CO, using CO<sub>2</sub>-fed systems exploiting Gas Diffusion Electrodes (GDEs) [96]. Although there are important advantages in delivering liquid rather than gas to the CO<sub>2</sub>RR reactor, the very low solubility of CO<sub>2</sub> in aqueous solutions makes fundamental the utilisation of the gas feed.

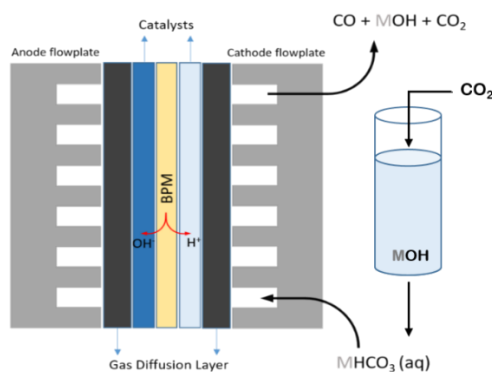
However, imaging to have only liquid feed containing bicarbonate, a bipolar membrane (BPM) delivering H<sup>+</sup> to the cathode makes the HCO<sub>3</sub><sup>-</sup> reacting and generating gaseous CO<sub>2</sub> [97] (reactions 7 and 8) that may be then available for the electro-reduction without any external CO<sub>2</sub> supply [98, 99].



A common system to capture CO<sub>2</sub> is by reaction with an alkali hydroxide solution into HCO<sub>3</sub><sup>-</sup> [100]: therefore it would be possible to use bicarbonate derived from capture as carbon reservoir for the carbon dioxide valorisation. In addition, since the electroreduction of CO<sub>2</sub> into CO follows the reaction (9), derived from the combination of reactions (1) and (3), the OH<sup>-</sup> formed may be used to regenerate the hydroxide sorbent solution, providing a closed circle able to capture and convert CO<sub>2</sub>.



Gaseous CO<sub>2</sub> is formed at the interface of the BPM where protons are delivered. Hence, since the catalyst has to be in contact with the membrane in order to suppress the HER, Membrane Electrode Assembly configuration is necessary. This configuration follows a different arrangement of the typical CO<sub>2</sub>RR reactors elements, as shown in Figure 7 [101, 102].

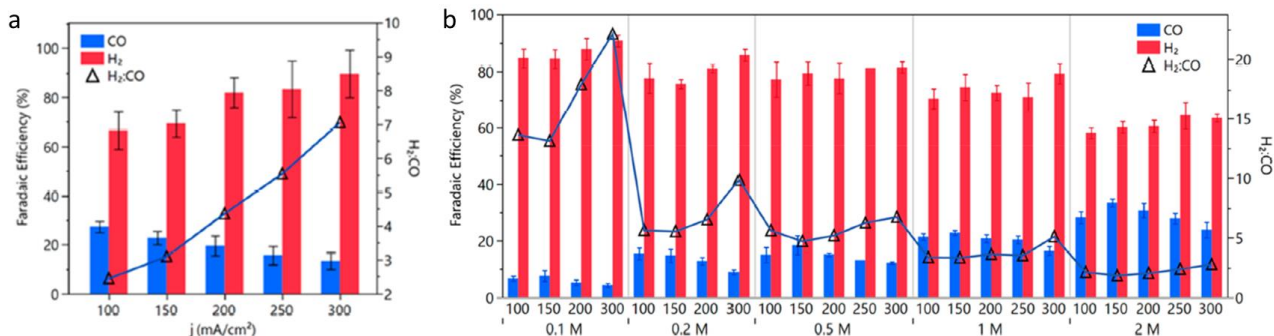


**Figure 7** Schematic representation of a fuel cell-like electrolyzer for CO<sub>2</sub>RR from bicarbonate for a closed carbon circle. M is a general alkali cation.

It has been shown that the electrochemically active specie is not the (bi)carbonate, but the gaseous CO<sub>2</sub> released from that one [98]. The conversion from bicarbonate to CO is enabled by an acidic zone near the membrane interface activating the CO<sub>2</sub> release and by a basic region at the catalyst arisen from the generation of OH<sup>-</sup> from the eCO<sub>2</sub>RR. This whole process is based on a different mechanism with respect the most explored systems exploiting amines, for which research tends to explore the road of the direct CO<sub>2</sub>-loaded adduct, e.g. carbamate.

Li *et al.* [99] used the set-up reported in Figure 7 exploiting Ag nano-structured cathodic electrocatalyst and Ni foam as the anode. They compared the performance of the conversion with pure and capture-generated

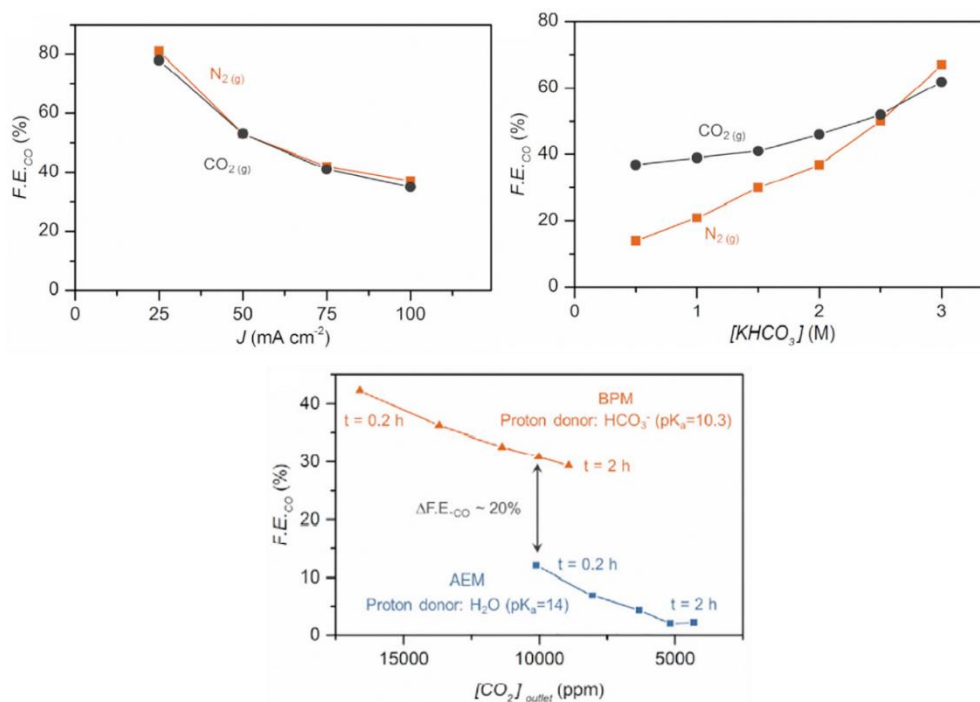
$\text{K}_2\text{CO}_3$ . Firstly, as shown in Figure 8, the  $\text{FE}_{\text{CO}}$  increases with increasing the concentration of KOH of the sorbent solution: this leads to augment the capture-generated  $\text{K}_2\text{CO}_3$ , hence the carbon source. Moreover, there is a slight improvement in FE with respect the case of pure  $\text{K}_2\text{CO}_3$  electrolyte, probably due to the fact that purging  $\text{CO}_2$  in the sorbent solution, not only increases the carbonate concentration, but it generates also a small amount of dissolved  $\text{CO}_2$ , giving an additional contribution to the reservoir of reactant.



**Figure 8**  $\text{FE}_{\text{CO}}$  obtained by Li *et al.* In (a) the experiments have been conducted with 1 M  $\text{K}_2\text{CO}_3$  with nitrogen purging to avoid dissolved  $\text{CO}_2$ . In (b), the experiments have been conducted with different concentrations of KOH purged with  $\text{CO}_2$  to simulate products generated by the capture solution. Reprinted with permission from [99].

Li *et al.* [98] carried out similar experiments using pure  $\text{KHCO}_3$  as catholyte supposing to be the product of  $\text{CO}_2$  capture from KOH and investigated the role of the BPM and the effect of the concentration of the electrolyte. Using a 4 cm<sup>2</sup> membrane electrode assembly with nickel foam anode and silver nanoparticles at the cathode, they confirmed that increasing  $[\text{KHCO}_3]$  brings an improvement of the  $\text{FE}_{\text{CO}}$  (Figure 9b), in agreement with Li *et al.* [99]. However, they observed very small differences comparing the case of  $\text{CO}_2$ -saturated and  $\text{N}_2$ -saturated  $\text{KHCO}_3$  electrolytes. On the other hand, fixing the current at 20 mA/cm<sup>2</sup>, at low electrolyte concentration, the  $\text{FE}_{\text{CO}}$  in  $\text{CO}_2$ -saturated solution is doubled, while the difference is negligible for 2.5 M and 3 M. Data reported in Figure 9c explains how much the employment of a BPM in such a system is fundamental. In the case of an Anion Exchange Membrane (AEM) the build-up of  $\text{OH}^-$  would deplete  $\text{HCO}_3^-$  forming  $\text{CO}_3^{2-}$ . Therefore, the high concentration of protons (lowering the pH) delivered by the BPM facilitates the conversion of  $\text{CO}_3^{2-}$  in  $\text{HCO}_3^-$ , that is then converted into  $\text{CO}_2$  through acid/base process. BPM is able to boost the formation rate of the carbon dioxide, providing a higher concentration of  $\text{CO}_2$  at the outlet, and consequently an important gain in  $\text{FE}_{\text{CO}}$ .

Although these works furnish important information for a simple integration of carbon capture and valorization, classic gas-fed electrolyzer reaches higher current density and FE. Therefore, it is very important to better understand how the performance may be improved. Fink *et al.* [103] studied how the alkali-metal cation can influence the selectivity of the conversion of  $\text{HCO}_3^-$  in order to select the optimal bicarbonate electrolyte that may be used for ICCU. The amount of  $\text{CO}_2$  generated and available at the catalyst results to be controlled only by the  $\text{H}^+$  flux from the BPM and mass transport of  $\text{HCO}_3^-$ , not by the identity of the cation. On the other hand, the selectivity for the CO increases with the cationic radius. This is coherent with what has been already seen in the standard electrochemical reduction of  $\text{CO}_2$  [104]. In all the works mentioned so far, at the anodic side of the fuel cell-like electrolyzer, KOH is used as electrolyte, hence without the need of the gas diffusion layer. In Zhang *et al.* [105], humidified  $\text{H}_2$  gas flows on the anode side reacts with a gas diffusion electrode made by Pt on carbon black. Therefore, using hydrogen oxidation reaction (HOR) instead of OER as source of protons, for a constant current of 500 mA/cm<sup>2</sup>, the total cell potential is below 2.3 V, which is a very small value for such kind of electrolyzer: the drawback is that the  $\text{FE}_{\text{CO}}$  are quite low. Moreover, a microfluidic buffer layer between the silver cathode and the membrane has to be employed: this permits to suppress the HER in favour of the  $\text{CO}_2\text{RR}$ . Also, since  $\text{H}_2$  gas must be produced by water electrolysis, the advantage gained by the small cell voltage must be evaluated with respect the power needed to produce hydrogen.



**Figure 9** a)  $FE_{CO}$  for  $CO_2$  and  $N_2$ -saturated as a function of the current applied. b)  $FE_{CO}$  for  $CO_2$  and  $N_2$ -saturated as a function of the electrolyte concentration at  $20\ mA/cm^2$ . c)  $CO_2$  concentration at the outlet of the cell and the corresponding  $FE_{CO}$  during a time working of 2 hours. Reprinted with permission from [98].

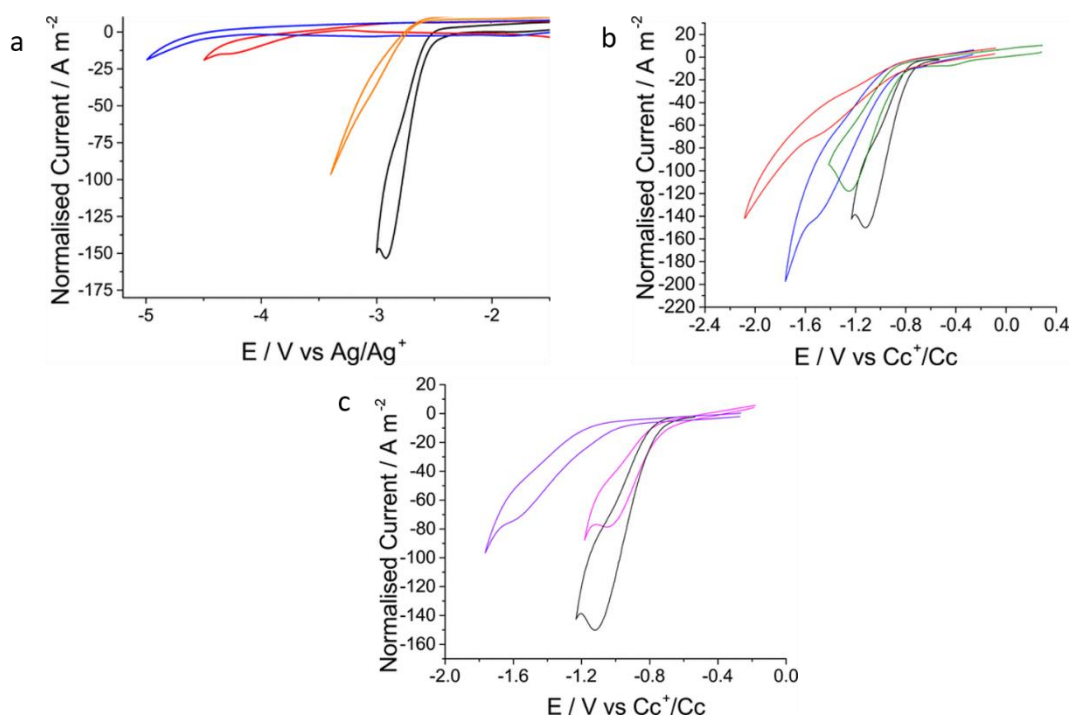
### 3.2.3 $CO_2$ capture and conversion with ionic liquids

Ionic liquids (ILs) are currently a promising solution to substitute amines as a  $CO_2$  capture media [89, 106–108]. At ambient conditions, the strong ion-ion interactions provide a very low evaporation. Also, they are characterized by high thermal stability and large electrochemical window. ILs are inflammable and non-volatile, which make them more environmentally friendly than other solvent such as amines. Furthermore, important chemical and physical properties are tunable by choosing the proper cation or anion part with certain functional group, such that a task specific ionic liquid (TSILs) can be synthesized [109]. Ionic liquids are also emerging as electrolyte in the electrochemical conversion of  $CO_2$ , since they are able to promote the production of useful chemical feedstock [110, 111].

$CO_2$  electroreduction has been studied for several years and, although great advances have been made, the intrinsic limit due to the low concentration of dissolved  $CO_2$  in aqueous electrolyte makes difficult to keep high current density without a further gas fed into the reactor. Rosen *et al.* [112] firstly reported a very selective electroreduction of  $CO_2$  into CO using Ag cathode in a mixed ionic liquid water solvent system. In particular, they obtained a lower overpotential with respect the one that is usually obtained in absence of the ionic liquid. In addition, it has been shown that IL suppress the HER, since it limits the diffusion of  $H^+$  to the catalytic sites [113, 114]. Given this information, there is a concrete possibility to exploit ionic liquids to develop systems where the electrocatalytic reduction is carried out within the capture media.

Tanner *et al.* [115] studied the influence of the electrode material, cation and anion of IL on the peak potential of  $CO_2$  reduction using IL-based electrolyte. Figure 10 highlights the main results of the work. The influence of electrode material on the electroreduction of  $CO_2$  in [Bmim][NTf<sub>2</sub>] [116] has been explored and results are reported in Figure 10a. In the cyclic voltammetry of glassy carbon and platinum, there is no peak corresponding to  $CO_2$  reduction, while with gold and silver electrodes the current density peaks associated to the one-electron reduction of  $CO_2$  are evident. Therefore, the enhanced reduction of  $CO_2$  in ionic liquids previously observed [112] is dependent on the material of the electrode. In particular, silver is able to considerably catalyse the process. Figure 10b and 10c are significant for what concerns the tunability of the chemical properties of ILs. It has been shown that varying the anionic and/or cation part the potential of the reductive wave shifts; in addition, the current density relative to the peak could be increased. However, the differences observed on the

peak current density for different anions/cations are relatively small with respect the influence given by the electrode material. As observed by Tanner *et al.* [115], although [Bmim][FAP] [117] is the IL with the highest solubility of CO<sub>2</sub> [118], it does not show an optimal behaviour as CO<sub>2</sub> electroreduction enhancer.



**Figure 10** a) CV of [Bmim][NTf<sub>2</sub>] on silver (black), gold (red), platinum (orange) and glassy carbon (blue) electrodes. b) CV of CO<sub>2</sub> reduction on silver where ILs cation varied: black [Bmim][NTf<sub>2</sub>], green [Bmpyr][NTf<sub>2</sub>], blue [Emim][NTf<sub>2</sub>] and red [Pmim][NTf<sub>2</sub>]. c) CV of CO<sub>2</sub> reduction on silver where the ILs anion varied: black [Bmim][NTf<sub>2</sub>], pink [Bmim][BF<sub>4</sub>], purple [Bmim][FAP]. Reprinted with permission from [115].

The conversion efficiency of CO<sub>2</sub> into CO in [Bmim][BF<sub>4</sub>] aqueous solution [119] has been investigated in some works. For instance Zhou *et al.* [120] obtained a FE for CO of 70% while, changing the anionic part to chloride, they got the best selectivity for CO with Ag electrode [104]. Also they analysed the detrimental effect of the viscosity on the electrochemical selectivity for CO. The viscosity of the IL is the main limiting factor in the reagent mass transport. Increasing the percentage of water in the solution means to decrease the viscosity and increase the conductivity, but it makes the CO<sub>2</sub> solubility lower and favor the H<sub>2</sub>O reduction. In Table 1 the effect of H<sub>2</sub>O concentration on CO<sub>2</sub>RR and HER are reported as selectivity for CO and H<sub>2</sub> in [Bmim][Cl] [104].

[Emim][OTf]/H<sub>2</sub>O is a further IL previously studied for the CO<sub>2</sub> conversion into CO in aqueous solution giving good selectivity, despite high concentration was required [114, 121]. Welch *et al.* [110] tried to improve the mass transport in [Emim][OTf]/H<sub>2</sub>O using elevated CO<sub>2</sub> pressures. Many ionic liquids have shown a decreasing in viscosity when are subjected to high pressure due to their volumetric expansion [122, 123]. In particular a positive shift in the onset potential and a large increase in the electrocatalytic current for CO<sub>2</sub> reduction occur when the pressure become larger.

In literature, there is not any proof-of-concept of a system performing both CO<sub>2</sub> capture and conversion using ILs as sorbent agent and electrolyte as well. In fact, the different studies have been performed separately on a specific ionic liquid as conversion enhancer or as sorbent agent. Since [Emim][OTf]/H<sub>2</sub>O has been already studied for both the processes [110, 124] it could represent the right solution for a future integration between capture and electrochemical conversion in a ILs-based system. However, such perspective must take into account the absorption selectivity for CO<sub>2</sub> with respect to the other components of flue gas. In general, although N<sub>2</sub> and O<sub>2</sub> has weak solubility in ILs [125], it is known that SO<sub>2</sub> has stronger interactions with ILs than CO<sub>2</sub> does [126], despite the absorption of CO<sub>2</sub> in ILs under the exposure of SO<sub>2</sub> is still under investigation.

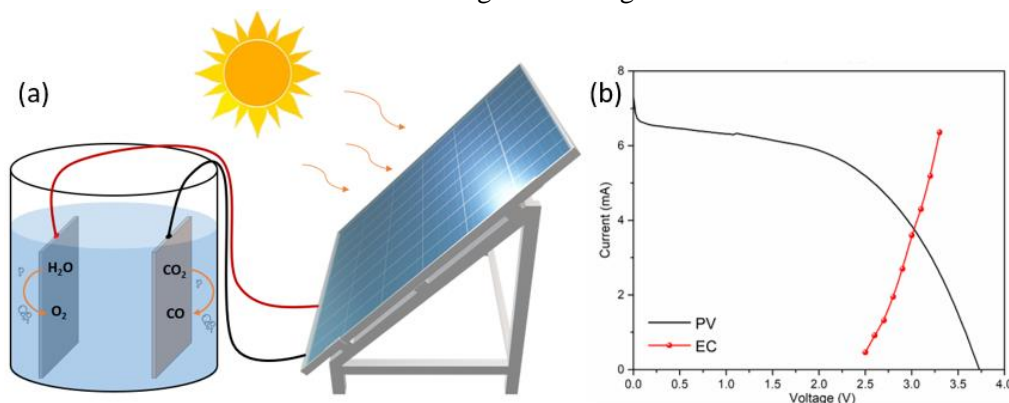


**Table 1** Influence of the water concentration in the [Bmim][Cl]/H<sub>2</sub>O [104] solution on the CO and H<sub>2</sub> selectivities [120].

H <sub>2</sub> O concentration	CO selectivity	H <sub>2</sub> selectivity
20 %	>99 %	-
40 %	99 %	1 %
60 %	70 %	30 %
70 %	50 %	50 %

#### 4. Solar-driven electrochemical CO<sub>2</sub> reduction

Photovoltaic-Electrochemical cells (PV-ECs) derive from the coupling between solar cell modules and electrochemical cells for the CO<sub>2</sub> reduction (Figure 11a). The maturity of the technologies involved [127] makes these devices suitable for scalability, stability and improved control of the efficiency of the single components. On the other hand, the main challenge regarding PV-ECs is related to the electrical operating point: in order to avoid losses and underperformances, in fact, both current and voltage must match between PV and EC modules. This matching can be achieved by engineering the single components such that the current-voltage curves cross each other at the desired operational point (Figure 11b) [128]. For instance, the I-V characteristics can be adjusted by tuning the number of solar cells for the PV module, or by changing the electrode area, catalyst material, cell volumes or electrolyte concentration in the EC module. In any case, in order to maximize the solar-to-fuel efficiency, the voltage-current point must be defined such that the PV works close to its maximum power point and the EC has its maximum selectivity for the desired products. Before reviewing the main PV-EC systems reported in the literature (section 4.3), in the following, an introduction on PV I-V characteristics and technologies will be given.



**Figure 11** (a) Schematic representation of a PV-EC device. (b) I-V characteristic of the PV module (black) and EC (red). Reprinted with permission from [128].

##### 4.1 Solar cell I-V characteristics

A solar cell is a diode in which the photogeneration of carriers (electron, holes) adds a “light current” component  $I_L$  (photocurrent) to the “dark current” of the diode without illumination. Therefore, under illumination, the photocurrent  $I_L$  shifts the I-V curve of the diode, such that a positive power  $P$  can be extracted.

A qualitative representation of the I-V characteristics of a solar cell is depicted in Figure 12. When evaluating the PV performance, there are some fundamental electrical parameters to consider: the open-circuit voltage  $V_{OC}$ , the short-circuit current  $I_{SC}$  and the fill factor  $FF$ . In particular, the  $FF$  defines the quality of the solar cell, by comparing the maximum power point that can be obtained ( $P_{MP}$ ) with the power retrieved by the  $I_{SC}$  and  $V_{OC}$  product ( $P_{MAX}$ ):

$$FF = \frac{P_{MP}}{P_{max}} = \frac{P_{MP}}{V_{OC}I_{SC}} \quad (10)$$

Lastly, the PhotoConversion Efficiency (PCE) defines the amount of electrical power generated for a given incident optical power:

$$PCE = \frac{V_{oc} I_{sc} FF}{P_{in}} \quad (11)$$

The standard test conditions for the solar cells are 1.5 AM or 1-sun illumination (i.e. incident power  $P_{in}$  of  $1000 \text{ W/m}^2$ ), temperature of  $25 \text{ }^\circ\text{C}$  and absence of wind.

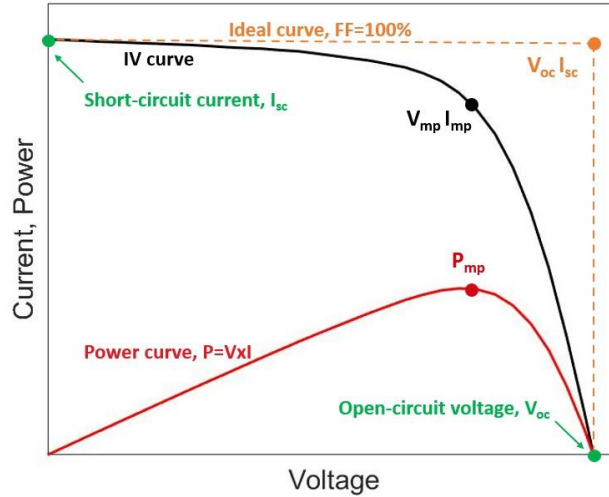


Figure 12 Sketch of the current-voltage characteristic for a generic solar cell under illumination.

## 4.2 Solar cell generations

PV is a well-established sector which takes advantage of a 50-year period of improvement and development [129]. Although different technologies are available today, it is important to carefully choose the PV component for the PV-EC system, since its output determines the solar-to-carbon conversion efficiency in the device.

The first-generation PVs are represented by wafer-based solar cells, which include single or multi-crystalline Si, characterized by high \$/W cost [130], which is a crucial point considering the low-cost target for the PV-EC device.

Second generation PVs get rid of the bulk structure in favor of a thin-film technology. Typical materials used are amorphous or polycrystalline Si (a-Si, p-Si), Cadmium Telluride (CdTe), Copper Indium Gallium Diselenide (CIGS) [131] deposited on either cheap glass substrates, flexible plastic backing or transparent conductive oxides (TCOs). The thin-film solar cells are promising in terms of low-cost manufacturing in large scale production.

The third generation PVs exceed the limitations given by single-junction devices, by introducing new emerging concepts. For instance, tandem cells consist of a multijunction of individual photoactive cells stacked on top of one another, allowing a wider range of wavelengths to be absorbed. Dye sensitized solar cells (DSSCs), in contrast with the conventional cells based on semiconductive materials, are photoelectrochemical devices which separate the photogeneration of charges and the charge transport mechanisms: they gained a lot of attention thanks to their low manufacturing costs and eco-friendly materials [132-134]. Lastly, the Perovskite solar cells (PSCs) take advantage of perovskite-structured crystals as the energy-harvesting active materials. Typical materials include organic-inorganic metal halide perovskites ( $\text{CH}_3\text{NH}_3\text{PbX}_3$ ) [135-137], where X are halogen ions like Br, Cl or I.

In PV-EC devices, the solar cell influences strongly the solar-to-carbon efficiency  $\eta_{\text{stc}}$ , defined as [138]:

$$\eta_{\text{stc}} = \frac{\mu_{\text{th}} \times J_{\text{op}}}{P_{in}} \times FE \quad (12)$$

where  $J_{\text{op}}$  is the operational current density and  $\mu_{\text{th}}$  the thermodynamic potential (e.g.  $\mu_{\text{th}} = 0.11 \text{ V}$  for CO). Unless otherwise specified, all the solar-to-carbon conversions reported in this review refer to the production

of CO. The  $\eta_{\text{stc}}$  describes the efficiency of the PV-EC device in exploiting solar energy for the production of chemical fuels: it is therefore important to both choose the right PV technology and to retrieve the maximum efficiency possible regarding the photogeneration of carriers. As an example, in a work of Gurudayal *et al.* [139], photoelectrochemical CO<sub>2</sub> conversion was performed with two different PV systems, in order to address the effect of the solar cells in the final performance. In the first case (TD1), two commercial Si solar cells were exploited in series ( $V_{\text{oc}}$  of 1.1 V and  $I_{\text{sc}}$  of 61.3 mA at 1-sun illumination), while in the second configuration (TD2) two laboratory-fabricated III-V Si tandem cells were used ( $V_{\text{oc}}$  of 1.4 V and  $I_{\text{sc}}$  of 33.4 mA at 1-sun illumination): in both systems, power matching was retrieved by a maximum power point (MPP) tracker. The CO<sub>2</sub> reduction is performed in the EC module with IrO<sub>2</sub> nanotubes as anode, CuAg as cathode and a CsHCO<sub>3</sub> electrolyte of different concentrations (from 0.1 M up to 0.5 M). In the TD1 case, a  $\eta_{\text{stc}}$  of 3.9% was reached, while a  $\eta_{\text{stc}}$  of 5.6% was achieved with the TD2 configuration: the work showed clearly that the PV device plays a big role in the output of the whole PV-EC system.

### 4.3 Solar-driven CO production

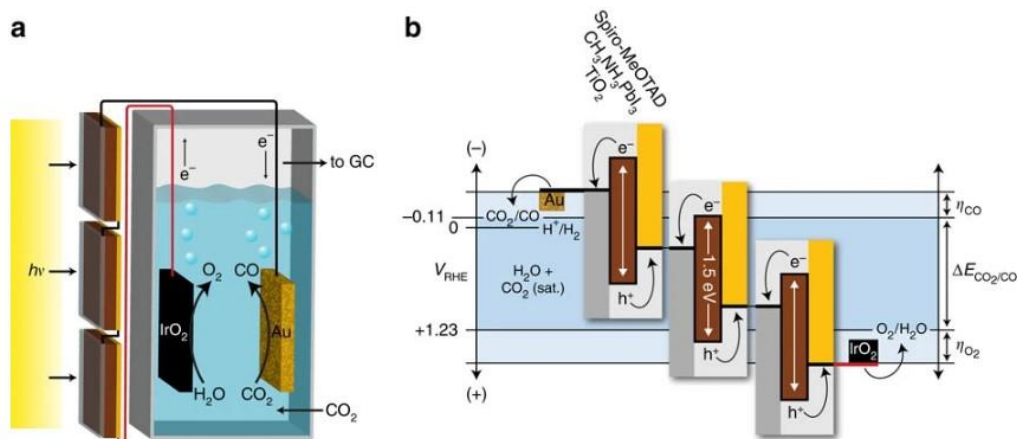
In this section, the main works proposed in literature regarding the conversion of CO<sub>2</sub> in CO, by means of PV-EC systems, are reported, grouped by the electrochemical cell setup employed.

The simplest configuration is given by the single cell setup (already shown in Figure 1a). In this framework, one of the first works was performed by Schreier *et al.* [140] in 2015. In this research, they exploited a series of three perovskite solar cells (for a total  $V_{\text{oc}}$  of 3.1 V and  $I_{\text{sc}}=1.65$  mA) as energy harvesting system, coupled with an electrochemical single cell operating at a current  $I_{\text{op}}\approx 1.65$  mA. Details about the PV-EC device and the energy diagram are depicted in Figure 13. Despite the problem of crossover of dissolved products, the authors chose to implement a single cell compartment without ion-exchange membrane, to avoid overpotentials related to pH gradients at the membrane interfaces. A CO<sub>2</sub>-saturated 0.5 M NaHCO<sub>3</sub> electrolyte is used for ion conduction, IrO<sub>2</sub> as anode for the OER and Au at the cathode as CO<sub>2</sub>RR catalyst. The device reached a FE  $\approx 90\%$  and a  $\eta_{\text{stc}} > 6.5\%$  at 2 V operating voltage for 18 hours: the experiment showed that such PV-EC systems are stable in extended operation under load, paving the way for further improvements.

Arai *et al.* [141] (2019) demonstrated a 3.4% solar-to-CO conversion by coupling six polycrystalline Si photovoltaics cells to earth-abundant catalysts for CO<sub>2</sub>RR. A Mn-complex polymer ([Mn-MeCN], area=3.24 cm<sup>2</sup>) on multi-wall carbon nanotubes has shown a high activity towards CO production with FE  $> 80\%$ , at *ca.* 5 mA in a single cell. A triple-junction amorphous Si cell has been exploited as well and implemented in the photocathode, reporting the possibility of future monolithic artificial photosynthesis systems. In 2021, the same group [142] proposed different supports for the Mn-complex polymer previously studied [141]. In particular, by using the same set-up with poly-Si solar cells and same electrical working conditions, they showed that carbon nanohorns (CNHs) provide a better support with respect to carbon nanotubes for [Mn-MeCN]. The authors report that the CNHs enable to achieve a 3.3%  $\eta_{\text{stc}}$  (almost as high as the previous reported device by Arai *et al.*) with smaller electrode area (1 cm<sup>2</sup> against 3.14 cm<sup>2</sup>).

Finally, for the first time in literature, Sacco *et al.* demonstrated experimentally a fully integrated PV-EC device [128]. A module of five DSSCs ( $V_{\text{oc}}=3.73$  V,  $I_{\text{sc}}=7$  mA) shares the Pt electrode at the cathode with the anode of the electrochemical cell, where OER occurs. The device was able to carry out an unassisted CO<sub>2</sub> reduction to CO, catalyzed by Cu-Sn cathode, with FE=78% and a  $\eta_{\text{stc}}=0.79\%$ . Despite the lower performance, the device opened the possibility for stand-alone PV-EC systems completely integrated.





**Figure 13** (a) Graphical representation of the PV-EC device. (b) Energy diagram of the series-connected perovskite cells and the  $\text{CO}_2$ -CO conversion, with the related overpotentials ( $\eta_{\text{O}_2}$ ,  $\eta_{\text{CO}}$ ) and reaction free energy ( $\Delta E$ ). Reprinted with permissions from [140].

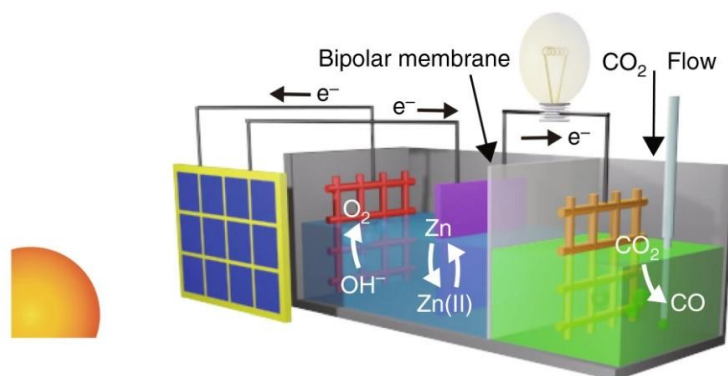
For what concerns PV-EC systems with based on H-type cells (shown in Figure 1b), in a work by Schreier *et al.* [143], a triple junction GaInP/GaInAs/Ge (PCE of 28.5% at 2.24 V) solar cell is exploited as PV, while  $\text{SnO}_2$ -modified CuO nanowires are used as catalyst for both cathodic and anodic compartments. In this case, an ion exchange membrane divides the anodic and cathodic compartments, and 0.1 M  $\text{CsHCO}_3$  and 0.25 M  $\text{CsOH}$  solutions were used as catholyte and anolyte, respectively. In this PV-EC device, they were able to achieve a  $\text{FE} \approx 81\%$  and  $\eta_{\text{stc}}=13.4\%$ , doubling therefore the previous performance. In the same year, as already discussed in the previous section, Gurudayal *et al.* demonstrated the importance of the PV device in the final  $\eta_{\text{stc}}$  of the whole PV-EC system [139].

Chung *et al.* [144] exploited a series of three perovskite solar cells connected to Co-Pi and Au dendrites electrodes for OER and  $\text{CO}_2$ RR respectively. At a  $I_{\text{op}}=2.1$  mA, they achieved a  $\text{FE}=80\%$  and a  $\eta_{\text{stc}}>8\%$  for CO production. Similarly, Bae *et al.* [145] chose a series of three triple-junction Si PV connected to  $\text{IrO}_2$  and nanoporous Au catalysts for OER and  $\text{CO}_2$ RR respectively, reaching a  $\text{FE}=100\%$  and  $\eta_{\text{stc}}=5.3\%$ .

In order to lower the production costs and obtain more environmentally friendly devices exploiting earth-abundant electrocatalysts, Zhang *et al.* [146] used a custom-built large-area  $[\text{CS}_{0.05}(\text{FA}_{0.85}\text{MA}_{0.15})_{0.95}]_{\text{Pb}_{0.9}(\text{I}_{0.85}\text{Br}_{0.15})_3}$  (CsFAMA)-based perovskite solar cell ( $V_{\text{op}}=4.6$  V,  $I_{\text{sc}}=4.3$  mA), single-atom Co anchored on  $\text{Zr}_6$ -cluster-porphyrin framework hollow nanocapsules (Co-SAs/Zr-CPF) as low-cost catalyst for  $\text{CO}_2$ RR and  $\text{RuO}_2$  on carbon paper as OER catalyst. Thanks to the hollow morphology and dispersed Co single atoms of Co-SAs/Zr-CPF, the catalyst showed high activity in the  $\text{CO}_2$ -to-CO conversion, reaching a  $\eta_{\text{stc}}=12.5\%$ .

Thanks to the employment of ion exchange membranes, and by implementing different components and stages to the PV-EC, it is also possible to exploit these devices for more complicated applications. In 2018, Wang *et al.* [147] created a redox-medium-assisted system capable of mimicking the light and dark reactions occurring in green plants. In particular, the photogenerated electrons by InGaP/GaAs/Ge PV ( $V_{\text{oc}}=2.54$  V,  $I_{\text{sc}}=4.38$  mA) are stored in a zinc/zincate ( $\text{Zn}/\text{Zn}(\text{II})$ ) redox pair, in which electrons can be controllably released for the spontaneous reduction of  $\text{CO}_2$ . With nano-gold and nickel-iron hydroxides as catalysts for  $\text{CO}_2$ RR and OER respectively, they managed to achieve a  $\text{FE} \approx 92\%$  and a  $\eta_{\text{stc}}=15.6\%$  at a fixed current of 3.2 mA. A graphical representation of the system is depicted in Figure 14.

With a different approach, a PV-EC system has been designed to obtain simultaneous conversion of  $\text{CO}_2$  and  $\text{H}_2\text{S}$  into CO and S [148]. Powered by a single three-junction Si solar cell, CO is produced through  $\text{CO}_2$  reduction at the cathode, while a redox couple ( $\text{EDTA-Fe}^{2+} / \text{EDTA-Fe}^{3+}$ ) is oxidized in the anodic compartment through electrolysis: the chemical energy stored in the solution enables the conversion of  $\text{H}_2\text{S}$  in S and protons, which flow through the bipolar membrane and close the circuit.

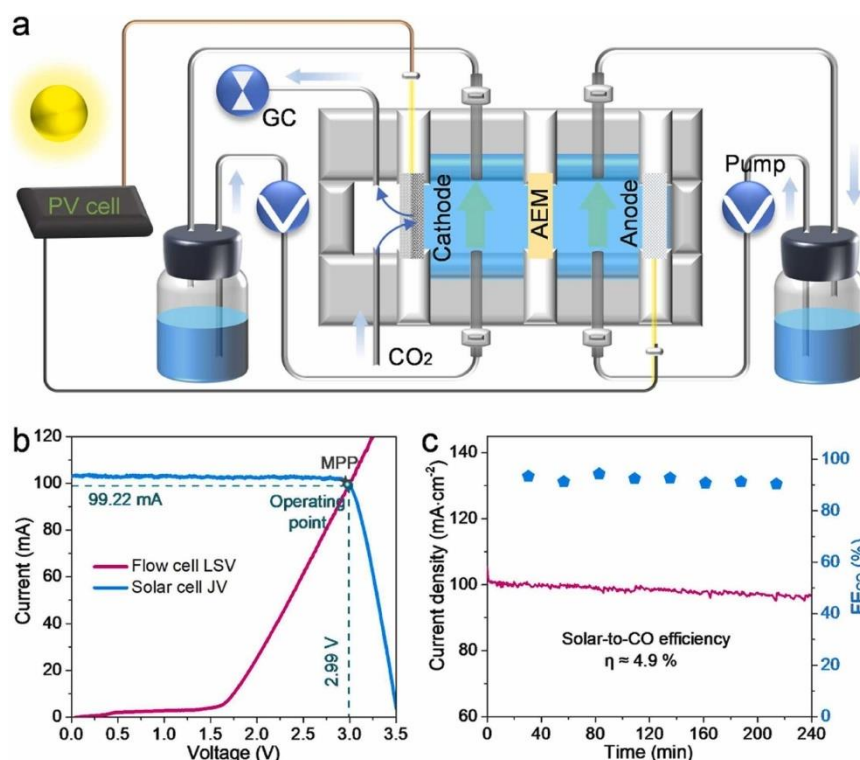


**Figure 14** Redox-medium assisted  $\text{CO}_2$  solar-driven reduction. Reprinted with permissions from [147].

Many efforts have been made to increase the performance and in particular the solar-to-carbon efficiencies by means of GDEs, in the flow type ECs (shown in Figure 1c). In a work of Kim *et al.* [149], Au clusters are anchored on the microporous layer of the GDE, in which gaseous  $\text{CO}_2$  is converted in CO: a NiFe inverse opal (IO) serves as OER catalyst, in a 3 M KOH electrolyte. The device, coupled with a GaInP/GaAs solar cell, recorded high values of  $\text{FE} > 90\%$  and  $\eta_{\text{stc}} = 18\%$  in a 100%  $\text{CO}_2$  gas stream, and  $\eta_{\text{stc}} = 15.9\%$  in a stream of 10%  $\text{CO}_2$  (typical concentration in flue gases). The authors report that, in order to exploit the higher current densities achievable by means of GDEs, it is important to use larger PV areas for high CO partial current densities ( $> 200 \text{ mA/cm}^2$ ).

Cheng *et al.* [150] exploited the flow cell structure as well, with GaInP/GaInAs/Ge PV ( $V_{\text{oc}} = 2.6 \text{ V}$ ,  $I_{\text{sc}} = 4.37 \text{ mA}$ ), Ni as anode in 1 M KOH and Ag nanoparticles on the GDE at the cathode. In order to prevent flooding, the authors chose to mount the cathode such that Ag-NP face the  $\text{CO}_2$  gas stream in a reverse-assembled GDE. With a current density of 4.5 mA, the device managed to reach a  $\text{FE} = 99\%$  and a  $\eta_{\text{stc}} = 19.1\%$  using a simulated AM 1.5G sun illumination at 1 sun, and  $\eta_{\text{stc}} = 18.7\%$  under outdoor light conditions at noon.

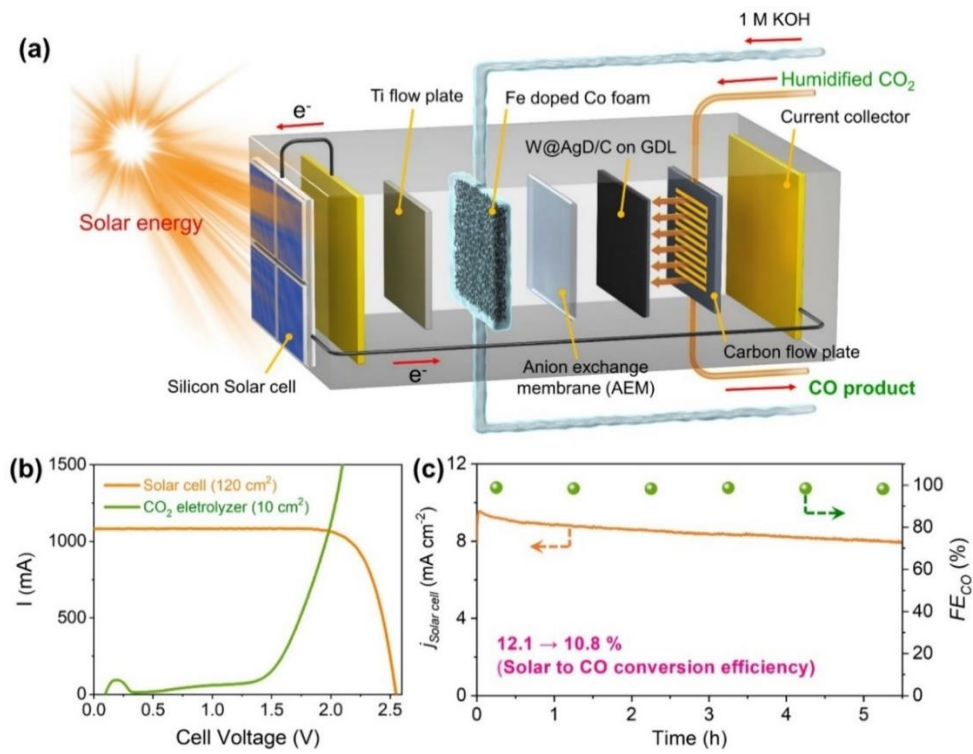
In 2022, Wang *et al.* [151] investigated a single-atom Co-N-C catalyst for solar-driven reduction of  $\text{CO}_2$ , with  $\text{CoN}_4$  sites supported on a carbon black ( $\text{CoN}_4\text{-CB}$ ) acting as GDE for the flow cell. Coupled with a commercial a-Si PV ( $V_{\text{oc}} = 3.51 \text{ V}$ ,  $I_{\text{sc}} = 103 \text{ mA}$ ), and with Ni foam as catalyst for the OER compartment, the device exhibited a  $\text{FE} \approx 92.1\%$  and a  $\eta_{\text{stc}} = 4.9\%$ , operating at a  $I_{\text{op}} = 99.2 \text{ mA}$ . For a better understanding of the device and all the parameters of interest, in Figure 15 the experimental set-up, I-V characteristics and efficiencies of the PV-EC system are reported.



**Figure 15** (a) Set-up of the PV-EC system with flow cell. (b) I-V characteristics of the PV and EC cells at 1 sun illumination, and operating point. (c) Stability test reporting current density and FE as a function of the time of the experiment. Reprinted with permissions from [151].

Finally, exploiting the zero-gap technology (shown in Figure 1d), Lee *et al.* [152] fabricated a large-scale PV-EC device with silicon-based solar cells with an area of 120 cm<sup>2</sup>, obtaining a  $\eta_{\text{stc}} = 12.1\%$  and FE=99% with an outstanding current of  $\approx 1$  A ( $J_{\text{op}} \approx 9.2$  mA/cm<sup>2</sup> normalized on the PV illuminated surface). In this study, to match the high current retrieved by the PV, a zero-gap cell is used as CO<sub>2</sub> electrolyzer, with tungsten-seed-based silver dendrite (W@AgD/C) as CO<sub>2</sub>RR catalyst, Fe-doped Co foam as OER catalyst and 1 M KOH electrolyte. The authors operated the device in real-world conditions as well, on the rooftop of a building: in these conditions, the current was found to be proportional to the solar radiation fluctuations, suggesting that the system is suitable for commercial applications. In Figure 16 it is reported the schematic representation of the PV-EC device with the zero-gap electrochemical cell.

Table 2 summarizes the main parameters of interest regarding the PV-EC devices studied in this present review, highlighting the PV technology, the electric operating point ( $V_{\text{op}}$ ,  $I_{\text{op}}$ ), the electrochemical cell configuration and its electrodes, the Faradaic and solar-to-CO efficiencies. It is important to emphasize that there is a lack of standardization in the specification of the current value at which the PV-EC is working: often, in literature, the current density is provided, but it is not always clear whether it refers to the PV or the EC electrodes. In this review, it has been chosen to report the values of the current intensity  $I_{\text{op}}$  and propose it as the standard value for the current specification in PV-EC devices.



**Figure 16** (a) Graphical representation of the PV-EC device with zero-gap cell. (b) I-V characteristics of the PV and EC cells at 1 sun illumination, and operating point. (c) Stability test reporting current density and FE as a function of the time of the experiment. Reprinted with permissions from [152].

**Table 2** Specification of the PV-EC devices, under 1 sun illumination. The “-” sign replaces data not reported in the articles.

PV (active area)	$V_{op}$ [V]	$I_{op}$ [mA]	EC	OER catalyst (area)	CO <sub>2</sub> RR catalyst (area)	FE [%]	$\eta_{ste}$ [%]	Ref.
3 series-connected Perovskite (0.285 cm <sup>2</sup> )	2.00	1.6	Single	IrO <sub>2</sub> (4.5 cm <sup>2</sup> )	Au (1 cm <sup>2</sup> )	90	>6.5	Schreier <i>et al.</i> (2015) [140]
6 series-connected poly-Si (1.6 cm <sup>2</sup> )	2.19	5.1	Single	$\beta$ -FeOOH:Ni/a-Ni(OH) (2 cm <sup>2</sup> )	[Mn-MeCN] (3.24 cm <sup>2</sup> )	82	3.4	Arai <i>et al.</i> (2019) [141]
Poly-Si (1.6 cm <sup>2</sup> )	2.12	5.1	Single	Ni-doped $\beta$ -FeOOH (2 cm <sup>2</sup> )	CP/CNH/[Mn-MeCN] (1 cm <sup>2</sup> )	-	3.3	Nishi <i>et al.</i> (2021) [142]
DSSC module – integrated (-)	3.00	3.6	Single	Pt (-)	Cu-Sn (1 cm <sup>2</sup> )	78	0.8	Sacco <i>et al.</i> (2020) [128]
GaInP/GaInAs/Ge (0.563 cm <sup>2</sup> )	2.38	6.5	H-type	CuO NW (20 cm <sup>2</sup> )	CuO NW (20 cm <sup>2</sup> )	81	13.4	Schreier <i>et al.</i> (2017) [143]
3 series-connected Perovskite (0.282 cm <sup>2</sup> )	2.68	2.1	H-type	Co-Pi (6.25 cm <sup>2</sup> )	Au (0.025 cm <sup>2</sup> )	80	>8.0	Chung <i>et al.</i> (2022) [144]
3 triple-junction Si (18 cm <sup>2</sup> )	2.70	72.0	H-type	IrO <sub>2</sub> (-)	Au (1 cm <sup>2</sup> )	100	5.3	Bae <i>et al.</i> (2022) [145]
CsFAMA-based perovskite (0.48 cm <sup>2</sup> )	3.20	3.2	H-type	RuO <sub>2</sub> /C (-)	Co-SAs/Zr-CPF (-)	-	12.5	Zhang <i>et al.</i> (2022) [146]
InGaP/GaAs/Ge (0.25 cm <sup>2</sup> )	1.96	3.2	H-type	NiFe hydroxide (0.3 cm <sup>2</sup> )	Au (0.3 cm <sup>2</sup> )	92	15.6	Wang <i>et al.</i> (2018) [147]
Triple-junction Si (-)	-	-	H-type	Graphene (-)	Graphene-encapsulated ZnO (-)	-	7.5	Ma <i>et al.</i> (2018) [148]
GaInP/GaAs (1 cm <sup>2</sup> )	1.63	14.1	Flow	NiFe IO (-)	Au (2 cm <sup>2</sup> )	>90	18.0	Kim <i>et al.</i> (2020) [149]
GaInP/GaInAs/Ge (0.31 cm <sup>2</sup> )	2.23	4.5	Flow	Ni (0.31 cm <sup>2</sup> )	Ag (0.31 cm <sup>2</sup> )	99	19.1	Cheng <i>et al.</i> (2020) [150]
a-Si (25 cm <sup>2</sup> )	2.99	99.2	Flow	Ni foam (1 cm <sup>2</sup> )	CoN <sub>4</sub> -CB (1 cm <sup>2</sup> )	92	4.9	Wang <i>et al.</i> (2022) [151]
Si (120 cm <sup>2</sup> )	-	1100.0	Zero-gap	Fe-doped Co foam (10 cm <sup>2</sup> )	W@AgD/C (10 cm <sup>2</sup> )	99	12.1	Lee <i>et al.</i> (2021) [152]

## 5. Conclusion and future perspectives

In this review, we collected and analyzed the main options proposed in the literature to introduce in the market scenario a new kind of platform able to play an important role toward a closed carbon circle, valorizing CO<sub>2</sub> without further emissions in the atmosphere. In particular, three techniques have been introduced to integrate the carbon capture and utilization, making possible to avoid expensive processes such as compression and transportation of gaseous CO<sub>2</sub>, necessary for instance in carbon capture and sequestration. Among these strategies, CO<sub>2</sub>RR from (bi)carbonate solutions emerges as the most promising one. In fact, different from amine-based processes, it does not include toxic agents; moreover, it demonstrated to be able to provide good FE<sub>CO</sub>. However, there is still room to work on this new solution, in terms of set-up and catalyst, to increase current and FE<sub>CO</sub> and reach the performance already obtained with zero-gap electrolyzer for humidified CO<sub>2</sub>. On the other hand, the utilization of ionic liquids has not been deeply investigated yet. Although they probably would introduce new issues related to the high viscosity and the low conductivity, a thorough investigation can be performed in order to find a suitable IL able to be employed both as capturing agent for CO<sub>2</sub> and as catalyst for eCO<sub>2</sub>RR.

Regarding the solar-driven CO<sub>2</sub> reduction, PV-EC systems are captivating due to the conversion of CO<sub>2</sub> in fuels by means of renewable energy sources, in a scalable and marketable device. Here we covered the progress of this technology throughout the years, highlighting the trend of the solar-to-CO efficiencies and electrical operational points. Different EC setups have been proposed in literature (cell configuration, ORR/CO<sub>2</sub>RR catalysts etc...), along with various PV design and generations, focusing the attention on the I-V characteristics. Current State-of-the-art  $\eta_{\text{stc}}$  of  $\approx 19.1\%$  has been achieved in a flow-cell configuration, while astonishing currents of  $\approx 1.1\text{A}$  have been retrieved by exploiting a large-scale Si solar cell and newer zero-gap cell. In this framework, to reach the current-density requirements for industrialization and large-scale production, PVs should be able to match the high currents of more innovative EC setups. Moreover, energy storage systems should be taken into consideration as well, in order to guarantee continuity in the energy supply to the electrolytic cell in not optimal light conditions (e.g. clouds passing by, or at nighttime). In fact, despite one of the purposes of CO<sub>2</sub> valorization driven by renewable energy sources is to convert the discontinuous electrical energy into chemical energy that can be easily stored, especially when considering the hard-to-abate sectors, the solar-driven electrochemical capture and valorization represents an intriguing solution toward decarbonization. In this framework, the employment of a power management circuit could be a possible solution to couple batteries with the PV-EC device for stand-alone systems.

Finally, considering the different technologies analyzed in this review, it appears that the level of maturity achieved in each of them makes it feasible to design and implement a solar-powered electrochemical system that would enable the coupling of CO<sub>2</sub> capture with its valorization.

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