

Flow-seaweed interactions of *Saccharina latissima* at a blade scale: turbulence, drag force, and blade dynamics

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# Reducing inter-pixel crosstalk in HgCdTe detectors

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**Abstract**—Three-dimensional, realistic full-wave electromagnetic and electrical simulations were done considering a planar HgCdTe  $5 \times 5$  pixel miniarray with  $5 \mu\text{m}$ -wide square pixels, illuminated by narrow Gaussian beams. The results suggest that, by avoiding quasi-neutral regions in the detector’s absorber through majority carriers depletion, the inter-pixel crosstalk due to the diffusion of photogenerated carriers is significantly reduced.

## I. INTRODUCTION

The II-VI alloy HgCdTe is one of the most versatile materials for the realization of large format infrared (IR) focal plane arrays (FPAs) [1]. Majority carrier depletion of the absorber was indicated as a method to suppress the dark current originating from quasi-neutral regions, reducing the need of expensive cryogenic cooling systems [2], [3]. We show that carrier depletion is also effective to cut down the diffusive inter-pixel crosstalk [4], [5], a deleterious effect due to lateral carrier diffusion in planar FPAs, particularly relevant when the pixel pitch (often  $3 - 15 \mu\text{m}$ ) is much smaller than minority carriers diffusion length (in the orders of tens of micrometers).

## II. PHOTODETECTOR STRUCTURE

Fig. 1 shows the photodetector structure: it is a planar  $5 \times 5$  pixels miniarray with  $5 \mu\text{m}$ -wide square pixels with  $p$ -on- $n$  doping scheme, consisting in a small modification of a literature example [6], more extensively described in [7]. A narrow-bandgap, low donor-doped and compositionally graded Hg $_{1-x}$ Cd $_x$ Te absorber is connected by two transition layers to two wide-bandgap HgCdTe regions (buffer and cap, Fig. 1(c))

with appropriately chosen doping profile. The absorber’s compositional grading makes the detector suitable for both mid wavelength (MWIR,  $\lambda \in [3, 5] \mu\text{m}$ ) and long wavelength (LWIR,  $\lambda \in [8, 14] \mu\text{m}$ ) operation. The HgCdTe properties were described through the models reported in [4], taking into account the composition, doping, and temperature dependence of the HgCdTe alloy. The Shockley-Read-Hall (SRH) recombination processes were modeled as in [8] considering a lifetime around  $100 \mu\text{s}$ . Fermi-Dirac statistics and incomplete dopant ionization were taken into account.

## III. MODELING METHOD

The geometry, doping and composition profiles were defined employing the Sentaurus three-dimensional (3D) numerical simulator by Synopsys [9], also used to perform the electrical simulations in the drift-diffusion approximation. With reference to Fig. 1(a,b), in the present work we defined the inter-pixel crosstalk as the photoresponse of a neighboring pixel (NNs or CNs) to a beam illuminating the central pixel (CP).

In order to obtain the solution of the electromagnetic problem, we sampled the absorber’s and the transition regions’ composition profiles [7], converting them to staircases of  $N = 30$  sublayers, each with uniform value for the complex refractive index  $n_r + i\kappa$  according to the sublayer’s HgCdTe composition ([4], Table I), as shown in Fig. 1(b,d). With this approach, the EMW commercial simulator [9] was able to solve the electromagnetic problem by a full-wave approach, according to the Finite Differences Time Domain (FDTD) method [10]. The optical generation rate distribution  $G_{\text{opt}}$  into the pixel due to interband optical absorption was inserted as

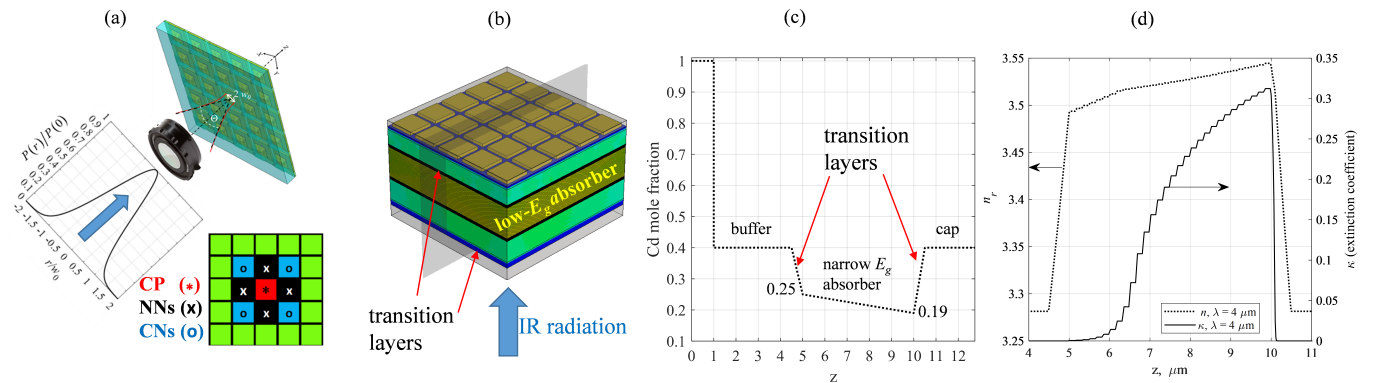


Fig. 1. (a) The 3D miniarray and (b) its Cd mole fraction  $x$  of Hg $_{1-x}$ Cd $_x$ Te profile along  $z$  ( $E_g$  is the bandgap). (c) The discretization of the real  $n_r$  and imaginary  $\kappa$  parts of the absorber’s refractive index profile along  $z$ .

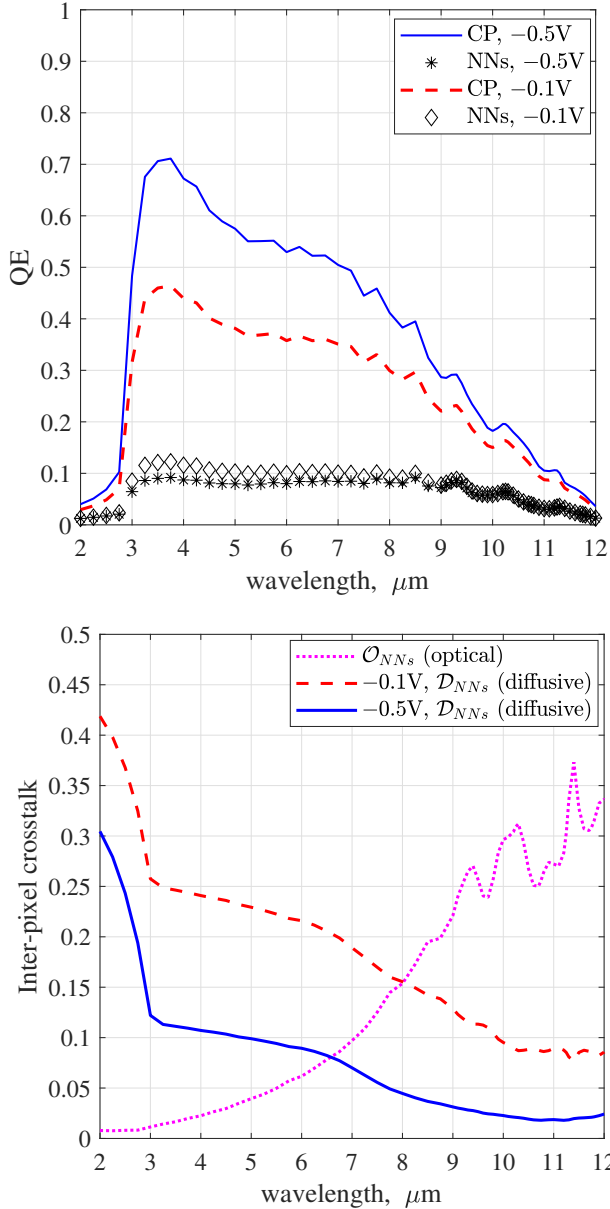


Fig. 2. (a) The CP and NNs spectral QE for the described Gaussian beam illumination centered on the CP, for  $T = 140$  K and  $V_{\text{bias}} = -0.1$  V and  $-0.5$  V. (b) For the same temperature, the “optical” and “diffusive” inter-pixel crosstalk (adimensional ratios) are shown for  $V_{\text{bias}} = -0.1$  V and  $-0.5$  V (the optical crosstalk is bias-independent).

a source term in the drift-diffusion continuity equations after having applied the same reverse bias  $V_{\text{bias}}$  to all the pixels.

#### IV. RESULTS, COMMENTS AND CONCLUSIONS

Fig. 2 shows the spectral quantum efficiency QE and the inter-pixel crosstalk at  $T = 140$  K for  $V_{\text{bias}} = -0.1$  V and  $-0.5$  V for the described illumination, where the definitions for the “optical”  $\mathcal{O}_{NNs}$ , “total”  $\mathcal{C}_{NNs}$ , and “diffusive”  $\mathcal{D}_{NNs}$

contributions to the crosstalk

$$\mathcal{O}_{NNs} = \frac{\int_{V_{NNs}} G_{\text{opt}}(x, y, z) dx dy dz}{\int_{V_{CP}} G_{\text{opt}}(x, y, z) dx dy dz} \quad (1)$$

$$\mathcal{C}_{NNs} = \frac{I_{ph, NNs}}{I_{ph, CP}}, \quad \mathcal{D}_{NNs} \approx \mathcal{C}_{NNs} - \mathcal{O}_{NNs} \quad (2)$$

have been introduced ( $I_{ph}$  is the photocurrent,  $V_{CP}$  and  $V_{NNs}$  are the CP and NNs pixel volumes). By increasing the reverse bias from  $-0.1$  V to  $-0.5$  V, the carrier depletion in the absorber increases significantly, allowing a larger fraction of photogenerated carriers to drift towards the CP contact, before they diffuse laterally: this is pretty apparent comparing the dashed and solid lines in Fig. 2(a,b), referred to  $-0.1$  V and  $-0.5$  V respectively. The moderate electrical field in the absorber that originates from the depletion of the majority carriers is enough to curtail the inter-pixel “diffusive” crosstalk even at moderate reverse bias. Beside the ensuing Auger suppression [3], this is an additional advantage of carrier-depleted detectors. Further investigations will cover the response to non-monochromatic illumination [11], [12], considering different and higher values of temperature, and characterizing the effect of the absorber’s background doping.

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