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1	Can pre-ozonation be combined with gravity
2	driven membrane filtration to treat shale gas
3	wastewater?
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21 Abstract: Low-cost gravity-driven membrane (GDM) filtration combined with appropriate pre-treatment processes has major potential to efficiently manage shale 22 gas wastewater (SGW). In this work, the feasibility of combining low dosage 23 24 pre-ozonation with the GDM process was evaluated in the treatment of SGW. The 25 results showed that pre-ozonation significantly increased the stable flux (372%) of GDM filtration, while slightly deteriorating the quality of the effluent water in terms 26 27 of organic content (-14%). These results were mainly attributed to the conversion of 28 macromolecular organics to low-molecular weight fractions by pre-ozonation. 29 Interestingly, pre-ozonation markedly increased the flux (198%) in the first month of operation also for a GDM process that comprised the addition of GAC (GGDM). 30 31 Nevertheless, the flux of O₃-GGDM systems dropped sharply around the 25th day of 32 operation, which might be due to the rapid accumulation of pollutants in the high flux 33 stage and the formation of a dense fouling layer. Pre-ozonation remarkably influenced 34 the microbial community structure and O₃-GDM systems were characterized by 35 distinct core microorganisms, which could degrade specific organics in SGW. 36 Furthermore, O₃-GDM outperformed simple GDM as a pretreatment for RO. These 37 findings can provide valuable references for combining oxidation technologies with 38 the GDM process in treating refractory wastewater.

39

40 Keywords: Shale gas wastewater; Pre-ozonation; Gravity driven membrane filtration;

41 Mechanism

42 1. Introduction

43 Horizontal drilling and hydraulic fracturing technologies are applied to overcome the challenge of shale gas extraction. Nevertheless, a large amount (~5200-25,870 m³) 44 45 per well) of shale gas wastewater (SGW) is produced during hydraulic fracturing 46 (Kondash and Vengosh, 2015). SGW is typically characterized by high salinity and 47 high concentrations of toxic metals and organics (Butkovskyi et al., 2017). If not 48 treated properly, its discharge would seriously threaten the water environment and 49 human health. At present, hybrid membrane technologies are regarded as suitable and 50 effective means to treat SGW (Tong et al., 2019). Specifically, low-pressure 51 membrane processes, such as ultrafiltration (UF), are investigated and implemented as 52 pretreatment steps for the subsequent desalination (Chang et al., 2019b; Guo et al., 53 2018; Miller et al., 2013). However, operational problems associated with membrane 54 fouling seriously reduce the efficicacy and economy of UF (Shang et al., 2019; Tang 55 et al., 2020).

Gravity driven membrane filtration (GDM), a recently developed membrane technology, has been proposed to replace traditional UF in the pretreatment of SGW (Chang et al., 2019a). The main rationale is that GDM filtration does not need cleaning and can obtain a stable flux driven solely by gravity with the advantages of simple operation, low cost, and low energy consumption (Pronk et al., 2019). The feasibility of the GDM process as a pretreatment option for SGW desalination was verified in a number of research efforts (Chang et al., 2019a; Tang et al., 2021a). While underlining the potential of GDM filtration, these studies highlighted the
current need for significant improvements in stable flux values and contaminant
removal rates of this technology (Chang et al., 2019a; Tang et al., 2021a).

Some processes, including adsorption, aeration, and coagulation were 66 successfully combined with GDM to the purpose of improving its performance (Ding 67 68 et al., 2016; Lee et al., 2021; Tang et al., 2021c). As a strong oxidant, ozone was 69 shown to effectively alleviate membrane fouling when used as a pretreatment process 70 for UF and for membrane bioreactors (MBR) (Sathya et al., 2019; Tang et al., 2020; 71 Wang et al., 2017; Zhang et al., 2020), owing to a reduction of organics molecular 72 size, an enhancement of foulants hydrophilicity, and a decrease of biofouling (Wang 73 et al., 2017). Therefore, we hypothesize that pre-ozonation should also effectively 74 increase the performance of GDM filtration. Generally, it is not recommended to 75 combine pre-ozonation with GDM in the treatment of drinking water, because 76 pre-ozonation has the risk of deteriorating water quality and may produce toxic 77 by-products (Tang et al., 2021b). On the other hand, these issues should not impact 78 the application of GDM filtration to treat wastewater, because this technology would 79 not act as a final polishing step, but instead as pretreatment for subsequent tertiary or desalination processes. The high potential of applying advanced oxidation in the 80 81 specific treatment of SWG and other producted waters has been recently highlighted 82 and it is of great significance to study synergy of ozonation and GDM filtration, two 83 of the most promising processes for efficient SGW management.

84 Therefore, in this study pre-ozonation is investigated in combination with GDM 85 filtration to treat SGW with the aim of increasing stable flux and contaminant removal 86 values in GDM, and improving the quality of the final desalinated effluent. Six GDM 87 systems are examined to understand the effect of pre-ozonation with low ozone 88 dosage on the performance of GDM systems with and without the presence of an 89 additional treatment step through activated carbon adsorption. The integration 90 between pre-ozonation and GDM filtration is thus discussed, also in the light of the effect on microbial communities that drive membrane fouling and organics removal 91 92 and biodegradation within the GDM unit.

93

94 **2. Materials and methods**

95 2.1 Water samples and water quality analysis

SGW samples were collected from the Weiyuan shale gas play (Sichuan Basin,
China). The water quality parameters of the SGW are summarized in Table 1. The
analytical methods for the determination of turbidity, dissolved organic carbon (DOC),
UV₂₅₄, fluorescent organics, and total dissolved solid (TDS) can be found in Text S1
of the Supporting Information (SI) and in our previous study (Tang et al., 2020).

- 101 **Table 1.** Water quality characteristics of the raw water and the raw water treated by O₃
- 102 at different dosages.

Deverseter	Down weaton	Raw water treated by O ₃			
Parameter	Raw water	20 mg/L	40 mg/L	80 mg/L	
DOC (mg/L)	17.48	17.91	18.95	18.54	

$UV_{254} (cm^{-1})$	0.095	0.097	0.100	0.098
Turbidity (NTU)	8.2	7.7	7.2	9.6
TDS (g/L)	19.85	20.14	20.71	19.86

103 **2.2 Experimental setups and procedures**

104	The schematic diagrams and the parameters of the six GDM systems utilized in
105	this work are shown in Fig. S1 and Table 2, respectively. The systems were operated in
106	parallel at room temperature (10-26 °C, Fig. S2) with a hydrostatic pressure of 70 mbar
107	as driving force. The characteristics of the poly(vinylidene fluoride) hollow fiber UF
108	membranes (Litree Purifying Technology Co., Ltd., China) with an effective membrane
109	area of 10 cm ² employed in this study can be found in a previous report (Chang et al.,
110	2019a). The systems ran continuously for 90 days, and the flux was monitored
111	through the electronic balance.

The system referred to as GDM1 treated raw water without any pre-preatment and represented the control unit. On the other hand, the feed water of four of the six GDM systems (namely, GDM-3, 4, 5, 6) was raw water treated by O_3 at different dosages. Low ozone dosages (20-80 mg/L) were applied and the detailed description of the pre-ozonation process can be found in our previous work (Tang et al., 2020). Before the subsequent GDM filtration, the residual ozone in water was quenched by heating the ozonated effluent at 50 °C for 30 min.

Granular activated carbon (GAC, CPG LF 12, Calgon Carbon Co., Ltd., USA)
adsorption was included in four of the six GDM systems, specifically, GDM-2, 3, 5, 6.
The four systems comprising adsorption are referred to as GGDM units. The GAC

122 was cleaned with deionized water and dried before use. A dosage of 4 g was used to 123 pre-treat the influent water to the GDM system, a much smaller quantity than that 124 used in our previous study (Tang et al., 2021a), to slightly reduce the adsorption effect 125 and highlight the effect of microbial degradation in the membrane reactor.

Reverse osmosis (RO) filtration experiments were carried out to verify the effect of different GDM pre-treatment systems on the desalination performance. The RO process was operated at a constant applied pressure of 5.5 MPa (55 bar) with 50% recovery. The RO setup and membrane are described in detail in our previous work (Tang et al., 2020).

131

 Table 2. The parameters of six GDM systems.

No.	Aeration	The addition of GAC	Pre-ozonation
GDM1 (GDM)	10 ml/min	-	-
GDM2 (GGDM)	10 ml/min	4 g	-
GDM3 (O_3^{20} -GGDM)	10 ml/min	4 g	20 mg/L O_3
GDM4 (O ₃ ⁴⁰ -GDM)	10 ml/min	-	40 mg/L O ₃
GDM5 (O ₃ ⁴⁰ -GGDM)	10 ml/min	4 g	40 mg/L O ₃
GDM6 (O ₃ ⁸⁰ -GGDM)	10 ml/min	4 g	80 mg/L O ₃

132 **2.3 Analysis of the membrane fouling layers**

The measurement and calculation methods of hydraulic resistance of the membrane fouling layers, namely, the reversible resistance (R_{re}) and the irreversible resistance (R_{ir}), were identical to our previous study (Chang et al., 2019a). The pure water contact angles and Fourier transform infrared (FTIR) spectra of membrane fouling layers were measured with a KRÜSS DSA 25S instrument (KRÜSS GmbH, Germany) and with an attenuated total reflectance FTIR spectrometer (Nicolet IS 20, 139 Thermo Fisher Scientific Inc., USA), respectively. The surface and the cross-section of the fouled membrane samples, as well as the thickness of membrane fouling layers, 140 141 were observed and measured by scanning electron microcopy (SEM) (FE-SEM, 142 Regulus-8230, Hitachi, Japan). The surface roughness of the fouled UF membrane 143 samples was determined with atomic force microscopy (AFM, Icon, Bruker, 144 Germany). The extracellular polymer substances (EPS) extraction was conducted 145 using a heating and sonication method and the EPS measuring protocol can be found in our recent studies (Tang et al., 2021d). The fluorescent compounds comprised in 146 147 the EPS matrix were measured by fluorescence excitation-emission (EEM) (F7000, 148 Hitachi, Japan)

149 **2.4 Microbial diversity analysis**

150 The variation of the microbial community and the dominant functional 151 microorganisms were analyzed through microbial diversity sequencing of the raw 152 water and membrane fouling layers. The amplified primer sets of 16S rRNA genes for 153 bacteria was 338F/806R. Details about microbial diversity sequencing and analysis 154 are presented in Text S2 of the SI and in our previous study (Tang et al., 2021a).

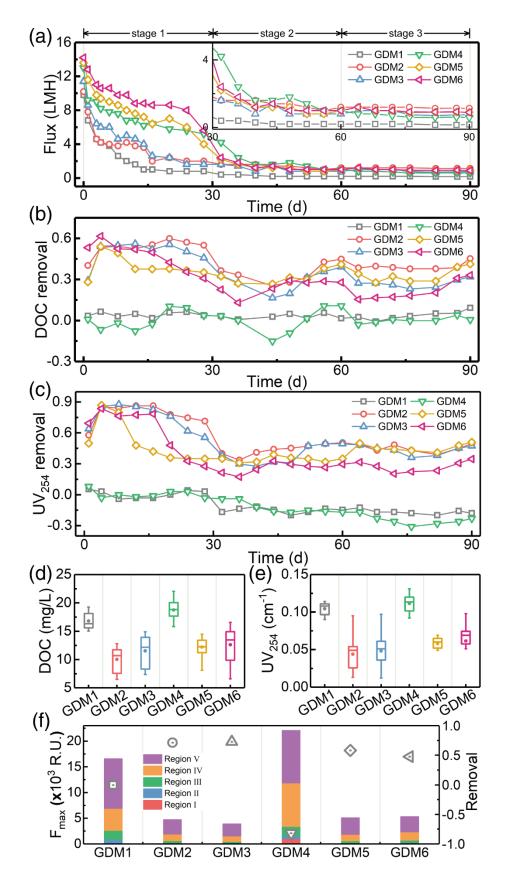
- 155 **3. Results and discussion**
- 156 **3.1 Permeate flux and organic matter removal performance**

157 The hypothesis of this study is that pre-ozonation performance should influence 158 the behavior of the subsequent GDM filtrations, with possibly higher productivity 159 achievable in the membrane step. As presented in Table 1, the DOC and UV_{254} 160 parameters in the raw stream did not decrease upon oxidation, most likely due to the competing effect of mineralization and solubilization of organics (Tang et al., 2021b). 161 Our previous research showed that pre-ozonation mainly changed the organic 162 163 composition and characteristics of SGW, rather than translating into mineralization of compounds (Tang et al., 2020; Tang et al., 2021b). For example, pre-oxidation 164 165 significantly improved the biodegradability of SGW (Liu et al., 2018; Tang et al., 166 2020). The composition and relative content of fluorescent organic matter components 167 in SGW are shown in Fig. S3. The soluble microbial by-product-like matters (region 168 IV) and humic acid-like matters (region V) were the dominant fluorescent organic 169 components in SGW: 3.1%-38.6% of fluorescent organic components were removed 170 by O₃.

171 The flux profiles measured in the six GDM systems are presented in Fig. 1a and 172 analyzed in the light of the pre-oxidation results. The flux trends can be divided into 173 three stages. During the initial filtration stage (stage 1, 0-30 days), a monotonic 174 decline of flux occurred in all the units. However, the flux of GDM systems treating 175 pre-ozonized SGW dropped very slowly and was significantly higher than that of the control GDM system and of the GGDM system without pre-oxidation (GDM2). 176 Specifically, the average flux in the O_3^{40} -GDM system was 2.8 times that of GDM 177 178 and 2.0 times that of GGDM. This result may be attributed to the degradation of 179 macromolecular organic compounds by O₃ into low molecular-weight and more hydrophilic molecules that take more time to deposit on the membrane surface (Tang 180

et al., 2020). However, on the 25th day of operation, the fluxes of O₃-GDM systems
also dropped sharply and this phenomenon may be due to the rapid accumulation of
pollutants due to the relatively high flux upon the formation of a more homogeneous
coating layer at this point of the experiment.

185 Later, the fluxes in the systems continually decreased (second stage, 30-60 days), 186 and ultimately tended to converge to roughly the same steady value (third stage, 60-90 days), due to the formation of stable fouling layers on the membrane surfaces. The 187 final stable flux values in the GDM, GGDM, O₃²⁰-GGDM, O₃⁴⁰-GDM, O₃⁴⁰-GGDM, 188 and O_3^{80} -GGDM units were 0.18, 1.17, 0.85, 0.67, 0.97, and 0.98 L m⁻²h⁻¹ (LMH), 189 respectively. These results suggest that pre-treatment significantly increased the 190 191 productivity of the GDM filtration and that: (i) the productivity increased non-linearly 192 but monotonically with ozone dosage; (ii) GAC adsorption significantly helped 193 increasing the GDM flux.





195 Fig. 1. (a) Flux profile; (b) DOC removal; and (c) UV_{254} removal measured in the six

196 GDM systems. Values of (d) DOC, (e) UV₂₅₄ in the six effluents. (f) Removal rate and

content of fluorescent organics in the effluent of the six systems. GDM1, GDM2,
GDM3, GDM4, GDM5, and GDM6 represent control GDM, GGDM, O₃²⁰-GGDM,
O₃⁴⁰-GDM, O₃⁴⁰-GGDM, and O₃⁸⁰-GGDM units, respectively.

200

Fig. 1b and Fig. 1c present the variation of DOC removal and UV₂₅₄ removal 201 202 rates in the six GDM systems. This rate decreased firstly, then increased, and gradually 203 stabilized. The gradual decrease of GAC adsorption sites is considered to be the main 204 reason for the decline of removal rate in the initial stage; note that the two systems that 205 did not comprise an adsorption process had near zero organics removal in the beginin of 206 the experiments. On the other hand, the increase in removal rate in the second part of 207 the tests may be attributed to the enhancement of microbial degradation and the 208 formation of denser membrane fouling layers (Tang et al., 2021c; Tang et al., 2021d). Instead, the control GDM system and the O_3^{40} -GDM system (no GAC adsorption) 209 210 showed no or decreasing removal rates of organics components, which reached netagive values for UV_{254} compounds. 211

Overall, these observations also support the conclusion that O_3 degraded macromolecular organics into low molecular weight fractions which, when not pre-adsorbed, could directly and more easily pass through into the permeate or undergo biodegradation within the fouling layers, thus further enhancing the passage through the membrane pores. Fig. 1f presents the composition and the relative content of fluorescent organic compounds in the effluent of the six GDM systems. The four 218 GGDM systems were associated with fluorescent organic compounds (47.6-72.8%). 219 However, the removal rate of fluorescent organic compounds, indicative of soluble microbial by-product-like matters, was negative in the O_3^{40} -GDM system. A factor 220 221 that should also be considered when analyzing removal results is the phenomenon of 222 concentration (Tang et al., 2021a). Since our GDM systems were based on dead-end filtration, contaminants would be concentrated in the reactor and this concentration 223 224 would be more important for systems associated with higher flux values. We assessed 225 the DOC value in the GDM reactors. (Fig. 1d and Fig. 1e): adsorption effectively 226 reduced the amount of organics in the feed streams to the membranes, and this amount was the highest in the O_3^{40} -GDM system, thus also contributing to a more 227 challenging separation and overall negative values of organics removal. Not 228 229 surprisingly, the higher the productivity of the systems the larger was the observed 230 DOC concentration.

231 To summarize, pre-ozonation produced improvied productivity in GDM filtration 232 systems, which in fact increased as a function of oxonation strength. Smaller and 233 more biodegradable organic compounds in the oxidized effluent would translate into a 234 somewhat facilitated passage of organics into the permeate stream, also exacerbated 235 by faster solubilization within the fouling layer. When adsorption of the oxidized 236 effluent was included as an intermediate pre-treatment step, a higher removal rate of 237 organics was consistently obtained compared to the treatment of the raw effluent without pre-ozonation. As suggested by these results, different properties and a 238

different composition of the membrane fouling layers should be expected following
the different pre-treatment combinations, as fouling layers are a direct consequence of
feed stream characteristics and water flux values.

242 **3.2** Characteristics of membrane fouling layers

243 Fig. S4, Fig. S5, and Fig. 2 present surface and cross-sectional micrographs of 244 fouled membrane samples collected from the six GDM systems. A dense fouling layer 245 was always observed, also corroborated by the fact that the typical IR peaks of virgin 246 PVDF membrane disappeared in the FTIR spectra of fouled membranes (Fig. S6c). 247 The layer thickness and roughness were the largest for the control GDM unit, while the distribution on the surface was very uneven. In addition, some pollutants were 248 also deposited within the membrane pores. Compared with GDM and GGDM, the 249 250 fouling layers of O₃-GDM systems were consistently thinner.

As summarized in Fig. S6a, the membrane fouling resistance of GDM systems is mainly reversible, with reversibility accounting for above 90% of the total resistance value. The pure water contact angles of fouling layers (Fig. S6b) indicated that pre-ozonation increased the hydrophilicity of the fouling layers by increasing the hydrophilicity of pollutants, while simultaneously GAC adsorption decreased the hydrophilicity of the fouling layers by absorbing hydrophilic pollutants.

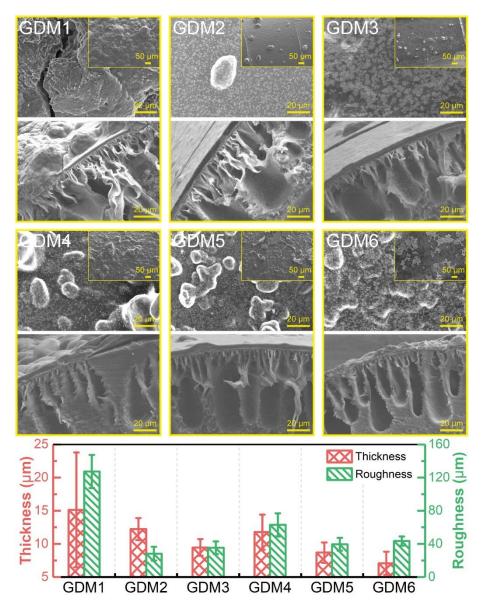


Fig. 2 Surface (top; $500 \times$ and $100 \times$) and cross-sectional (bottom; $500 \times$) micrographs of the fouled membrane samples from the six GDM systems, as well as thickness and roughness values measured for the membrane fouling layers. GDM1, GDM2, GDM3, GDM4, GDM5, and GDM6 represent control GDM, GGDM, O_3^{20} -GGDM, O_3^{40} -GDM, O_3^{40} -GGDM, and O_3^{80} -GGDM units, respectively.

263

257

The results presented in Fig. 3a suggest that the accumulation of overall organic contaminants on the membrane of control GDM and O_3^{40} -GDM systems was the

266 lowest and the largest, respectively. This observation is corroborated by the amount of 267 EPS detected on the membranes and by the EEM analysis (Fig. 3b, c). The EPS 268 content of the fouling layer in the four O₃-GDM systems was higher than that observed in GDM and GGDM units, and highest in the O₃⁴⁰-GDM unit. The same 269 270 conclusion can be also drawn for fluorescent organic compounds. In particular, thse 271 compounds were distributed in region II (aromatic protein) and especially in region 272 IV (soluble microbial by-product-like matters), suggesting the important contribution 273 of transformation phenomena occurring within the fouling layer.

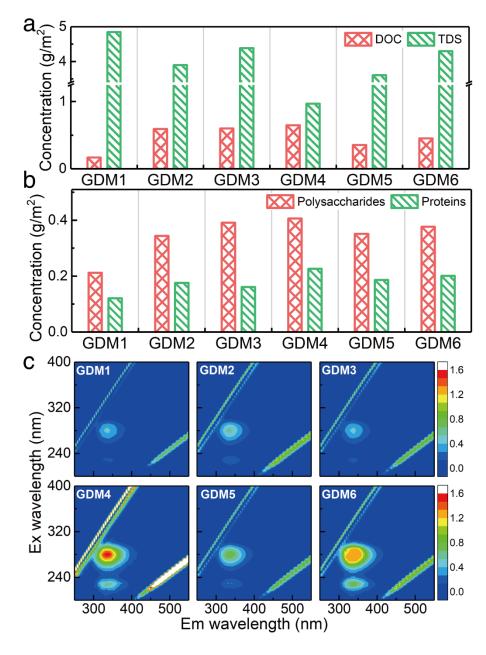


Fig. 3 Concentration of (a) DOC and TDS, (b) EPS (includes polysaccharides and
proteins) in the fouling layers. (c) EEM spectra of compounds in the fouling layers.
GDM1, GDM2, GDM3, GDM4, GDM5, and GDM6 represent control GDM, GGDM,
O₃²⁰-GGDM, O₃⁴⁰-GDM, O₃⁴⁰-GGDM, and O₃⁸⁰-GGDM units, respectively.

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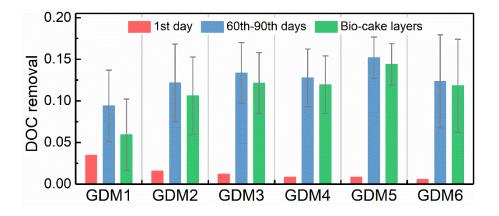


Fig. 4 DOC removal of UF membrane of six GDM systems at 1st day and 60th-90th
days of operation and DOC removal of fouling layers at 60th-90th days. GDM1,
GDM2, GDM3, GDM4, GDM5, and GDM6 represent control GDM, GGDM,
O₃²⁰-GGDM, O₃⁴⁰-GDM, O₃⁴⁰-GGDM, and O₃⁸⁰-GGDM, respectively.

284

285 The relative DOC removal rates of UF membranes can be obtained from the 286 varying concentrations of DOC in the reactor and effluent at any time to understand 287 the role of fouling layers as they form during operation (Fig. 4). The fouling layers 288 three functions, physical interception, perform namely., adsorption, and 289 biodegradation, which increase the contaminants removal in GDM systems (Tang et 290 al., 2021d). Specifically, the DOC removal attributable to the fouling layer can be 291 estimated by subtracting the DOC removal of the 1st day (no fouling layer present) 292 from that observed during the stable flux stage (days 60-90). The DOC removal of 293 the fouling layer was 5.9% and 10.6% in control GDM and GGDM systems, respectively. This parameter was significantly higher in all units treating pre-ozonized 294 295 streams. As mentioned above, the thickness of the fouling layer of GDM and GGDM

296 was thick and one would expect higher DOC removal by physical exclusion. Therefore, the higher DOC removal assessed in the four O₃-GDM systems might be 297 298 attributed to the higher biodegradation function of the fouling layers. In our work, we 299 did not directly appraised the relative proportion of physical interception and 300 biodegradation mechanisms resulting in organic removal. However, previous research 301 indirectly determined the importance of these phenomena by adding biological 302 inhibitors, such as sodium azide (Tang et al., 2021d), with results consistent with the 303 present observations.

304 **3.3 Microbial diversity analysis**

The number of effective sequences, alpha diversity indexes, OUTs, and rarefaction curves for microbial communities in the raw water and in the fouling layer of the six GDM systems are presented in Table 3 and Fig.S7. The richness and diversity of microbial communities in the raw water were higher than those on membranes. The coverage values and rarefaction curves suggested the sequencing depth were sufficient.

Principal component analysis (PCA) at OUT level (Fig. S8) provides information on the affinity relationships of microbial community between the raw water and the fouling layers in the six GDM systems, as well as among the six GDM systems. The microbial community composition in the raw water was vastly different from that observed in the samples from the six GDM systems, indicating new dominant microorganisms had been formed in the filtration reactors. Also, pre-ozonation

317 seemed to have a large effect in the microbial community. The microbial community 318 compositions from the four GDM systems treating pre-ozonized SGW as feed water 319 were all similar, but different from the composition of the other two GDM systems 320 This result also indicates that GAC had little effect on the microbial community. 321

322 Table 3 Number of effective sequences, OTUs, alpha diversity indexes for microbial

Sample Name	Number of effective Sequences	OTUs at 97% identity	Shannon	Chao	Coverage
Raw water	36178	316	3.83	334.6	0.9988
GDM1	36064	115	2.50	119.2	0.9996
GDM2	30672	113	2.68	121.3	0.9994
GDM3	28903	88	2.52	107.4	0.9993
GDM4	29351	62	2.75	66.2	0.9997
GDM5	29713	92	2.93	105.0	0.9994
GDM6	24814	81	3.01	84.0	0.9997

323 communities in the raw water and on the membrane of the six GDM systems.

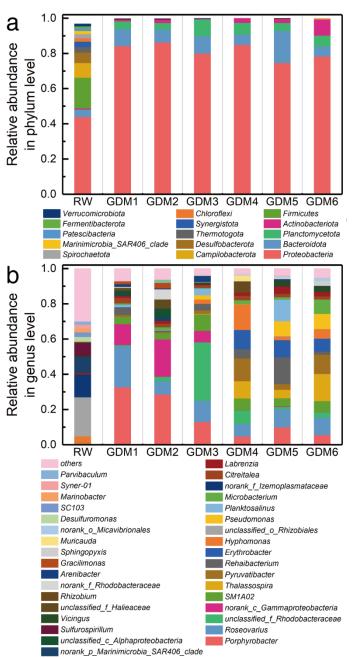
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Fig. 5a and Fig. 5b show the microbial community composition at the phylum 325 326 and genus level, respectively. Proteobacteria (44.1%), Firmicutes (17.5%), 327 Campilobacterota (8.4%), Desulfobacterota (5.9%), and Bacteroidota (4.2%) were 328 the major phyla in the raw water, comprising 80.1% of bacteria. After operation, 329 Proteobacteria (74.8%-86.5%) and Bacteroidota (5.6%-18.2%) became the absolute 330 dominant microbial phyla in GDM reactors. The major genera in the raw water were unclassified_o_Rhizobiales, 331 norank_f_Izemoplasmataceae, Parvibaculum,

332 Sulfurospirillum, and Desulfuromonas. A large amount of relatively low abundance microorganisms (<0.5%) was enriched in GDM systems, like Porphyrobacter 333 334 (4.8-32.8%), Roseovarius (7.0-23.2%), unclassified_f_Rhodobacteraceae (0.8-33.3%), 335 *SM1A02* (3.6% - 9.4%),*Pyruvatibacter* (0.6% - 13.0%)and Rehaibacterium 336 (0.5-15.2%). Some research showed that members of Porphyrobacter can degrade 337 organics, such as polycyclic aromatic hydrocarbons (Balázs et al., 2020; Fan et al., 338 2016). Roseovarius, as an iodine oxidation bacterium, can promote the formation of 339 large amounts of iodinated organic compounds (Almaraz et al., 2020). 340 Rhodobacteraceae were widely reported in various environments with ability of degrading organic matter and removing nitrogen (Chen et al., 2021; Ma et al., 2020). 341 Some works proved that *Pyruvatibacter* as a halophilic bacterium can degrade 342 343 acetoacetic acid and pyruvate (Wang et al., 2016). Rehaibacterium was reported as a 344 thermotolerant, halophilic, and strictly aerobic bacterium with the function of 345 degrading some organic compounds (Yu et al., 2013).

In this work, O_3 -GDM systems had their own characteristic microorganisms. Specifically, *Porphyrobacter* and *norank_c_Gammaproteobacteria*, were enriched in the two GDM systems treating non-ozonized SGW as feed water. *Thalassospira* (5.0-15.5%), *Pyruvatibacter* (3.2-13.0%), and *Erythrobacter* (7.2-10.9%) were enriched in three of the O₃-GDM systems. It was reported that some species of *Thalassospira* can degrade quaternary ammonium compounds, which are often used as biocides in SGW (Acharya et al., 2020). *Pyruvatibacter* as an aerobic marine

bacterium can degrade some organics, such as pyruvate (Wang et al., 2016). As
aerobic phototrophs, *Erythrobacter* often exist in organic-rich environments, and can
degrade PAHs, one of the main organic pollutants in SGW (Butkovskyi et al., 2017;
Kahla et al., 2021).



357

Fig. 5 Bacterial community compositions at (a) the phylum (> 1%) and (b) the genus

level (> 1.5%) in raw water and on the membrane of the six GDM systems. GDM1,

GDM2, GDM3, GDM4, GDM5, and GDM6 represent control GDM, GGDM,
 O₃²⁰-GGDM, O₃⁴⁰-GDM, O₃⁴⁰-GGDM, and O₃⁸⁰-GGDM units, respectively.

362

363 3.4 Summary on mechanisms and effect of pre-ozonation on GDM systems and 364 desalination

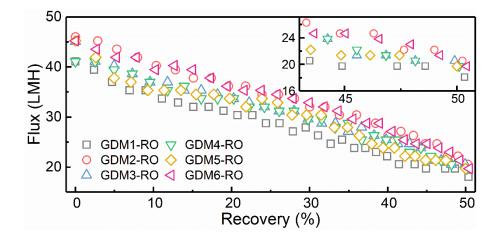
365 The rapid decline of flux in GDM system should be attributed to the blocking of 366 membrane pores by the rapid formation of dense fouling layer (Fig. 1 and Fig. 2). 367 Pre-ozonation significantly increased the initial flux (245%) but deteriorated the 368 quality of effluent water in terms of DOC concentration (-14%) (Fig. 1). These results 369 are mainly attributed to the conversion of macromolecular organics to low fractions by pre-ozonation (Fig. 1 and Fig. 4). EPS played an important role in flux 370 371 development of GDM, and a large number of studies found negative correlation 372 between EPS content and stable flux (Pronk et al., 2019; Tang et al., 2021d). However, 373 some contradictory results were observed in this study. O₃-GDM system had higher EPS concentration compared to GDM (Fig. 3), while the stable flux of O₃-GDM 374 375 system was 3.7 times of GDM. This observation suggests that there were other factors that played roles in stabilizing the flux. Compared with GDM, it was observed that the 376 377 thickness of the fouling layer of O₃-GDM system was thinner, the hydrophilicity of 378 the fouling layer was higher, and biodegradation ability of the fouling layer was 379 enhanced (Fig. 2, Fig. S6, and Fig. 4). All these factors might play a positive function in the improvement of stable flux. However, we hypothesize that the reduction of 380

381 organics molecular size may be the main result of pre-ozonation that increased the382 stable flux.

Compared with GDM, GGDM had higher stable flux (637%), likely because GAC adsorption reduced the concentration of organic matters blocking membrane pores. For GGDM systems, pre-ozonation also markedly increased the flux (198%) in the first month of operation. Pre-ozonation improved the stable flux by reducing organics molecular size and GAC adsorption improved the stable flux by reducing the concentration of organic matters blocking membrane pores, also simultaneously improving the quality of the effluent.

390 The permeate of the six GDM systems was collected and fed individually to the 391 RO system to study the effect of pretreatment on RO performance. The RO flux was 392 higher when treating effluents that were previously ozonized, despite the fact the the 393 DOC level in these streams was not necessarily lower than that from the control 394 system (Fig. 6). Considering that the RO unit was operating in dead-end mode, the 395 observed increase (9%) can be considered significant (Chang et al., 2019a). Some 396 research found that pre-ozonation reduced RO membrane fouling by improving the 397 hydrophilicity of foulants and weakening the adhesion forces between foulants and the membrane and among foulants (Yin et al., 2020a,b). Furthermore, the use of GAC 398 399 significantly increased the flux of GDM-RO (13.6%) and slightly improve the flux of 400 O₃-GDM-RO. GAC adsorption may further reduce RO membrane fouling by decreasing the overall content of organic foulants (Monnot et al., 2017). Table S1 401

402 presents the effluent quality of six GDM-RO systems and indicates that within the 403 range of errors, the water quality of the six systems was almost the same. In general,



404 O₃-GDM outperformed GDM in terms of productivity.

406 Fig. 6 Effect of pretreatments on the RO desalination performance. GDM1, GDM2,
407 GDM3, GDM4, GDM5, and GDM6 represent control GDM, GGDM, O₃²⁰-GGDM,
408 O₃⁴⁰-GDM, O₃⁴⁰-GGDM, and O₃⁸⁰-GGDM units, respectively.

409

405

410 **4. Conclusions**

411 Pre-ozonation was investigated in combination with GAC adsorption and with 412 GDM system to treat SGW. Pre-ozonation changed the properties and molecular 413 weight of organic compounds. Macromolecular organics are oxidized by ozonation to 414 low fractions organics, which have a lower fouling tendency, can more easily pass 415 through the membrane pores, and can be more readily biodegraded the the 416 microorganisms in the fouling layers. At the same time, the decrease of the molecular weight of organic matter also led to the deterioration of the effluent quality of 417 O₃-GDM in terms of organic content. The higher concentration of organic compounds 418

419 in the feed solution and the laerger amount of EPS in the fouling layers of O₃-GDM systems may be the reason why the stable flux of the systems treating ozonized 420 421 effluents without adsorption was lower than that of systems including GAC. A large 422 number of microorganisms with the ability to degrade organics and of denitrification 423 were generally enriched in the membrane fouling layer. The O₃-GDM systems had 424 distinct core microorganisms that may help degrade characteristic organic compounds 425 in SGW, such as quaternary ammonium compounds and PAHs. The contribution of microorganisms in the degradation of organic matter needs further investigation. 426

427 Supporting Information

428 The Supporting Information is available free of charge on the website.

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