

Theory of critical distances: A discussion on concepts and applications

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Theory of Critical Distances: a discussion on concepts and applications

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Abstract:	<p>Theory of Critical Distances (TCD) collects several methods adopted in failure prediction of components provided with stress concentration features. The idea of evaluating stress effect in a zone rather than in a single point was proposed decades ago but, only thanks to relatively recent works, TCD concepts showed to be a successful extension of Linear Elastic Fracture Mechanics (LEFM), able to assess strength and fatigue life. The increasing computational power has made Finite Element Method (FEM) widespread, hence stress fields can be easily extracted and used as input data for fatigue post-processing and durability analyses. In this scenario, TCD reveals as a powerful tool which, thanks to the introduction of a single material parameter (critical distance, L), integrates classical fracture models by considering the presence of microscale phenomena acting in fracture process. In this sense, TCD behaves as a link between continuum mechanics and LEFM. Modalities and reasons for this connection to occur are interesting points of further investigations. Literature on TCD and its theoretical-experimental background is quite extended, nevertheless few industrial applications are available in literature to the best of authors' knowledge. In this paper, an overview of concepts and applications related to TCD are reported highlighting the relevance of theoretical arguments in actual applications.</p>

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Theory of Critical Distances: a discussion on concepts and applications

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C.D. and R.S. contributed to review, editing and supervising.

Abstract

Theory of Critical Distances (TCD) collects several methods adopted in failure prediction of components provided with stress concentration features. The idea of evaluating stress effect in a zone rather than in a single point was proposed decades ago but, only thanks to relatively recent works, TCD concepts showed to be a successful extension of Linear Elastic Fracture Mechanics (LEFM), able to assess strength and fatigue life. The increasing computational power has made Finite Element Method (FEM) widespread, hence stress fields can be easily extracted and used as input data for fatigue post-processing and durability analyses. In this scenario, TCD reveals as a powerful tool which, thanks to the introduction of a single material parameter (critical distance, L), integrates classical fracture models by considering the presence of microscale phenomena acting in fracture process. In this sense, TCD behaves as a link between continuum mechanics and LEFM. Modalities and reasons for this connection to occur are interesting points of further investigations. Literature on TCD and its theoretical-experimental background is quite extended, nevertheless few industrial

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3 26 applications are available in literature to the best of authors' knowledge. In this paper, an overview
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5 27 of concepts and applications related to TCD are reported highlighting the relevance of theoretical
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8 28 arguments in actual applications.
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10 11 29 **1. Introduction**

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14 30 Fatigue assessment in many engineering components is frequently related to the behavior of notched
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16 31 structures. When fatigue life results from a Finite Element Analysis (FEA) post-processing, two kinds
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19 32 of approaches are possible:

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21 33 • Local approaches;
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23 34 • Non-local approaches.

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25 35 Local approaches manage different fatigue life criteria ¹. They focus on the stress state in critical
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28 36 points and can be adopted basing on FEA results. This way, most complex stress distributions and
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30 37 geometries are calculated. By using local approaches for fatigue life assessment, stress gradients
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33 38 effect is weakly taken into account ¹ since fatigue strength at each point is considered independently.

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35 39 Few questions easily arise from this discussion:

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37 40 • What is the effect of surrounding stress state in the study of the fatigue behavior of the hot-
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39 41 spot?
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42 42 • How can stress gradient effect be included in engineering fatigue analyses?

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44 43 Answering these questions is not trivial, however non-local methods proved to be suitable ¹⁻³ when
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46 44 stress gradients are not negligible as it occurs for notched components.

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48 45 Non-local approaches appear as effective tools for stress gradients evaluation ¹; this process performs
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50 46 a stress correction, which considers the entire stress distribution in a limited area.

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53 47 In the field of non-local approaches, Theory of Critical Distances (TCD) ^{1,4,5} finds a wide range of
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55 48 applications in fracture and fatigue life estimation.

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58 49 Theory of Critical Distances is the name **originally** used by Taylor and Susmel ^{4,5} to refer to that group
59
60 50 of theories adopted for the study of stress concentration features. However, the story of TCD started

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3 51 when Neuber understood that fatigue limits of notched elements could only be predicted by averaging
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5 52 the stress state, close to the stress concentration feature, over material characteristic units. From a
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8 53 TCD point of view, this idea results in the so called Line Method (LM), whereas Point Method (PM)
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10 54 stems from Peterson's idea that reference stress for components' strength estimation is located at a
11
12 55 certain distance from the notch ^{6,7}.

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14 56 Over the past decade a considerable literature has grown up around the theme of TCD, as emphasized
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16
17 57 in Fig. 1. Namely, many Authors have developed research branches devoted to theoretical
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19 58 investigations as much as to the enhancement of the fields of TCD application. However, a literature
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21 59 contribution providing a wide-ranging account of the different ramifications in which TCD is
22
23 60 evolving is not currently available. This motivated the Authors of this work to provide this kind of
24
25 61 contribution. Indeed, this work aims to discuss the main TCD concepts and applications which arise
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27 62 from a literature review. In this sense, it is beyond the scope of this work to focus on a specific
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29 63 application, but rather it explores the array of possibilities which have established yet. To this aim,
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31 64 the main TCD notions, initially introduced in the works of Taylor and Susmel ^{4,5,8}, are at first
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33 65 presented. Then, the ever-growing fields of application are discussed together with different
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35 66 interpretations offered by the literature on some issues such as critical distance estimation. This
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37 67 literature portrait is accompanied by considerations which project TCD applications in an industrial
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39 68 analysis context where automatable structural integrity assessments are often performed by means of
40
41 69 commercial fatigue post-processors.

42 68 43 44 45 46 47 48 70 **2. TCD: origins and fundamentals**

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50
51 71 Fatigue notch concentration factor is one of the first parameters analyzed through this approach. It is
52
53 72 well known that notch concentration factor K_t is generally higher than the corresponding fatigue
54
55 73 notch concentration factor K_f . These quantities are related as follows:

$$56 73 \quad q = \frac{K_f - 1}{K_t - 1} \quad (1)$$

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74 To explain this difference, Neuber assumed that the material around the notch can be modelled with
 75 a stack of layers and that each of them, being unable to support stress gradients, is subjected to a
 76 constant stress state. Therefore, the total force can be obtained as the sum of constant stress state
 77 distribution in each layer⁹. By following this hypothesis, it is possible to demonstrate that the stress
 78 in the surface layer (linked to K_f) is lower than the stress coming from the theoretical continuous
 79 curve one (linked to K_t)⁹. If layer thickness is considered material property:

$$K_f = 1 + \frac{K_t - 1}{1 + \sqrt{\frac{A}{r}}} \quad (2)$$

80 where A is a quantity strictly related to the layer thickness and r is the notch radius. We refer to this
 81 example as one of the first attempts at including a material characteristic length in strength
 82 assessment.

83 **2.1 TCD formalization: static**

84 Let us introduce a material property:

$$L = \frac{1}{\pi} \left(\frac{K_{IC}}{\sigma_0} \right)^2 \quad (3)$$

85 where K_{IC} is the material toughness and σ_0 is called “inherent strength”. For ceramics and generally
 86 for brittle materials¹ σ_0 corresponds to UTS (also indicated as σ_u), whereas for ductile materials $\frac{\sigma_0}{\sigma_u}$
 87 > 1 ^{1,5}. In this concept lies one of the degrees of freedom for experimental data correlation since the
 88 value of σ_0 can be seen as a calibrating parameter.

89 It is clear by looking at Eq. (3) that if both L and σ_0 are unknown, it is not possible to estimate L .
 90 Therefore different approaches are adopted in literature. One of them¹ uses a first approximation
 91 value of σ_0 (corresponding to UTS) to perform an analytical estimation of K_{IC} by using TCD. Then,
 92 the experimental value of K_{IC} is compared with the analytical one searching for the value of L which
 93 better fits data. Finally, the ratio σ_0/σ_u is defined. Through this approach, according to Taylor⁸, no
 94 physical meaning is assigned to σ_0 . Strictly speaking, σ_0 is certainly a stress but it refers to elastic
 95 properties in a region where plasticity could be involved. Indeed, the value of σ_0 was found to be

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3 96 even two or three time higher than σ_u in materials where plasticity was the main toughening
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6 97 mechanism, whereas, unitary value were attributable to the ratio σ_0/σ_u when plasticity did not play
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8 98 a key role in the fracture process. According to Taylor ⁸, this is explainable by the fact the mechanism
9
10 99 involved in the fracture of plain specimen is slightly different from that of notched ductile
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13 100 components.

15 101 **2.2 TCD formalization: fatigue**

17 102 However, in many applications, especially in the field of fatigue, the first approximation inherent
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20 103 strength is employed as the number of parameters influencing it becomes larger. One of all is the
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22 104 number of cycles to failure N_f .

24 105 Fatigue equivalent of Eq. (3) is Eq. (4).

$$27 \quad L = \frac{1}{\pi} \left(\frac{\Delta K_{th}}{\Delta \sigma_0} \right)^2 \quad (4)$$

30 106 The threshold intensity factor is ΔK_{th} , $\Delta \sigma_0$ is the inherent strength of the material that in general
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33 107 corresponds to the fatigue limit. L values from Eq. (3) and Eq. (4) are the scale lengths used to
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35 108 introduce four different TCD approaches. These methodologies, initially reported by Taylor ⁸, found
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37 109 a wide range of application in many structural integrity problems which will be presented and
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40 110 discussed in Section 3. Static and fatigue analyses may be carried out by referring to the
41
42 111 corresponding L .

44 112 **2.3 Point Method (PM) and Line Method (PM)**

46 113 The Point Method (PM) relies on the assumption that reference stress to account for failure
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49 114 assessment is located at a distance $r = \frac{L}{2}$ from the notch. This fact results evident by linking TCD to
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52 115 LEFM. It is considered a sharp notch whose behavior is comparable to cracks' one. Stress curve close
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54 116 to crack tip is expressed as ($r \ll a$):

$$56 \quad \sigma(r) = \sigma \sqrt{\frac{a}{2r}} \quad (5)$$

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3 117 Failure condition is reached when nominal stress σ , far from crack, equals fracture stress σ_f . In this
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6 118 circumstance, there will be a distance r for which $\sigma(r) = \sigma_0$. Eq. (5) therefore becomes:

$$\frac{\sigma_0}{\sigma_f} = \sqrt{\frac{a}{2r}} \quad (6)$$

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11 119 Fracture stress σ_f is known from LEFM:

$$\sigma_f = \frac{K_{IC}}{\sqrt{\pi a}} \quad (7)$$

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16 120 Then, by substituting Eq. (7) and Eq. (3) in Eq. (6), it appears that: $r = L/2$. Thus, the occurring link
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19 121 between TCD and LEFM provides a possible interpretation of PM.

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21 122 Line Method (LM) is similar to PM but stress distribution is averaged over a length $r = 2L$. In this
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23 123 case, a PM-like explanation is achieved by performing stress field integrations and searching for the
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25 124 length at which the averaged stress equals σ_0 (incipient failure). By extending these concepts to area
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28 125 and volume integrals, Area Method (AM) and Volume Method (VM) emerge as natural
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30 126 consequences. However, PM and LM are mostly applied because of they represent a trade-off
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33 127 between good accuracy and simple use.

34 35 128 **2.4 Imaginary Crack Method (ICM) and Finite Fracture Mechanics (FFM)**

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37 129 Imaginary Crack Method (ICM) assumes that an imaginary crack is placed at the notch root. Failure
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40 130 is assumed to occur when stress intensity factor K reaches material toughness K_{IC} . Then, LEFM
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42 131 concepts are applied to assess fracture behavior.

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44 132 Finite Fracture Mechanics (FFM) does not find actual applications in the industrial world to the best
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47 133 of the authors' knowledge. Nevertheless, according to Taylor ^{1,10} one of the possible explanation for
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49 134 TCD ability to predict failure conditions in notched structures lies in FFM.

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51 135 FFM is essentially a reinterpretation of LEFM in which the mathematical integrations required to
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53 136 express fracture energy are performed in finite steps. The main hypothesis behind this argument is
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56 137 that crack growth occurs discontinuously developing by discrete quanta ¹⁰, namely with a Δa
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58 138 increment rather than a da . This is not unrealistic if we think of microstructural obstacles as
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60 139 discontinuity factors. By applying these concepts ¹⁰ it is possible to demonstrate:

$$\sigma_f = \frac{K_{IC}}{\sqrt{\pi\left(a + \frac{\Delta a}{2}\right)}} \quad (8)$$

Eq. (8) describes fracture stress behavior both in the small cracks and in the long cracks zone, this is not trivial as emphasized in the following.

Let's suppose a crack of length a in a component. Continuum mechanics, as the name suggests, is not able to properly manage discontinuities because of the hypothesis on which it is based. LEFM, on the contrary, uses energy to describe discontinuities such as cracks and can predict failure condition and fracture stress by using Eq. (7). **This way, singularities such as cracks can be managed.**

If crack length changes, σ_f varies as well because an energy-based criterion is adopted and fracture is supposed to be K -governed. **Instead**, if there were no crack or a small one, a stress-based approach would be used, since failure would be defined by using the critical stress as threshold quantity ($\sigma_f = \sigma_0$). **Indeed, this corresponds to the classic engineering failure approach which limits the allowable**

stress conditions to assess structural integrity of plain specimen. Fracture stress would be, in this case, constant and not influenced by crack length. In the field of fatigue and crack propagation analysis the same considerations may be done by using fatigue limit in place of UTS and ΔK_{th} in place of K_{IC} , as expressed in the Kitagawa-Takahashi diagram ¹¹ (Fig. 2). **This diagram shows the aforementioned concepts. In particular, when crack length decreases, the stress amplitude leading to crack propagation increases according to LEFM. Moreover, the stress-based and the LEFM models intersect in the critical length L , thus defining the region of propagating and non-propagating cracks.**

Short cracks behavior is, in any case, more complex to describe in terms of crack growth because of continuum mechanics limits in modelling entities with the same order of magnitude of microstructure.

FFM, just as PM, LM and ICM, is able to depict the whole range of crack size behavior with Eq. (8).

Indeed the fracture stress behavior of Eq. (8) is retraced by applying PM, LM and ICM as well.

However, this capability is explainable only for FFM since a relation between Δa and L is identifiable.

Indeed, when crack size becomes very small, Eq. (8) turns into:

$$\sigma_f = \frac{K_{IC}}{\sqrt{\pi\left(\frac{\Delta a}{2}\right)}} \quad (9)$$

it is worth noticing that if LEFM alone were applied, Eq. (7) would lead to an infinitely strong material for a close-to-zero crack size. Considering fracture stress equal to inherent strength $\sigma_f = \sigma_0$ in Eq. (9):

$$\sigma_0 = \frac{K_{IC}}{\sqrt{\pi\left(\frac{\Delta a}{2}\right)}} \quad (10)$$

that turns to be Eq. (3) for $L = \frac{\Delta a}{2}$. This provides an interpretation of the occurring relation between FFM and TCD.

This is one of the examples from which the link between LEFM, microstructural mechanisms (represented by discrete quanta Δa) and TCD emerges, **candidating TCD as a more general fracture theory which embraces several multi-scale aspects.**

One of the TCD limits, **highlighted by Taylor^{8,10}**, may be emphasized in this point. Whenever component characteristic dimensions become comparable with critical distance value, FFM is modeling a crack that is passing through the whole component that, consequently, will be predicted to be infinitely unable to support stress. LM, on the contrary, is averaging stress over the entire component, resulting in a quasi-zero averaged stress. In this case, LM would model a component infinitely able to support stresses. Therefore, LM and FFM assessments would diverge and combined methods (LM+FFM) would be necessary¹⁰. Hence, when component characteristic dimensions become comparable with critical distance value, both LM and FFM collapse and only combined methods are applicable.

Recently, Liu et al.¹² handled the coupled approaches to estimate fatigue limits of notched specimens. Namely, it was concluded that for blunt notches the difference between LM and LM+FFM estimations is insensitive to notch radius. Conversely, for sharp notches the variability is appreciable but, especially for very sharp notches, it is negligible from an engineering point of view. Then, Naimark¹³ analyzed the variety of crack paths from a FFM point of view.

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3 185 It results clear that LM and PM are stress based methods whereas ICM and FFM are energy-based
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5 186 methods directly coming from LEFM. In most common fatigue post-processors, critical distance
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7 187 methods are implemented in form of PM and LM as stresses coming from FEA are ready to use for
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10 188 this kind of approaches. To the best of the authors' knowledge, FFM and ICM are not currently
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12 189 implemented in commercial fatigue post-processor. Therefore, in an industrial context their
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15 190 application is bounded by the possibility of developing own codes.
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18 191 **3. TCD in Multiaxial Fatigue**

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21 192 In many applications ^{2,14-17} multiaxiality of loads affects fatigue behavior. The problem of TCD
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23 193 implementation in these problems has been addressed by several authors.

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25 194 As in static conditions, multiaxial fatigue criteria assume that an equivalent stress to compare with
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28 195 uniaxial material properties can be found in order to solve complex stress states. Since fatigue damage
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30 196 is related to a localized plasticity, yield criteria were originally introduced also in fatigue analyses
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32 197 and equivalent stress amplitudes were originally defined by combining principal stresses amplitudes
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35 198 ¹⁸.

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37 199 However, stress variability in time is what distinguishes fatigue from static failure. This adds some
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39 200 complexities since stresses are essentially vectors and their direction becomes an influent parameter
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42 201 in fatigue analyses.

43 44 202 **3.1 Critical Plane Criteria**

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46 203 In order to take into account this phenomenon, critical plane criteria were introduced. Indeed, when
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49 204 components experience out-of-phase loadings, principal stress directions vary in time even if load
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51 205 directions are constant. In this case, mathematical combinations of principal stress amplitudes may
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53 206 be meaningless. For instance, Gough and Sines methods are static yield criteria ¹⁸⁻²⁰.

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56 207 Then, Findley ²¹ was the first to introduce the concept of critical plane referring to the plane on which
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58 208 a certain damage parameter is maximized. The damage parameter for fatigue crack initiation and
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60 209 growth is usually related to the shear stress/strain amplitude, to the normal stress/strain or, as in the

case of Findley criterion, a combination of these. Brown and Miller developed the same concept in the Low Cycle Fatigue (LCF) regime²². The applicability of these criteria in the form of local approach in actual automotive applications has been proved yet^{23,24}.

However, in the most general cases, the maximum shear stress plane may be different in each instant because of principal stresses directions relocation. The computation of shear stress amplitude in a specific plane is not always a simple task. The longest chord method, longest projection method, minimum circumscribed circle method^{25,26} are among the most used algorithms for the determination of the shear stress amplitude starting from the path described by the resolved shear stress vector. In the last decade, Susmel²⁷ proposed an algorithm based on the Maximum Variance Method (MVM) whose numerical advantage lies in the time needed to calculate the critical plane as it does not depend on the stress history length. As suggested by the name, MVM acts by searching for the plane experiencing the maximum variance of the resolved shear stress. Moreover, Constant Amplitude (CA) and Variable Amplitude (VA) time histories can be treated in the same manner.

3.2 Modified Wöhler Curve Method (MWCM)

In order to apply TCD to multiaxial fatigue, Susmel and Taylor^{14,16} proposed a methodology for implementing the MWCM along with TCD with the aim of estimating fatigue failure of notched components under VA and CA loadings. Remarkably, this can be applied both in the case of in phase and out-of-phase stress histories. In many of the presented applications the conjunction between MWCM and TCD showed to be a powerful tool for multiaxial fatigue assessment. Therefore, a short account of this methodology is reported in the following.

In a CA case, once the critical plane is defined as the maximum shear stress amplitude plane, it is defined the stress ratio:

$$\rho_{eff} = \frac{m\sigma_{n,m} + \sigma_{n,a}}{\tau_a} \quad (11)$$

where m is the mean stress sensitivity and it is defined as a material constant, $\sigma_{n,m}$ is the mean normal stress acting on the critical plane, $\sigma_{n,a}$ and τ_a are the normal stress amplitude and the shear stress

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234 amplitude computed on the critical plane. By using Mohr's circles, it is simple to show that ρ_{eff} may
235 vary between 0 and 1 respectively in a fully reversed torsion and fully reversed uniaxial loading case.
236 It is also assumed that a threshold value ρ_{lim} actually exists in order to model the change in the
237 physical phenomena behind crack initiation¹⁶ process.

238 In the medium-high cycle range ρ_{eff} contains the information about multiaxiality and, as reported in
239 Eq. (12) and Eq. (13), it is used to modify the fully-reversed torsion Wöhler curves. The slope k_τ and
240 the reference stress $\tau_{A, ref}$ at N_A cycles change through linear laws and their values are obtained
241 interpolating between the fully-reversed tension and the fully-reversed torsion conditions:

$$k_\tau = a\rho_{eff} + b \quad (12)$$

$$\tau_{A,ref} = c\rho_{eff} + d \quad (13)$$

242 where a, b, c, d are material constants that can be calculated, for instance, from fatigue properties at
243 $\rho_{eff} = 1$ and $\rho_{eff} = 0$.

244 The notch bisector is taken as focus path and the critical plane shear stress amplitude τ_a is computed
245 by a linear-elastic FEA as a function of r , distance from the hot-spot.

246 Since τ_a depends on the coordinate r , the number of cycles to failure N_f is computed as a function of
247 r :

$$N_f(r) = N_A \left[\frac{\tau_{A,ref}(\rho_{eff})}{\tau_a} \right]^{k_\tau(\rho_{eff})} \quad (114)$$

248 PM and is adopted together with the hypothesis that L depends on N_f with a power law :

$$r = \frac{AN_f^B}{2} \quad (15)$$

249 where A and B are calibrating constant. The point on the focus path for which Eq. (16) is solved:

$$\frac{AN_f(r)^B}{2} - r = 0 \quad (16)$$

250 represents the coordinate at which the reference stress, according to TCD, is located and from which
251 number of cycles to failure is estimated.

It is clear that, in a VA case, this methodology needs some corrections since stress history will contain more than a single τ_a and a cycle counting method (e.g. Rainflow) must be adopted.

Critical plane is identified through MVM²⁷, whereas Rainflow²⁸ may be adopted to extract several τ_a experienced by the component for a number of cycles n . For each $\tau_{a,i}$, a number of cycles to failure $N_{f,i}$ is estimated and cumulative damage D_{tot} is computed.

$$\sum_{i=1}^j \frac{n_i}{N_{f,i}} = D_{tot} \quad (1712)$$

$N_{f,eq}$ is then estimated:

$$N_{f,eq} = \frac{n_{tot}}{D_{tot}} \quad (1813)$$

where n_{tot} is the sum of the extracted n_i .

As in the CA case, $N_{f,eq}$ is a function of the coordinate r and, by using PM, the reference stress point is found:

$$\frac{AN_{f,eq}(r)^B}{2} - r = 0 \quad (19)$$

In this procedure it is implied a unitary critical cumulative damage. Calibrating constants can be added to consider the variability of the critical damage sum that will lead component to failure.

4. Applications of TCD

TCD applicability field is not restricted to notched components: examples of its use are found in the study of fretting fatigue^{2,3}. In this context, the so called “notch analogue”^{2,3,29} is noteworthy: this term refers to similarities of stress states both around notches tip and contact surfaces in fretting fatigue. This is the starting point for applying the same fatigue concepts in two apparently different situations linked by the presence of a multiaxial stress state. Indeed Kouanga et al.² studied the crack initiation process in fretting fatigue loadings by using TCD. In this case, TCD showed to be able to predict finite lifetime in metals subjected to Constant Amplitude (CA) loads. In this case, the use of linear-elastic FE models and multiaxial fatigue analyses paved the way for a design methodology suitable for real mechanical components subjected to fretting fatigue loadings. Then, Zabala et al.³⁰

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3 273 adopted a mesh control approach to analyze fretting fatigue from a TCD point of view. This resulted
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5 274 in a reduction of the simulation time with respect to the original TCD. Indeed, the use of FE models
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8 275 in conjunction with TCD concepts call for attention on the relation between mesh refinement and the
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10 276 size of the area in which stresses are averaged. The mesh control approach works on element sizes
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12 277 relatable to L in such a way that the stress calculated in the hot spot retraces the one of TCD. In this
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15 278 way, the computational time related to small element sizes is reduced. Recently, Pinto et al. ³¹
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17 279 investigated the problem of fretting fatigue in aeronautical Al 7075-7651 alloy proposing a life
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19 280 assessment procedure which involved TCD. This contribution introduced the possibility of
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22 281 estimating fretting fatigue life under variable amplitude load conditions which included wear effect.
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24 282 TCD has not to be addressed to as a static or fatigue failure criterion itself but as a standpoint from
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26 283 which most of fatigue life criteria may be applied. Indeed, in the case of fretting fatigue, Araújo et al.
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28 284 ³ compared two different multiaxial critical plane criteria ¹⁸ using them both in form of local and non-
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31 285 local (TCD) approach. In particular, the mesoscopic scale Dang Van criterion ³²⁻³⁴ and the Modified
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33 286 Wöhler Curve Method (MWCM) ^{14,16} applied along TCD exhibited their capability to predict size
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35 287 effect. In this case, MWCM revealed to be a more accurate critical plane criterion. Moreover, it was
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38 288 emphasized the noteworthy advantage of achieving promising results by simply post-processing
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40 289 linear-elastic FE analyses thanks to the use of TCD ³⁵. This feature broadens the applicability of TCD
41
42 290 in estimating fatigue strength of real mechanical assemblies. Critical distance application along with
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45 291 critical plane analysis was further investigated in multiaxial fatigue by Liao et al. ³⁶. It was found that
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47 292 better accuracy may be achieved if critical plane analysis is applied before TCD. Similarly, a
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49 293 combined critical distance/plane approach was employed for predicting fatigue crack initiation in
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51 294 superalloy components ³⁷.
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54 295 In recent times, then, TCD found application in random fatigue assessments. Luo et al. ^{38,39} proposed
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56 296 a damage gradient model to estimate fatigue lives of notched metallic components subjected to
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58 297 random biaxial fatigue loadings. The model was further validated by experimental results.
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3 298 Looking at industrial applications, TCD concepts implementation is present in engines durability
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5 299 analyses ¹⁵. In these cases, FEA results, coming from thermal-structural simulations, are post-
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8 300 processed for fatigue life assessment even if complex loading paths and geometries are involved. For
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10 301 instance, Bishop ¹⁵ applied non-local approaches, very similarly to what was later formalized in TCD,
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12 302 to fatigue analyses of the cylinder head and block of automotive engines. Of course, this kind of
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14 303 analyses imply a higher degree of complexity with respect to the study of test specimens. For this
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17 304 reason, a compromise between analysis complexities, theory implications and material behavior
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19 305 model must be found introducing some simplifications.

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21 306 However, some aspects cannot be completely neglected; i.e. by reducing TCD to a simple stress
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24 307 assessment far from hot-spots, TCD ability to predict fatigue behavior of notched components
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26 308 inevitably fails. Certainly, by means of TCD, stress status is investigated in an area and not only in
27
28 309 the stress concentration points, but what is the size of this area? The answer is one of the TCD key
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30 310 points. It depends on material ^{1,4,5} just like Ultimate Tensile Strength (UTS) and Fatigue Endurance
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33 311 Limit and generally cannot be arbitrarily defined to expand components limits of acceptability.

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35 312 Then, TCD applications are present in cast iron components, bones, welded joints ^{40,41}. In this context,
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37 313 Taylor presented several case-studies ^{40,42}. For instance, the improvement of the notch radius in cast
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39 314 iron components did not show fatigue benefits since critical distance value was larger than the radius
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42 315 itself. Further, the relation between notch radius and critical distance was investigated to avoid brittle
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44 316 fracture in bones modified by orthopedic operations. Among biological materials, remarkable
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47 317 considerations were advanced for what concerns eggshells, providing interpretations of commercial
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49 318 interest since many eggs may break prematurely. Taylor et al. ⁴³ measured the fracture toughness of
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51 319 notched eggshells estimating the effect of stress concentration features by means of TCD. Instead,
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53 320 Schimdt et al. ⁴⁴ offered an insight into the toughening mechanisms occurring in insect wings. In this
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56 321 study, TCD showed capable to assess crack growth and crack arrest, laying the foundation to
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58 322 investigate crack-resistant materials for engineering applications in a TCD perspective.
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3 323 Then, in welded joints applications, the use of TCD allows to FE model a null notch radius without

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5 324 affecting the results as long as the radius real value is smaller than L . More recently, Fang et al. ⁴⁵

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7 addressed the problem of stress concentration in wind-induced fatigue assessment of welded

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9 325 structures by adopting TCD. This study confirmed TCD reliability in this field of application.

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11 326 High level of accuracy were obtained in the cases of torsional fatigue ⁴⁶, aluminum tubular beams ⁴⁷

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13 327 and environmentally assisted cracking ^{48,49} (EAC). Guitérrez et al. ^{48,49} analyzed EAC process in

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15 328 notched steel specimen by means of PM. In this context, TCD was successfully applied to analyze

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17 329 Hydrogen Embrittlement conditions which caused cleavage-dominated fracture micromechanisms.

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19 330 Then, notch effect was observed in Stress Corrosion Cracking (SCC) and it was effectively predicted

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21 331 by means of TCD ⁵⁰. Next, PM and LM accuracy was emphasized in estimating fatigue lives of high-

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23 332 strength steel wires with corrosion pits ⁵¹.

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25 333 Also, Critical Distance approaches were applied to the study of the fracture behavior of rocks. Cicero

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27 334 et al. ⁵² investigated the notch effect on biotite granite and oolitic limestone through an experimental

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29 335 campaign involving 84 notched specimen tested in 4-points bending. The TCD approach revealed

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31 336 defect sizes much smaller than L to be harmless and a good agreement between critical distance

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33 337 estimation and experimental evidence was achieved. Similar results were obtained on different type

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35 338 of rocks such as Carrara marble ⁵³. More recently, Justo et al. ⁵⁴ analyzed the fracture behavior of

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37 339 rocks subjected to Mode I loads in different temperature conditions. Interestingly, temperature

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39 340 influenced material toughness but had not clear effect on critical distance. *Instead*, the effect of

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41 341 temperature on metallic materials was studied by Louks and Susmel ⁵⁵. In this case, TCD showed to

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43 342 be successful in estimating high-cycle fatigue strength at elevated temperatures. The remarkable

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45 343 advantage of modeling the non-linear behavior of metals subjected to high temperature with a linear

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47 344 elastic stress field stem, even more in this context, as one of the main TCD benefits. Also at high

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49 345 temperature, the notch geometry showed to have no influence on critical distance values. However,

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51 346 the effect of geometry on L is one of the main issue which emerges from literature, since some

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53 347 research activities are devoted to the development of notch-dependent critical distances. The

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3 349 variability of L with the number of cycles to failure has been discussed as well ^{14,56}. A more in-depth
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5 350 discussion of this topic is provided in Section 4.

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8 351 Applications are also found in the field of ceramic materials ⁵⁷ and concrete structures ⁵⁸. In a recent
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10 352 work of Alanazi and Susmel ⁵⁸, TCD linear-elastic modeling was proficiently applied in notched un-
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12 353 reinforced concrete subjected to mixed mode static and dynamic loadings.

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15 354 Further research projects are devoted to the study of notch fatigue in additively manufactured
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17 355 materials ⁵⁹ and 3D printed components ⁶⁰. Benedetti and Santus ⁵⁹ employed critical distance
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19 356 approaches for the fatigue analysis of Ti-6-Al-4V additively manufactured via selective laser melting.

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22 357 In this case, defects strongly affect the fatigue behavior and TCD efficacy is linked to the knowledge
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24 358 of the actual defectiveness. The work of Ahmed ⁶⁰ investigated the static strength of Polylactic acid
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26 359 (PLA) notched components obtained by means of fused deposition modeling. The application of

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29 360 TCD concepts showed to be promising, estimating static strength within +/-20% error range. Fatigue
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31 361 strength of PLA was investigated by Ezeh and Susmel ⁶¹. This work showed that, in 3D-printed
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33 362 polymers, fatigue cracks follow irregular paths which retrace the orientation of the extruded filaments.

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36 363 Besides, TCD exhibited its capabilities to assess notch fatigue strength. The same considerations were
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38 364 advanced thanks to the study of the static strength of ABS ⁶². Overall, good experimental agreement
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40 365 was achieved by applying TCD to polymers, such as PMMA ⁶³.

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43 366 Composite materials were analyzed from a TCD perspective as well. Namely, the structural integrity
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45 367 of short glass fiber reinforced polyamide 6 (SGFR-PA6) was investigated basing on Failure
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47 368 Assessment Diagrams ⁶⁴ and LM stress corrections. Whereas, Nguyen-Hoang and Becker explored
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49 369 the behavior of composite bolted joints for aeronautical applications ⁶⁵.

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52 370 Next, fracture toughness was analyzed from a TCD point of view ⁶⁶, apparent fracture toughness of
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54 371 notched structures was investigated by Cicero et al. ⁶⁷ and, more recently, Taylor provided an
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56 372 interpretation of the multiscale toughening mechanism relying on TCD concepts ⁶⁸.

5. Remarks on Critical Distance

It was introduced a scale length whose ability of predicting fatigue failure was widely proved^{1-3,14,16}. Actually, explaining the meaning of this length is not straightforward. Thanks to FFM, L was related to crack growth discrete quanta but its correlation with fracture mechanism is not fully assessed. Critical distance can be considered as a good working tool but how to relate it to other fracture theories? Different interpretations come out of this discussion¹.

5.1 Physical interpretations of critical distance parameter

For instance, process zone models^{1,69,70} represent fracture nonlinearities by entrusting this task to special stress-displacement curves which model material behavior close to stress concentrations features. The zone in which these properties are assigned is the so-called “process zone”. Interestingly, a close correlation of the size of this zone with critical distance is recognizable.

Then, fracture statistical models⁷¹ link probability of failure to material constants. Weibull model is one of these:

$$P_f = 1 - e^{\left(-\frac{\sigma}{\sigma_m}\right)^b} \quad (2014)$$

where P_f is the cumulative probability of failure, the ratio $\frac{\sigma}{\sigma_m}$ is descriptive of how much the component is stressed (σ) in relation with its strength properties (σ_m) and b describes how much stochastic phenomena affect strength.

When b is very large, stress state at the hot-spot is alone responsible for component failure, on the other hand low values of b indicate that failure process involves a wider material volume, since probability of failure is significant also far from hot-spots. This concept, as suggested by Taylor¹, sounds very similar to what happens when critical distance argument is applied.

Then, microstructure properties⁷², such as grain size, appear closely related to critical distance values. The presence of an intrinsic material length is detectable in other fracture theories such as Gradient Mechanics models^{73,74} that may themselves be related to TCD.

5.2 Critical Distance Estimation

In light of these ideas, it is clear that a practical application of TCD requires an estimation methodology for L . Basically, by using Eq. (3) or Eq. (4), critical distance estimation calls for the knowledge of two different material properties. However, two main issues arise: the first is related to the fact that ΔK_{th} may be difficult to measure⁷⁵, the second concerns the use of σ_0 . Indeed, for some materials the value of σ_0 corresponds to UTS or, equivalently, to the fatigue limit in the cycling loading case. Nevertheless, being σ_0 physical significance strictly related to whether plasticity phenomena are involved in fracture process, it should be considered as a dependent variable coming from L and ΔK_{th} or K_C .

Following TCD main assumptions, L is considered a material constant in most of the methodologies adopted for its estimation^{2,75-79} and this is explainable by the following. If it is reasonable to link L to microstructure, no geometry effect is expected to influence L since TCD itself, as a more inclusive interpretation of LEFM, should be able to predict size effect rather than be affected by that. Nevertheless, in some cases theoretical constraints can be relaxed to allow mathematical models to fit physical reality, especially in practical applications.

On the other hand, Wang et al.⁸⁰ obtained a higher accuracy level by modifying PM and LM to consider critical distance geometry effect in Ti-6Al-4V.

Moving on to the substance, critical distance estimation is obtained from the post-processing of the linear elastic stress field by using PM. The procedure is applied to a notched component of which a FEM model is built for stress field extraction (Fig. 3).

L can be computed for any number of cycles to failure. Essentially, the plain and the notch fatigue curves are employed. From the latter it is extracted the $\Delta\sigma_{nom}$ at the given N_f , whereas $\Delta\sigma_1$ is extracted from the first curve. Then, literature on TCD suggests a sharp notch to be employed⁷⁵ for critical distance estimation. The stress field resulting from the application of $\Delta\sigma_{nom}$ is studied along the “focus path” represented by the notch bisector. According to PM, this condition of incipient failure

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3 421 occurs when, at a certain distance from stress concentration feature ($r = L/2$), linear elastic stress $\Delta\sigma$
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5 422 equals inherent strength $\Delta\sigma_1$. Then, the coordinate r for which the linear elastic stress-distance curve
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8 423 has the value of $\Delta\sigma_1$ is $r = \frac{L}{2}$ and L may be extracted.
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11 424 Referring to Fig. 3, the computational problem related to mesh size has not to be neglected since L
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13 425 should be considerably greater than the element size⁸¹. Indeed, Braun et al.⁸² analyzed the mesh
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15 426 requirements for stress gradients methods.

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18 427 However, two different notch geometries exhibit two different critical distance values when the
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20 428 presented procedure is applied because different sharpness corresponds to different stress gradients.

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22 429 As a matter of fact, this seems to endorse the existence of a possible geometry effect on L . For sake
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25 430 of TCD generality, it should be accepted that, when plasticity phenomena are involved in fracture
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27 431 process, inherent strength cannot be assessed a priori, as it is not always true that it coincides with
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29 432 fatigue limit (or UTS in static loadings). Therefore, two notches with different levels of sharpness
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31 433 (e.g. sharp and blunt notches) may be used (Fig. 4)¹⁷. Figure 4 shows the stress curves resulting from
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34 434 the application of $\Delta\sigma_{nom}$ to blunt and sharp notched specimen. Therefore, the value of $\Delta\sigma_0$ is assessed
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36 435 on the basis of the intersection between different curves. This way, it is searched for the combination
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39 436 of the parameters L and $\Delta\sigma_0$ which are invariant with respect to notch geometry.

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41 437 The inherent strength value now acts as a calibrating constant thanks to which the same critical
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43 438 distance for both geometries is found, canceling any geometry effect.

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45 439 A different approach is followed by Yang et al. in the study of DS superalloy⁸³ where authors found
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48 440 non-constant critical distances when standard TCD is applied while the product of K_t and L remained
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50 441 constant.

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53 442 Therefore, conventional TCD was be modified^{80,83} by introducing K_t and by considering a new
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55 443 critical distance value:

$$L^* = K_t L \quad (21)$$

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60 444 At a fixed number of cycles, experimental evidence of this quantity to remain constant is declared.

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445 Then, notch factor is used as a geometry describer in order to include size effect in critical distance
446 evaluation. Nevertheless, when loads and geometry complexities starts to approach actual industrial
447 applications, K_t definition is not straightforward, especially if multiaxiality is involved. Indeed, even
448 if multiaxiality were solved by equating multiaxial stress state to an equivalent stress, a possible
449 theoretical inconsistency may occur as reported in the following.

450 Principal stresses directions do not remain constant in time when non proportional loadings act on
451 components, and this makes equivalence stress criteria unadvisable for the fatigue assessment ⁸⁴.

452 Critical plane criteria, on the contrary, consider only some stress components related to fatigue crack
453 initiation (e.g. shear stress, normal stress, shear strain, normal strain, and combinations of these) and
454 their variability is studied along precise directions searching for the critical one.

455 Since critical plane criteria are most used in actual industrial applications, by using Eq. (12) it may
456 occur that an equivalence criterion is used for K_t evaluation whereas a critical plane criterion is used
457 for fatigue life assessment. The present authors raise an issue on this point as it may result both in a
458 harmless event and in, at least theoretically, inconsistency. *Moreover, the definition of K_t for
459 components subjected to complex stress states may be different with respect to the adopted standard.
460 In this sense, the definition of a K_t -dependent critical distance may erase the generality of TCD since
461 geometry would affect theory formulation.*

462 However, in the field of automotive industry some research activities are devoted to Variable Critical
463 Distance Methods ⁸⁵, *providing promising results in the field of automotive components design.*

464 *Other works investigated critical distance estimation methods. For instance, Santus et al. ^{75,79,86}*
465 *proposed a refined methodology for critical distance estimation based on the inverse search method*
466 *and they provided a sensitivity analysis based on the specimen geometry. In this method, critical*
467 *distance is estimated considering an, up to this point, unmentioned aspect. By using relatively low*
468 *stress gradients, small variations of the fatigue limit introduce large alterations in critical distance*
469 *value whereas, in sharp notches, contained error on L bring to large error in the reference stress and,*

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consequently, on strength assessment. Moreover correction functions are introduced in ^{75,79}. Then, Benedetti and Santus ⁸⁶ studied the statistical properties of the thus determined critical distance. As earlier anticipated, critical distance can be evaluated for a certain N_f and at least two cycle regimes are necessary to build Eq. (22) which, as often occurs in fatigue problem, is a power law:

$$L = AN_f^B \quad (22)$$

where A and B are material constants that can be tuned by performing suitable experiments ^{16,78}. Then, when critical distance arguments are employed to compare reference stress with allowable stress, the knowledge of L with respect to a prescribed N_f for safety factor computation is enough, but what if N_f were unknown? This is the case of finite life estimation. In this condition the size of the averaged stress zone depends on the number of cycles to failure itself and an iterative process is required. One of the great advantages of Eq. (22) power law ¹⁴ lies in the fact that it makes TCD available in the medium-high cycles regime by using a linear elastic stress field as explained in the following. Given a negative B constant, L increases as N_f decreases following actual alterations that plastic zone around notch tip undergoes when applied load increases. Thanks to these assumptions, cyclic plastic behavior is modelled through a linear elastic field by changing the size of process zone we are looking at ¹⁴. These models lose in accuracy when N_f is lower than $10^3 - 10^4$ cycles since this hypothesis is no more sufficient. In this cases, an elasto-plastic reformulation of TCD is required ^{87,88}. To the best of the authors' knowledge, commercial fatigue post-processors currently do not implement an iterative procedure for L and N_f computation and fixed High Cycle Fatigue (HCF) critical distance is usable. For this reason, fatigue life assessment in terms of number of cycles to failure, for what concerns the medium-high and medium-low cycle regime by TCD, is not possible by using commercial codes. On the contrary, safety factor computation for infinite life is usually available through TCD algorithms since fixed critical distances can be used.

6. Discussion and conclusions

This is the result of the recollecting work performed by the authors in order to link two aspects.

The first is the ever-growing industrial need to develop accurate as much as simple and ready-to-use models for failure prediction in real components, especially if they are subjected to complex load distributions both in space and time. The second is the academic world where theoretical arguments acquire primary relevance. **These aspects are otherwise connected by the necessity of portraying a current frame of TCD applications and implications.**

By analyzing TCD from both points of view, many questions arose.

1. What is TCD? If we were looking for a method suitable for strength assessment in an industrial component, we could propose TCD as a stress evaluation carried out far from hot-spots. As presented in this work, there is something more beyond this simplification. Indeed, it is quite complex to describe cracking micro-mechanism by using equations and it becomes even more difficult to apply those to real cases because microstructure needs to be considered. On the other hand, continuum mechanics models allow us to solve the problem by using stresses, strains and energy as parameters. Explaining the reasons why continuum mechanics shows better accuracy when applied from the TCD point of view is not straightforward. However, if critical distance is actually linked to microstructure, it starts to be clear that we are somehow including micro-mechanism in continuum mechanics models reinforcing them. This candidates TCD as a general fracture theory.
2. What is L and how is it used? It is introduced a material constant that may be linked as much to microstructure as well as to other fracture theories. Practically, this quantity is used to define the size of the zone over which continuum mechanics quantities are averaged. Critical distance measurement may be done in static and cyclic loading conditions. In the second case a distinction between infinite and finite life regime must be done in order to consider the possible variability of L with the number of cycles to failure. Commercial fatigue post-processors bound TCD applicability to a fixed L , allowing Safety Factor computations through

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3 519 critical distance argument but not cycles to failure estimation in the finite life regime. This
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5 520 fact represents a limitation in the industrial world. In fact, Safety Factors estimation in terms
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8 521 of stresses is for sure simpler to correlate with experimental data but this quantity actually
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10 522 represents a measure of what we do not know about physical phenomena occurring in failure
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12 523 process. Consequently, threshold values are defined upon experience. That is, the more our
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14 524 model is good, the more threshold Safety Factor will resemble unitary value. On the contrary,
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17 525 number of cycles to failure can be seen as a measure of what we know, being directly
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19 526 comparable with experimental data. In fact, the prediction of N_f is a more refined information
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22 527 telling us when failure will occur and not simply how much, on the basis of experience, we
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24 528 are far from it. Finally, critical distance estimation problem and its dependence on geometry
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26 529 is an open issue.

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29 530 3. How to apply TCD? Most of the failures occurring in machines are related to fatigue. In the
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31 531 most general, but not unlikely case, multiaxial non-proportional loadings occur. Therefore,
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33 532 critical plane criteria should be applied by considering stress vector paths besides stress
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35 533 values. MWCM is presented as one of the possible methods because it is applicable in the
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38 534 most complex case of a multiaxial loading path with VA non-proportional loadings in the
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40 535 finite life regime.
- 42 536 4. Limitations in the available commercial fatigue post-processors employed in the industrial
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45 537 field narrow TCD applicability in this context.

47 538 TCD fields of application are growing and the accuracy of the method is continuously confirmed.
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49 539 Many works were initially devoted to the study of metallic materials, whereas recent applications
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51 540 investigated additively manufactured materials, polymers and random fatigue loadings. The available
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54 541 literature offer an insight into several issues regarding critical distance. In particular, several studies
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56 542 which considered complex mechanical assemblies, such as in the field of automotive industry,
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58 543 developed their considerations on the variability of critical distance with geometry. On the other hand,
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60 544 although the problem of notch geometry is deeply discussed in literature, critical distance variability

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3 545 is mainly studied with respect to material properties, temperature conditions and number of cycles to
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5 546 failure but geometry effect on material strength is expected to be assessed by means of L rather than
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8 547 the opposite. This is reasonable if TCD generality as fracture theory is embraced, since it is expected
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10 548 a more inclusive fracture model by introducing a material property linked also to microstructure. In
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12 549 this sense, TCD proposes itself as a link between micromechanical models and continuum-mechanics
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15 550 models.

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17 551 Then, a growing research body is moving in the direction of TCD issues related to FE modeling.
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19 552 This could be an interesting point for the full implementation of TCD in fatigue post-processors.
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22 553 Although the computational power is always increasing, the problem of mesh refinement with respect
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24 554 to critical distance values is indeed not negligible.

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26 555 The validity of TCD is somehow being undermined by component dimensions. Therefore, the
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29 556 application of these concepts to micromechanical components, such as MEMS, is still challenging
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31 557 and proposes itself for future developments.
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33 34 558 **References**

- 35
36
37 559 1. Taylor D. *The Theory of Critical Distances: A New Perspective in Fracture Mechanics*. 2007.
- 38
39 560 2. Kouanga CT, Jones JD, Reville I, et al. On the estimation of finite lifetime under fretting fatigue
40 561 loading. *Int J Fatigue*. Epub ahead of print 2018. DOI: 10.1016/j.ijfatigue.2018.03.013.
- 41
42 562 3. Araújo JA, Susmel L, Taylor D, et al. On the prediction of high-cycle fretting fatigue strength: Theory
43 563 of critical distances vs. hot-spot approach. *Eng Fract Mech*. Epub ahead of print 2008. DOI:
44 564 10.1016/j.engfracmech.2007.03.026.
- 45
46 565 4. Susmel L. The theory of critical distances: a review of its applications in fatigue. *Eng Fract Mech*
47 566 2008; 75: 1706–1724.
- 48
49 567 5. Taylor D. The theory of critical distances. *Eng Fract Mech* 2008; 75: 1696–1705.
- 50
51 568 6. Peterson RE. Notch sensitivity. *Met fatigue* 1959; 293–306.
- 52
53 569 7. Pilkey WD, Pilkey DF. *Peterson's stress concentration factors*. John Wiley & Sons, 2008.
- 54
55 570 8. Taylor D. *The Theory of Critical Distances: A New Perspective in Fracture Mechanics*. 2007.
- 56
57 571 9. Draper J. *Modern metal fatigue analysis*. EMAS publications, 2008.
- 58
59 572 10. Taylor D, Cornetti P, Pugno N. The fracture mechanics of finite crack extension. *Eng Fract Mech*
60 573 2005; 72: 1021–1038.

- 1
2
3 574 11. Richard HA, Sander M. *Fatigue crack growth*. Springer, 2016.
4
5 575 12. Liu Y, Deng C, Gong B. Discussion on equivalence of the theory of critical distances and the coupled
6 576 stress and energy criterion for fatigue limit prediction of notched specimens. *Int J Fatigue* 2020; 131:
7 577 105326.
8
9 578 13. Naimark O. Duality of singularities of multiscale damage localization and crack advance: length
10 579 variety in theory of critical distances. *Frat ed Integrita Strutt* 2019; 13: 272–281.
11
12 580 14. Susmel L, Taylor D. A critical distance/plane method to estimate finite life of notched components
13 581 under variable amplitude uniaxial/multi-axial fatigue loading. *Int J Fatigue* 2012; 38: 7–24.
14
15 582 15. Bishop JE. *Implementation of a Non-Local Critical-Plane Fatigue Analysis Program with Applications*
16 583 *to Cylinder Heads and Blocks*. 2004.
17
18 584 16. Susmel L, Taylor D. The Modified Wöhler Curve Method applied along with the Theory of Critical
19 585 Distances to estimate finite life of notched components subjected to complex multi-axial loading
20 586 paths. *Fatigue Fract Eng Mater Struct* 2008; 31: 1047–1064.
21
22 587 17. Susmel L, Taylor D. The Theory of Critical Distances to estimate the static strength of notched
23 588 samples of Al6082 loaded in combined tension and torsion. Part II: Multi-axial static assessment. *Eng*
24 589 *Fract Mech*. Epub ahead of print 2010. DOI: 10.1016/j.engfracmech.2009.10.004.
25
26 590 18. Socie DF, Marquis GB. *Multi-axial fatigue*. Society of Automotive Engineers Warrendale, PA, 2000.
27
28 591 19. Gough HJ, Pollard HV. The strength of metals under combined alternating stresses. In: *Proceedings*
29 592 *of the institution of mechanical engineers*. 1935, pp. 3–103.
30
31 593 20. Sines G. Behavior of metals under complex static and alternating stresses. *Met fatigue* 1959; 1: 145–
32 594 169.
33
34 595 21. Findley WN. A theory for the effect of mean stress on fatigue of metals under combined torsion and
35 596 axial load or bending. *J Eng Ind* 1959; 81: 301–305.
36
37 597 22. Brown MW, Miller KJ. A Theory for Fatigue Failure under Multi-axial Stress-Strain Conditions. *Proc*
38 598 *Inst Mech Eng* 1973; 187: 745–755.
39
40 599 23. Delprete C, Rosso C. Exhaust manifold thermo-structural simulation methodology. *SAE Tech Pap*.
41 600 Epub ahead of print 2005. DOI: 10.4271/2005-01-1076.
42
43 601 24. Delprete C, Sesana R, Vercelli A. Multi-axial damage assessment and life estimation: Application to an
44 602 automotive exhaust manifold. *Procedia Eng* 2010; 2: 725–734.
45
46 603 25. Bernasconi A, Papadopoulos I V. Efficiency of algorithms for shear stress amplitude calculation in
47 604 critical plane class fatigue criteria. *Comput Mater Sci* 2005; 34: 355–368.
48
49 605 26. Papadopoulos I V. Critical plane approaches in high-cycle fatigue: on the definition of the amplitude
50 606 and mean value of the shear stress acting on the critical plane. *Fatigue Fract Eng Mater Struct* 1998;
51 607 21: 269–285.
52
53 608 27. Susmel L. A simple and efficient numerical algorithm to determine the orientation of the critical
54 609 plane in multi-axial fatigue problems. *Int J Fatigue* 2010; 32: 1875–1883.
55
56 610 28. Matsuishi M, Endo T. Fatigue of metals subjected to varying stress. *Japan Soc Mech Eng Fukuoka,*
57 611 *Japan* 1968; 68: 37–40.
58
59 612 29. Giannakopoulos AE, Lindley TC, Suresh S, et al. Similarities of stress concentrations in contact at
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56 650

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58 651

59

60

round punches and fatigue at notches: Implications to fretting fatigue crack initiation. *Fatigue Fract Eng Mater Struct* 2000; 23: 561–571.

30. Zabala A, Infante-García D, Giner E, et al. On the use of the theory of critical distances with mesh control for fretting fatigue lifetime assessment. *Tribol Int* 2020; 142: 105985.

31. Pinto AL, Cardoso RA, Talemi R, et al. Fretting fatigue under variable amplitude loading considering partial and gross slip regimes: Numerical analysis. *Tribol Int* 2020; 146: 106199.

32. Ballard P, Van KD, Deperrois A, et al. High cycle fatigue and a finite element analysis. *Fatigue Fract Eng Mater Struct* 1995; 18: 397–411.

33. Van KD, Griveau B, others. On a new multiaxial fatigue limit criterion: theory and application. In: *ICBMFF2*. 1989.

34. Hofmann F, Bertolino G, Constantinescu A, et al. Numerical exploration of the Dang Van high cycle fatigue criterion: application to gradient effects. *J Mech Mater Struct* 2009; 4: 293–308.

35. Susmel L, Taylor D. On the use of the Theory of Critical Distances to predict static failures in ductile metallic materials containing different geometrical features. *Eng Fract Mech* 2008; 75: 4410–4421.

36. Liao D, Zhu SP, Qian G. Multiaxial fatigue analysis of notched components using combined critical plane and critical distance approach. *Int J Mech Sci* 2019; 160: 38–50.

37. Leidermark D, Moverare J, Simonsson K, et al. A combined critical plane and critical distance approach for predicting fatigue crack initiation in notched single-crystal superalloy components. *Int J Fatigue* 2011; 33: 1351–1359.

38. Luo Z, Chen H, Zheng R, et al. A damage gradient model for fatigue life prediction of notched metallic structures under multiaxial random vibrations. *Fatigue Fract Eng Mater Struct* 2020; 43: 2101–2115.

39. Luo Z, Chen H, He X. Influences of correlations between biaxial random vibrations on the fatigue lives of notched metallic specimens. *Int J Fatigue* 2020; 139: 105730.

40. Taylor D. Applications of the theory of critical distances in failure analysis. *Eng Fail Anal* 2011; 18: 543–549.

41. Abdulkarim I. *Formalisation of bespoke fatigue approaches to design aluminium-to-steel thin hybrid welded joints*. Doctoral dissertation, University of Sheffield, 2019.

42. Taylor D. Analysis of fatigue failures in components using the theory of critical distances. *Eng Fail Anal* 2005; 12: 906–914.

43. Taylor D, Walsh M, Cullen A, et al. The fracture toughness of eggshell. *Acta Biomater* 2016; 37: 21–27.

44. Schmidt J, O'Neill M, Dirks JH, et al. An investigation of crack propagation in an insect wing using the theory of critical distances. *Eng Fract Mech* 2020; 232: 107052.

45. Fang Z, Li A, Ding Y, et al. Wind-induced fatigue assessment of welded connections in steel tall buildings using the theory of critical distances. *Eur J Environ Civ Eng* 2020; 24: 1180–1205.

46. Susmel L, Taylor D. The theory of critical distances to estimate finite lifetime of notched components subjected to constant and variable amplitude torsional loading. *Eng Fract Mech* 2013; 98: 64–79.

47. Marcos S, Cicero S, Arroyo B, et al. Coupling Finite Element Analysis and the Theory of Critical

- 1
2
3 652 Distances to Estimate Critical Loads in Al6060-T66 Tubular Beams Containing Notches. *Metals*
4 653 (*Basel*); 10.
5
6 654 48. González P, Cicero S, Arroyo B, et al. On the use of the Theory of Critical Distances to predict static
7 655 failures in ductile metallic materials containing different geometrical features. *Eng Fract Mech* 2020;
8 656 78: 1611–1629.
9
10 657 49. González Gutiérrez P, Cicero González S, Arroyo Martínez B, et al. Prediction of crack propagation
11 658 thresholds in notched steels subjected to environmentally assisted cracking: An approach from the
12 659 theory of critical distances. *Mater Des Process Commun* 2019; 1–12.
13
14 660 50. González P, Cicero S, Álvarez JA, et al. Analysis of stress corrosion cracking in X80 pipeline steel: An
15 661 approach from the theory of critical distances. *Procedia Struct Integr* 2018; 13: 3–10.
16
17 662 51. Jie Z, Susmel L. High-strength steel wires containing corrosion pits: stress analysis and critical
18 663 distance based fatigue life estimation. *Fatigue Fract Eng Mater Struct* 2020; 43: 1611–1629.
19
20 664 52. Cicero S, García T, Castro J, et al. Analysis of notch effect on the fracture behaviour of granite and
21 665 limestone: An approach from the Theory of Critical Distances. *Eng Geol* 2014; 177: 1–9.
22
23 666 53. Justo J, Castro J, Cicero S, et al. Notch effect on the fracture of several rocks: Application of the
24 667 Theory of Critical Distances. *Theor Appl Fract Mech* 2017; 90: 251–258.
25
26 668 54. Justo J, Castro J, Cicero S. Notch effect and fracture load predictions of rock beams at different
27 669 temperatures using the Theory of Critical Distances. *Int J Rock Mech Min Sci* 2020; 125: 104161.
28
29 670 55. Louks R, Susmel L. The linear-elastic Theory of Critical Distances to estimate high-cycle fatigue
30 671 strength of notched metallic materials at elevated temperatures. *Fatigue Fract Eng Mater Struct*
31 672 2015; 38: 629–640.
32
33 673 56. Li C, Xie LY, Xie YJ, et al. Calculation of characteristic size and fatigue life of structural members with
34 674 blunt notches. *Eng Fract Mech*; 239. Epub ahead of print 2020. DOI:
35 675 10.1016/j.engfracmech.2020.107310.
36
37 676 57. Taylor D. Predicting the fracture strength of ceramic materials using the theory of critical distances.
38 677 *Eng Fract Mech* 2004; 71: 2407–2416.
39
40 678 58. Alanazi N, Susmel L. Estimating static/dynamic strength of notched unreinforced concrete under
41 679 mixed-mode I/II loading. *Eng Fract Mech* 2020; 240: 107329.
42
43 680 59. Benedetti M, Santus C. Notch fatigue and crack growth resistance of Ti-6Al-4V ELI additively
44 681 manufactured via selective laser melting: A critical distance approach to defect sensitivity. *Int J*
45 682 *Fatigue* 2019; 121: 281–292.
46
47 683 60. Ahmed AA. *The Theory of Critical Distance to design 3D printed notched components*. University of
48 684 Sheffield, 2020.
49
50 685 61. Ezeh OH, Susmel L. On the notch fatigue strength of additively manufactured polylactide (PLA). *Int J*
51 686 *Fatigue* 2020; 136: 105583.
52
53 687 62. Ng CT, Susmel L. Notch static strength of additively manufactured acrylonitrile butadiene styrene
54 688 (ABS). *Addit Manuf* 2020; 34: 101212.
55
56 689 63. Cicero S, Madrazo V, Carrascal IA. Analysis of notch effect in PMMA using the Theory of Critical
57 690 Distances. *Eng Fract Mech* 2012; 86: 56–72.
58
59 691 64. Cicero S, Madrazo V, Carrascal IA, et al. Assessment of notched structural components using Failure
60

1

2

3 692

Assessment Diagrams and the Theory of Critical Distances. *Eng Fract Mech* 2011; 78: 2809–2825.

4

5 693

65. Nguyen-Hoang M, Becker W. Tension failure analysis for bolted joints using a closed-form stress solution. *Compos Struct* 2020; 238: 111931.

6 694

7

8 695

66. Susmel L, Taylor D. The Theory of Critical Distances as an alternative experimental strategy for the determination of K_{Ic} and ΔK_{th} . *Eng Fract Mech* 2010; 77: 1492–1501.

9 696

10

11 697

67. Cicero S, García T, Madrazo V. On the Line Method apparent fracture toughness evaluations: Experimental overview, validation and some consequences on fracture assessments. *Theor Appl Fract Mech* 2015; 78: 15–19.

12 698

13 699

14

15 700

68. Taylor D. Analysis of fracture data from notched specimens can provide information on multiscale toughening mechanisms. *Theor Appl Fract Mech* 2020; 109: 102730.

16 701

17

18 702

69. Barenblatt GI. The formation of equilibrium cracks during brittle fracture. General ideas and hypotheses. Axially-symmetric cracks. *J Appl Math Mech* 1959; 23: 622–636.

19 703

20

21 704

70. Hillerborg A, Modéer M, Petersson PE. Analysis of crack formation and crack growth in concrete by means of fracture mechanics and finite elements. *Cem Concr Res*. Epub ahead of print 1976. DOI: 10.1016/0008-8846(76)90007-7.

22 705

23 706

24

25 707

71. Weibull W. The phenomena of rupture in solids. *Ingeniors Vetenskops Akadamien-Hawdlingar* 1939; 1–55.

26 708

27

28 709

72. Taylor D. The theory of critical distances: a link to micromechanisms. *Theor Appl Fract Mech* 2017; 90: 228–233.

29 710

30

31 711

73. Susmel L, Askes H, Bennett T, et al. Theory of critical distances versus gradient mechanics in modelling the transition from the short to long crack regime at the fatigue limit. *Fatigue Fract Eng Mater Struct* 2013; 36: 861–869.

32 712

33 713

34

35 714

74. Askes H, Livieri P, Susmel L, et al. Intrinsic material length, Theory of Critical Distances and Gradient Mechanics: analogies and differences in processing linear-elastic crack tip stress fields. *Fatigue Fract Eng Mater Struct* 2013; 36: 39–55.

36 715

37 716

38

39 717

75. Santus C, Taylor D, Benedetti M. Determination of the fatigue critical distance according to the Line and the Point Methods with rounded V-notched specimen. *Int J Fatigue* 2018; 106: 208–218.

40 718

41

42 719

76. Pelekis I, Susmel L. The Theory of Critical Distances to assess failure strength of notched plain concrete under static and dynamic loading. *Eng Fail Anal* 2017; 82: 378–389.

43 720

44

45 721

77. Louks R, Askes H, Susmel L. A generalised approach to rapid finite element design of notched materials against static loading using the Theory of Critical Distances. *Mater Des* 2016; 108: 769–779.

46 722

47 723

48

49 724

78. Liu B, Yan X. An extension research on the theory of critical distances for multiaxial notch fatigue finite life prediction. *Int J Fatigue* 2018; 117: 217–229.

50 725

51

52 726

79. Santus C, Taylor D, Benedetti M. Experimental determination and sensitivity analysis of the fatigue critical distance obtained with rounded V-notched specimens. *Int J Fatigue* 2018; 113: 113–125.

53 727

54

55 728

80. Wang J, Yang X. HCF strength estimation of notched Ti–6Al–4V specimens considering the critical distance size effect. *Int J Fatigue* 2012; 40: 97–104.

56 729

57

58 730

81. Vargiu F, Sweeney D, Firrao D, et al. Implementation of the Theory of Critical Distances using mesh control. *Theor Appl Fract Mech* 2017; 92: 113–121.

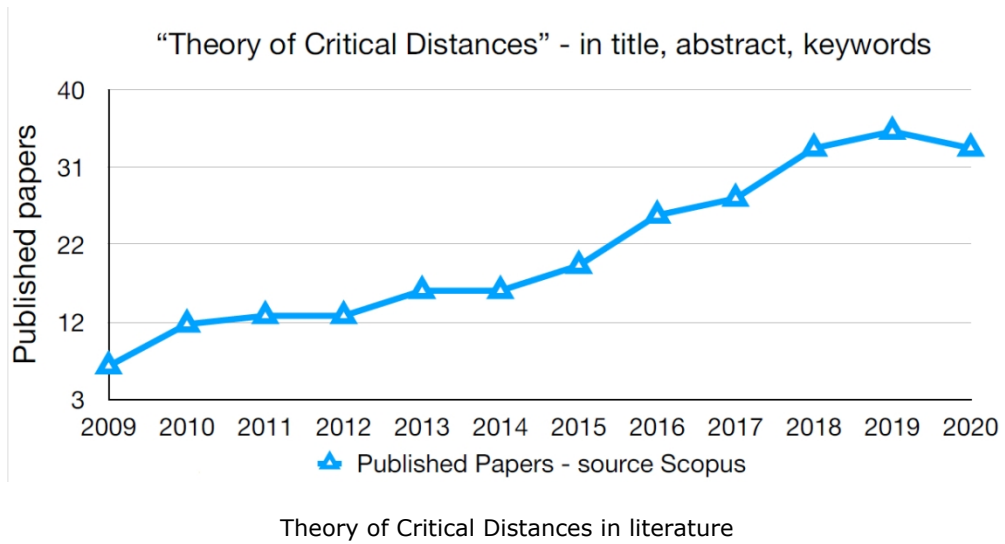
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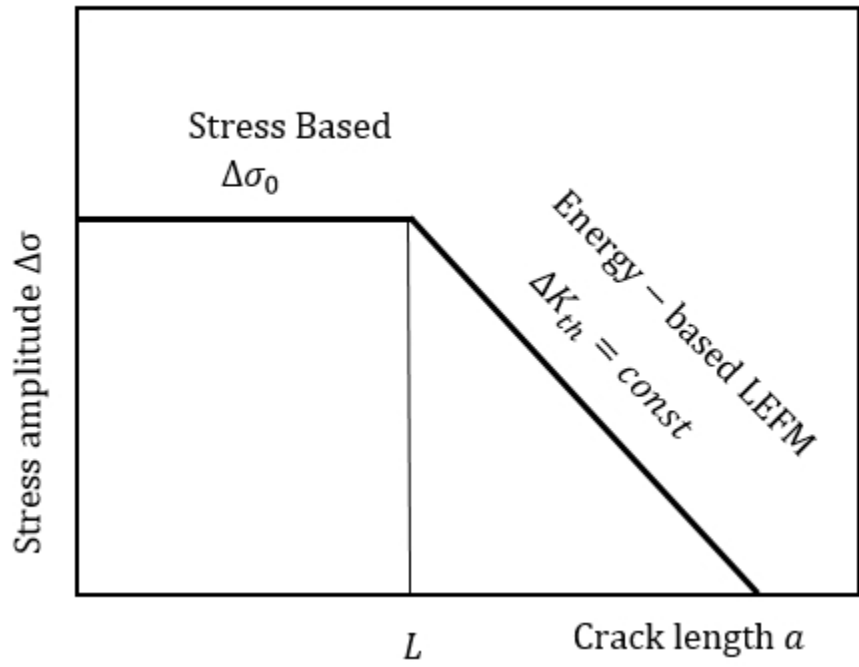
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- 732 82. Braun M, Müller AM, Milaković AS, et al. Requirements for stress gradient-based fatigue assessment of notched structures according to theory of critical distance. *Fatigue Fract Eng Mater Struct* 2020; 1–14.
- 733
734
- 735 83. Yang X, Wang J, Liu J. High temperature LCF life prediction of notched DS Ni-based superalloy using critical distance concept. *Int J Fatigue* 2011; 33: 1470–1476.
- 736
- 737 84. Googarchin HS, Sharifi SMH, Forouzesh F, et al. Comparative study on the fatigue criteria for the prediction of failure in engine structure. *Eng Fail Anal* 2017; 79: 714–725.
- 738
- 739 85. Carpenter N, Jha P, Ray S, et al. Fatigue tests of Un-Notched and notched specimens and life prediction using a variable critical distance method. *SAE Tech Pap*. Epub ahead of print 2019. DOI: 10.4271/2019-01-0801.
- 740
741
- 742 86. Benedetti M, Santus C. Statistical properties of threshold and notch derived estimations of the critical distance according to the line method of the theory of critical distances. *Int J Fatigue* 2020; 137: 105656.
- 743
744
- 745 87. Susmel L, Taylor D. An elasto-plastic reformulation of the theory of critical distances to estimate lifetime of notched components failing in the low/medium-cycle fatigue regime. *J Eng Mater Technol* 2010; 132: 1–8.
- 746
747
- 748 88. Susmel L, Taylor D. Estimating lifetime of notched components subjected to variable amplitude fatigue loading according to the elastoplastic theory of critical distances. *J Eng Mater Technol* 2015; 137: 1–15.
- 749
750
- 751

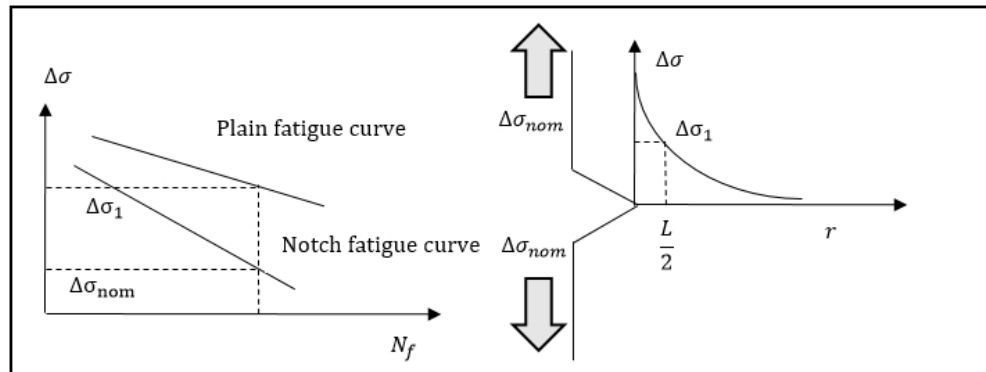
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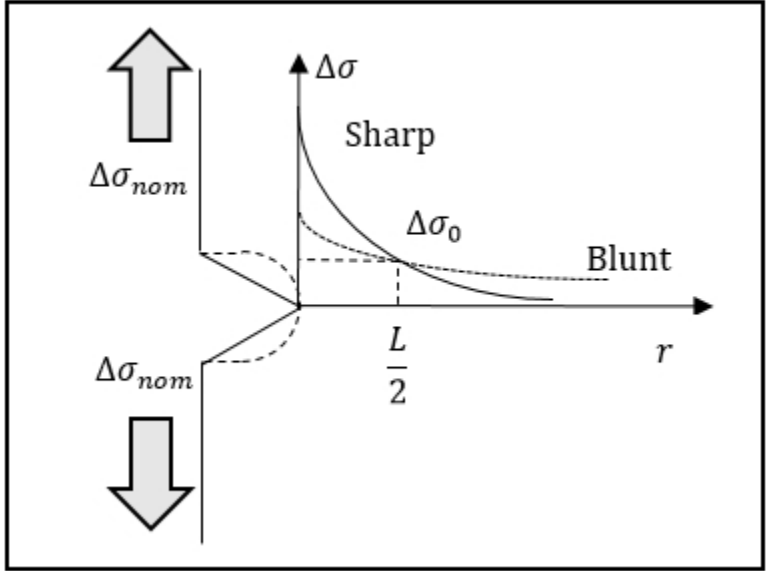


Kitagawa-Takahashi diagram



Critical distance estimation procedure

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Notch sharpness and critical distance estimation