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Biowaste for SOFCs

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Abstract

Organic Fraction of Municipal Solid Waste was adopted to produce biogas to feed a SOFC generator. Several experimental tests were accomplished on the trace compounds monitoring with PTR-ToF-MS instrument. The main organic compounds detected with the instrument were: sulfurs, terpenes, carboxyls, carbonyls and siloxanes. Coupled to these tests SOFC experiments were accomplished investigating the slipover influence from sorbent materials of sulfurs, chlorines and siloxanes. Limiting factors were evidenced from sulfur, chlorine and siloxane impact on SOFC using an electrochemical impedance spectroscopy (EIS). Tolerable concentration level of single organic compounds appears to be below 1 ppm(v) for H₂S and no concentration is tolerated for siloxanes.

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Keywords: OFMSW, SOFC, PTR-ToF-MS, trace compounds, ashes.

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Nomenclature

AD, Anaerobic Digestion, ASC, Anode Supported Cell, ASR, Area Specific Resistance, D4, OctamethylCyclotetrasiloxane, EIS, Electrochemical Impedance Spectroscopy,	FU, Fuel Utilization, ppm(v), parts per million by volume, SOFCs, Solid Oxide Fuel Cells, TCE, Tetrachloroethylene, TPB, Three Phase Boundary.
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1. Introduction

Biogas from the anaerobic digestion of sewage sludge or organic waste represents a possible way for the biofuel production alternatively to fossil fuels. Anaerobic digestion is a biological process in which biodegradable matter is degraded or decomposed by the activity of specific microorganisms in the absence of oxygen. The resulting biogas

(mainly methane and carbon dioxide) can be used for electricity generation [1]. Organic Fraction of Municipal Solid Waste (OFMSW) offers the possibility to obtain a valuable bio-fuel from a waste that otherwise would be disposed in landfill. Typically, 50-70 % v/v methane, 30-50 % v/v carbon dioxide and trace volatile compounds [2–4]. To meet horizon 2020 requirements is fundamental the coupling between the biogas production and a energy high efficient system. Among many energy generators, Solid Oxide Fuel Cells represent the most promising one, in term of electrical and thermal energy conversion from the raw fuel [5–7]. Fuels however contain minor constituents as impurities. It is mandatory to provide the SOFC energy generator with a gas cleaning section in order to reach the trace compounds requirements [8–10]. Potential technologies for removal of the trace compounds in biogases include various adsorbents [11,12], absorbents [13] and biofilters [14]. Usually, in case of very stringent targets for removal of contaminants (as in case of SOFC), activated carbons are used as sorbent materials, when impregnated with metals, such as iron, copper or chromium [8,9,12]. Despite the gas cleaning section, the trace compound concentrations can be higher due to the slip-over phenomenon. Among trace compounds Sasaki et al., (2011) investigated on the H₂S, PH₃, Cl₂ and D₅ effect on NiScSz anode based fuel cell. The most detrimental compound on SOFCs performance considered in literature works are H₂S and chlorine [15]. As reported by Haga et al., (2008) D₅ was selected as model compound for siloxanes. 10 ppm(v) of D₅ was demonstrated to be fatal on SOFCs performance [15]. No studies were accomplished on siloxanes at ultra-low concentration, even if they seem to strongly influence the cell performance at ppm(v) level [16]. Our goal was to investigate on the cell performance losses related to the different trace compounds concentration contained in a biogenous fuel. A commercial high temperature fuel cell was fed with simulated reformat mixture to which hydrogen sulfide and D₄ were added singularly. Cell performance drop were investigated in galvanostatic mode, and tolerable concentration limits (representing the concentration at which the fuel cell performance are still reversible) were investigated.

Finally, the paper ends with the preliminary investigation on the digestate, adopted as culture medium for the algae growth removing CO₂ from the exhausts of energy generator.

2. Material and methods

The digester pilot plant, located at Foundation Edmund Mach (S. Michele a/A, Italy) was adopted to process the OFMSW, as organic source to produce biogas. Before digester loading, OFMSW was mixed with chipped wood at a volume ratio from 0.6 to 0.7 to achieve suitable biomass porosity. Before the anaerobic digestion phase, biomass was subjected to a four day of pre-oxidation process. After the aerobic phase, the digester was isolated to transition from aerobic to anaerobic conditions. Under these conditions the anaerobic digestion was accomplished in approximately 30 days. The biomass was subjected to a further aerobic composting treatment for 20 days before final use as fertilizer. Table 1 summarizes the composition and physicochemical characteristics of the OFSMW batch used in this study.

Table 1 - Starting values of digestion cycle – Initial biomass parameters.

	Volume (m ³)	Mass (t)	Water content (%)	Volatile Solids (%)	pH in	pH out
Digestate from previous batch	7.70 [±0.41]	7.00 [±0.49]	64.68 [±1.0]	56.3 [±3.3]	8.8 [±0.2]	
OFMSW + Wood	9.75 [±0.41]	5.61 [±0.38]	62.48 [±0.85]	83 [±3.0]	5.9 [±0.2]	
Mix	15.70 [±0.42]	12.61 [±0.36]	61.74 [±1.19]	60.79 [±3.1]	7.9 [±0.2]	8.2 [±0.2]

where:

pH in: pH measured at the beginning of loading into the digester; pH out: pH at end of digestion process; Mix: total biomass loaded into the digester; Square brackets indicate the standard deviation of measurements; * Mix was left at ambient temperature for 4 days prior to loading into the digester, thereby probably changing the pH e.g. via CO₂ escaping into the atmosphere.

To monitor and to detect the trace compounds contained in the biogas sample, a PTR-ToF-MS instrument was adopted. Samples (0.3 L) were collected in 3L Nalophan bags and sealed with Teflon stopper. VOCs analysis was conducted using a PTR-ToF-MS 8000 instrument in its V-mode configuration (Ionicon Analytik GmbH, Innsbruck, Austria). The sample was directly injected into the drift tube of the instrument via a heated (110°C) PEEK inlet tube. The experimental procedure adopted is reported elsewhere [2]. In order to meet SOFC requirements a gas cleaning section is mandatory. It was adopted the same instrument and procedure described above to study the behaviour of

the gas cleaning section, focusing on the sorbent material removal performance. Upstream (C0) and downstream (C) of the gas cleaning section were considered to measure the pass through ratio for a specific compound. Experimentally it was calculated the adsorption capacity of ashes. A glass reactor filter (340 ml) was filled with ashes from a wood chips boiler (3.3 MW, Viessman, Allendorf Germany). The digester is coupled to a glass filter using a blower to reach the min pressure around 30 mbar, with an average flow of 0.3 Nm³/h and a GHSV of 882 h⁻¹. The most abundant compound identified in the ash sample with a SEM-EDS analysis (FEI Inspect, Philips 525 M - SW9100 EDAX) is oxygen followed by silicon, carbon, potassium, calcium, magnesium and aluminium.

Table 2 - Elements identified with SEM-EDS analysis in the ash sample.

Element	Atomic % virgin	Atomic % tested
C	8.1	18
O	38.1	53.2
Mg	2.9	0.6
Al	4.3	0.6
Si	9.2	19.6
Cl	0	0.3
K	10.8	6.8
Ca	11.6	0.9
Fe	11.5	0
Ti	1.3	0
Na	1.2	0
Mn	1	0
Total:	100	100

Simulated gas mixture concerning different fuel conditions are considered for the tests with trace compounds, see Table 3. Synthetic biogas was prepared and obtained by mixing pure gas feeds from CH₄, CO₂, CO, N₂ and H₂ cylinders (Siad, Italy). The biogas mixture was sent to the ASC cell with mass flow controllers (Bronkhorst, The Netherlands). Experiments were performed with anode supported solid oxide fuel cells (ASC) - nickel based.

The fuel cell galvanostatic test was carried out with an electronic load (Kikusui Electronics Corp., Japan) in conjunction with an additional power supply in current-following mode (Delta Elektronika, The Netherlands). The oven temperature was kept constant at 750 °C. It was also carried on a specific experimental campaign to investigate the impact of H₂S, operating temperature and current density. H₂S concentration was fixed at 4 ppm(v), while the operating temperature was changed from 700 °C to 750 °C and to 800 °C, and the current density was changed from 0.21 to 0.32 and 0.42 Acm⁻².

Table 3 – Test conditions.

Pollutant test	Conc. Range (ppm(v))	Cell adopted	H ₂	CO	CO ₂	CH ₄	N ₂	H ₂ O	T	FU
			(ml min ⁻¹)				(g h ⁻¹)	(°C)	%	
H ₂ S	0.84-6.4	ASC700	151.5	136.4	68.2	15.2	386.4	2.9	750	30
D4	0.11-1.92	TOFC	348	133.7	62.1	5		6.58	750	21

At the end of the paper, preliminary results are achieved considering the algae growth from the digestate of the anaerobic digestion process, described above, and considering the removal of CO₂ from the SOFC generator. The digestate was sterilized in autoclave at 121°C for 20 min to consider only the chlorella vulgaris as inoculum. The illumination was controlled with lamps at vapour mercury of 250 W. The CO₂ flow was sent with a MFC (Bronkhorst, The Netherlands) using a gas cylinder (Siad, Italy). The algae growth was tested considering the following conditions:

B1: digestate – sterilized at T and p, dilution 1:20, with inoculum 20%, Lumen 12000;

B2: digestate – sterilized at T and p, dilution 1:50, with inoculum 20%, Lumen 12000;

B3: digestate – sterilized at T and p, dilution 1:70, with inoculum 20%, Lumen 12000;

B4: digestate – sterilized at T and p, dilution 1:50, with inoculum 9%, Lumen 12000;

B5: digestate – sterilized at T and p, dilution 1:50, with inoculum 20%, Lumen 2000;

B6: digestate – sterilized at T and p, dilution 1:50, with inoculum 32%, Lumen 12000;

R1: digestate – sterilized at T and p, dilution 1:50, with inoculum 20%, Lumen 12000 and CO₂ 100Nm³/min for 8 h/day for 15 days.

The goal was to identify the best dilution condition, the inoculum concentration, the effect of the external illumination and CO₂ flow.

3. Results

3.1. Trace compounds detection with PTR-ToF-MS

Table 4 lists a selection of the spectrometric peaks which are identified and monitored. Each compound has its experimental and expected m/z values, its chemical formula and tentative identification. PTR-ToF-MS provides only the chemical formula of the spectrographic peaks.

Table 4 - Spectrometric peaks which has been used in this paper along with their experimental and expected m/z values, their chemical formula and tentative identification supported also by available literature.

Measured m/z	Theoretical m/z	Protonated chemical formula	Tentative identification	References for PTR-MS spectra	References for biogas from waste management
18.033	18.0338	NH ₄ ⁺	Ammonia	[17]	[18]
31.018	31.018	CH ₃ O ⁺	Formaldehyde	[19]	[20]
34.995	34.995	H ₃ S ⁺	Hydrogen sulfide	[24]	[23]
45.033	45.033	C ₂ H ₅ O ⁺	Acetaldehyde	[20]	[21]
47.013	47.013	CH ₃ O ₂ ⁺	Formic acid	[17]	[26]
47.049	47.049	C ₂ H ₇ O ⁺	Ethanol	[19]	[21]
49.01	49.011	CH ₅ S ⁺	Methanethiol	[22]	[23]
61.028	61.0284	C ₂ H ₃ O ₂ ⁺	Acetic acid	[22]	[23]
63.022	63.0284	C ₂ H ₇ S ⁺	Dimethylsulfide (DMS)	[28]	[23]
73.065	73.065	C ₄ H ₉ O ⁺	2-butanone/butanal	[19]	[23]
75.044	75.044	C ₃ H ₇ O ₂ ⁺	Propionic acid/propanoates	[22]	[23]
77.041	77.042	C ₃ H ₉ S ⁺	Propanethiol	[22]	[23]
79.054	79.054	C ₆ H ₇ ⁺	Benzene	[28]	[23]
89.059	89.059	C ₄ H ₉ O ₂ ⁺	Butyric acid/butyrate	[22]	[20]
93.07	93.07	C ₇ H ₆ ⁺	Toluene	[20]	[23]
105.07	105.07	C ₈ H ₆ ⁺	Styrene	[28]	[23]
107.086	107.086	C ₈ H ₁₁ ⁺	Xylene	[28]	[23]
121.101	121.101	C ₉ H ₁₃ ⁺	Cumene	[17]	[21]
135.117	135.117	C ₁₀ H ₁₅ ⁺	p-Cymene	[28]	[21]
137.126	137.132	C ₁₀ H ₁₇ ⁺	Monoterpenes	[28]	[3]
205.195	205.195	C ₁₅ H ₂₅ ⁺	Sesquiterpenes	[20]	[3]
223.061	223.064	C ₆ H ₁₈ O ₃ Si ₃ H ⁺	D3	[21]	[26]
297.075	297.082	C ₈ H ₂₄ O ₄ Si ₄ H ⁺	D4	[21]	[26]
311.162	311.135	C ₁₀ H ₃₀ O ₃ Si ₄ H ⁺	L4	[21]	[26]
371.092	371.101	C ₁₀ H ₃₀ O ₃ Si ₃ H ⁺	D5	[21]	[26]

[3] = Mata-Alvarez et al., (2000); (2008); [17] = Jordan et al., (2009); [18] = Scaglia et al (2011); [19] = Buhr et al., 2002; [20] = Font et al., (2011); [21] = Singer et al., (2011); [22] = Papurello et al., (2012); [23] = Lomans et al., (2002); [24] = Orzi et al., (2010); [26] = Papadias et al., (2012); [28] = Biasioli et al., (2011);

Considering sulfur compounds detected from the anaerobic digestion batch of OFMSW, we have the following situation:

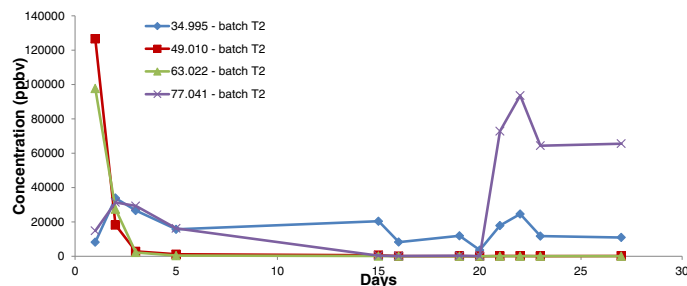


Figure 1 – Sulfur compounds detected during the AD process.

At the beginning of the digestion process, both CH₄S and C₂H₆S show a decreasing rate. These concentration profiles exhibit a remarkably steep reduction suggesting their participation in degradative reactions in the presence of sulfate. The H₂S concentration showed two peaks at the beginning and at the end of process, where the concentration reached 33 and 25 ppmv, respectively. Considering the coupling with a SOFC system is mandatory a gas cleaning section.

3.2. Sorbent materials to remove trace compounds for SOFC application

Fig. 2 depicts the pass through ratio of sulfur compounds, considering as sorbent materials ashes from wood-chips boiler. The higher removal of H₂S compared to the other sulfur compounds is due to the Ca and K oxide particles in the ash sample that helps the S removal. After 3 h of removal test only H₂S shows a pass through ratio still below 50% while the other sulfur compounds have a pass through ratio above 80%. The total sulfur removed by ashes is 61.8 mgS/kgash.

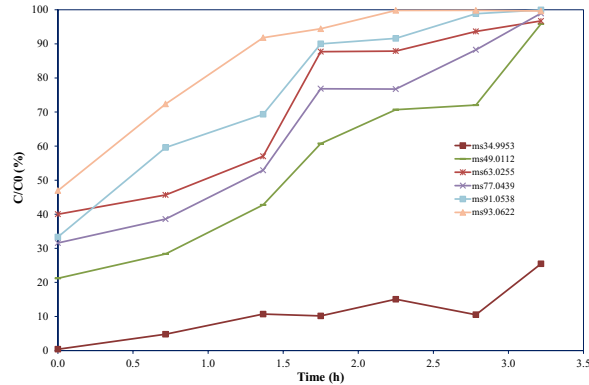


Figure 2 – Sulfur compounds detected during the removal of VOCs – 34.99 H₂SH+, 49.011 CH₄SH+, 63.02 C₂H₆SH+, 77.04 C₃H₈SH+, 91.05 C₄H₁₀SH+.

The most abundant siloxanes compound detected is D5 at 255 ppb(v), followed by D3 at 63.5 ppb(v), D4 at 47.1 ppb(v) and L4 at 26.7 ppb(v). Fig. 3 depicts the pass through ratio of siloxane compounds. A pass through ratio above 50% is recorded for all the Si compounds at the beginning of the test. The adsorption capacity of siloxanes was 0.21 mgSi/kgash.

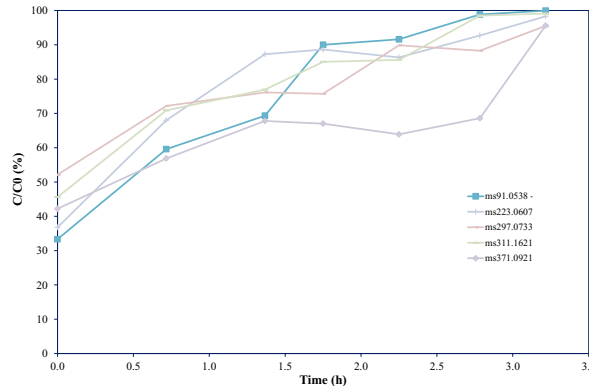


Figure 3 – Siloxane compounds detected during the removal of VOCs – 91.05 C₃H₁₀O₅SiH+, 223.06 D₃H+, 297.07D₄H+, 311.16 L₄H+, 371.09 D₅H+.

3.3. Impact of sulfur and siloxane compounds on SOFC performance

Sulfur impact on an anode supported fuel cell (Ni/8YSZ/8YSZ/GDC+LSCF) was investigated with the combination of two important operating variables: temperature T and current density i. Table 5 illustrates the results of the experimental tests. The cell voltage was measured between each poisoning and recovery steps to individuate the

performance drop of the cell. This experimental section investigated on the combined effect of current density and operating temperature when the cell was fed by a fixed H₂S concentration.

Table 5 - H₂S effect on performance drop at different operating temperatures and current densities.

H ₂ S (ppm(v))	Voltage (mV)	i (A/cm ²)	Temperature (°C)	Performance drop (%)
0.00	779.5	0.21	700	0.00
4.04	763.9	0.21	700	-2.05
0.00	658.8	0.32	700	0.00
4.04	615.0	0.32	700	-6.64
0.00	366.1	0.43	700	0.00
4.04	307.5	0.43	700	-16.00
0.00	819.1	0.21	750	0.00
4.04	809.5	0.21	750	-1.16
0.00	742.8	0.32	750	0.00
4.04	722.9	0.32	750	-2.67
0.00	594.2	0.43	750	0.00
4.04	537.1	0.43	750	-9.61
0.00	850.5	0.21	800	0.00
4.04	840.0	0.21	800	-1.24
0.00	799.2	0.32	800	0.00
4.04	777.6	0.32	800	-2.71
0.00	737.9	0.43	800	0.00
4.04	690.2	0.43	800	-6.46

At 700°C when the current density was fixed at 0.21 Acm⁻² the performance voltage drop registered was around 2%. This value increased at 6.64% when the current density increased to 0.32 Acm⁻², and reached a performance drop of 16% when the current density was fixed at 0.43 Acm⁻². A similar behavior was described in literature studies. Singhal et al., (1986) found that the power output drop increased from 10.3% to 15.6% when the cell was exposed to 10 ppm(v) of H₂S and the current density increased from 160 to 250 mAcm⁻² at 1000°C [31].

The poisoning of S is due to the blockage of surface sites by adsorbed sulfur [32]. In this case SO₂ formation desorbed from the surface, leading to alleviated poisoning effect. This explanation seems reasonable since one would expect that higher oxygen ion flux would lead to quicker removal of more adsorbed sulfur. But it also noted that SO₂ may exist only as a “short lived” reaction intermediate because sulfur dioxide may be reduced back to H₂S in the fuel environment. This is possible even only from a thermodynamic point of view. This explanation was confirmed experimentally, see Table 5. Here, at higher current density there is no alleviation of the sulfur effect on the cell performance. The same behavior described above was clearly visible, even if in lighter way, when the operating temperature was increased to 750°C and to 800°C. The absolute value of the performance drop decreased when the operating temperature was increased. This is due to positive effect of the temperature on the ohmic resistance and polarization resistance. The first term is reduced by the improvement of the material conductivity. The second term considers the electrochemical and mass transport losses, as reported elsewhere [33]. The electrochemical losses were reduced when the operating temperature was increased. This phenomenon was linked to the activation of chemical reactions at the electrodes. Here, the temperature increases the probability to reach the activation energy required for an electrochemical reaction. The mass transport losses were positively influenced by the operating temperature. In fact, the diffusion of the reactants in the porous media improved with the temperature increasing. Also D4 test have been analysed: Figure 4 in the upper right part showed how the cell performance was irreversibly affected by the D4 test. In fact, already at 111 ppb(v) the cell voltage decreased was not recovered. This was due to the silica precipitation that may cause a decrease in the active triple phase boundary (TPB) areas. The siloxane concentration acted on the cell blocking the anode pores and consequently the TPB region was reduced strongly [33] The phenomena reported above are separated but linked to the silica compounds formation.

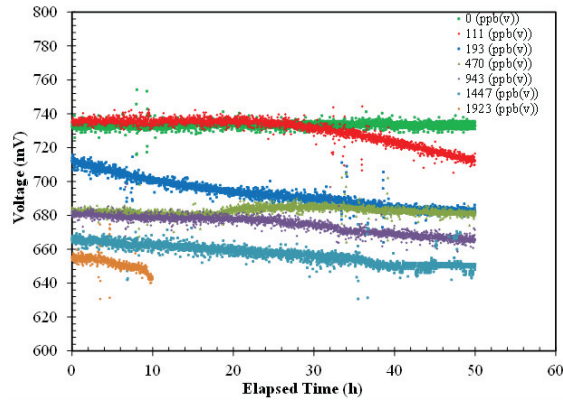


Figure 4 – Siloxane compounds effect on cell voltage.

3.4. Preliminary results of the algae growth from SOFC exhausts

The algae growth using digestate (from the anaerobic digestion batch) as culture media was analyzed. Preliminary results are obtained considering the dilution effect, the inoculum percentage of algae added to the starting batch, the effect of the light and the effect of the CO₂ fuel flow. In the following figures are reported the batch results and the testing description. The best dilution for the digestate was found to be around at 1:70 (B3), with a biovolume of cells around 1349 mm³/ml at the end of campaign (312 h), 37% and 64% lower than the dilution of 1:50 (B2) and 1.20 (B1), respectively. Fig. 5 b) shows how the nominal inoculum condition (+20% (B2)) has the highest initial algae growth with a total production around 850 mm³/ml. The highest (B6) and the lowest (B4) inoculum condition have a similar starting condition with 221 mm³/ml. At the end of the process B6 showed an increasing trend of 110% compared to the nominal case. B4 showed the lowest production with a decreasing of 31% compared to the nominal case. Fig. 5 c) showed the effect of the light, 12000 lm (B2) allowed an average production increasing growth around 62% compared to the low illumination case (B5). Fig 5 d) shows the algae growth for B2 and R1, considering or not the feeding with CO₂. R1 was fed with CO₂ (100 Nml/min) for 8 h/day for two weeks. The final production of algae is similar to the case without the CO₂ flow, 911 mm³/ml versus 850 mm³/ml. It was measured the pH at the end of the process to understand why the algae production is not substantially increased. R1 showed an acid pH value compared to B2 (6.2 vs 9.2). The starting pH value for R1 reactor was 8.5 and it was acidified due to the highest CO₂ flow. For future test this concentration must be decreased to achieve more basic values.

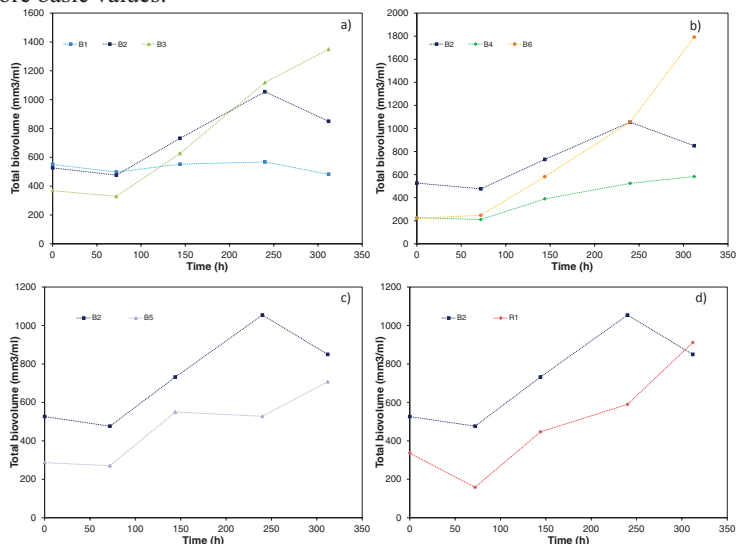


Figure 5 – a) Dilution effect B1=1:20, B2=1:50, B3=1:70; b) Inoculum effect B2=+20%, B4=+9%, B6=+32%; c) Lighting effect B2=12000lm, B5=20000lm; d) B2=0 CO2Nml/min, R1=100 CO2Nml/min.

Conclusions

Organic Fraction of Municipal Solid Waste was adopted to produce biogas to feed a SOFC generator. PTR-ToF-MS instrument was adopted to identify and to monitor several trace compounds, the most important for SOFCs application are sulfurs, siloxanes, terpenes and aromatic compounds. Ashes from wood chips boiler are adopted to remove trace compounds; the effectiveness was proved for H₂S and minor compounds. SOFC experiments were accomplished investigating the slipover influence from sorbent materials of sulfurs, chlorines and siloxanes. Tolerable concentration level of single organic compounds appears to be below 1 ppm(v) for H₂S. The effect of current density and fuel utilization was also investigated varying the operating temperature. Preliminary results on the algae production were shown. The optimal dilution of digestate was found to be around at 1:70. Factors that affect the algae production are light and percentage of algae inoculum. CO₂ flow must be settled to lower values in order to avoid the acidification of the environment.

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