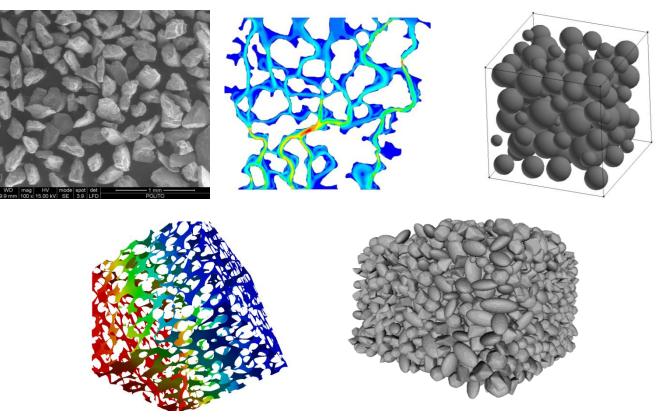
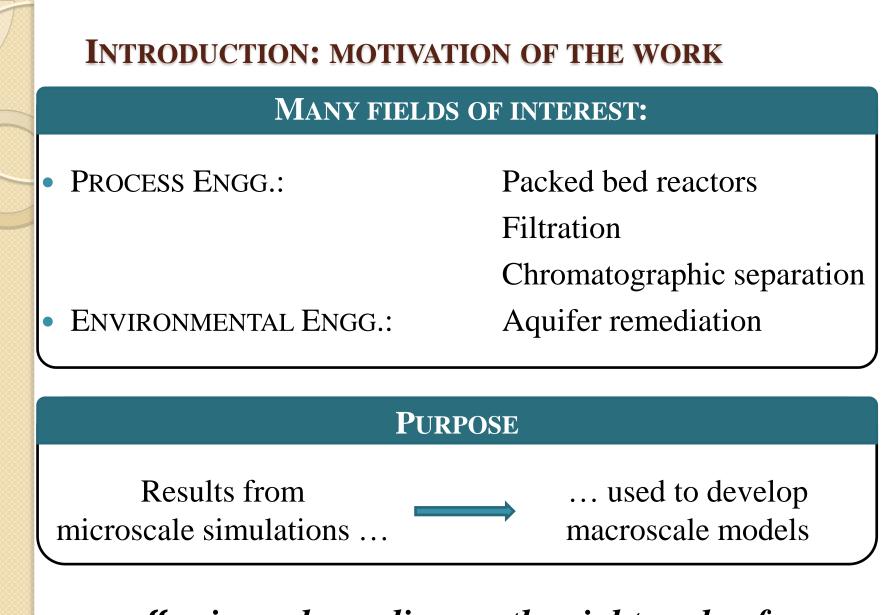
SIMULATION OF FLOW AND PARTICLE TRANSPORT AND DEPOSITION IN POROUS MEDIA WITH COMPUTATIONAL FLUID DYNAMICS



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"... since, depending on the right scale of observation, everything is porous. "



THEORETICAL BACKGROUND: FLUID FLOW

MACROSCALE PSEUDO-CONTINUUM APPROACH

• Creeping flow (Re < 1): linear relationship

DARCY'S LAW
$$\frac{\Delta P}{L} = \frac{\mu}{k} q$$

• Re > 1: nonlinear relationship

FORCHHEIMER'S LAW
$$\frac{\Delta P}{L} = \frac{\mu}{k} q + \beta \rho q^2$$

Packed beds filter law (wide range of Re) ERGUN'S LAW $\Delta P^* = \frac{\Delta P \rho D_g \varepsilon^3}{L G_0^2 (1 - \varepsilon^3)}$ $Re^* = \frac{D_g G_0}{(1 - \varepsilon)\mu}$



THEORETICAL BACKGROUND: PARTICLE DEPOSITION

MACROSCALE 1D ADVECTIVE-DIFFUSIVE EQUATION

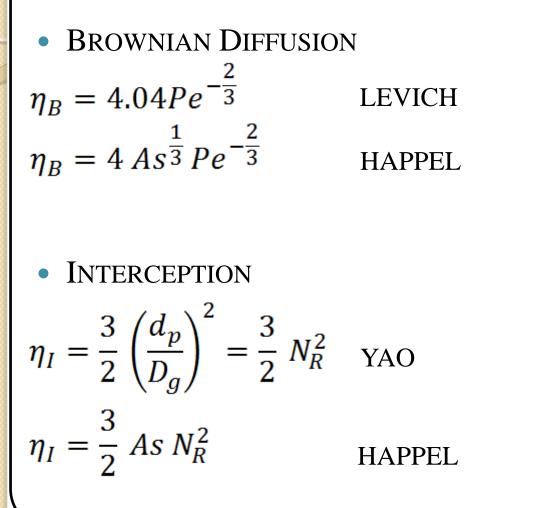
$$\frac{\partial C}{\partial t} + q \frac{\partial C}{\partial x} - D \frac{\partial^2 C}{\partial x^2} = Source$$

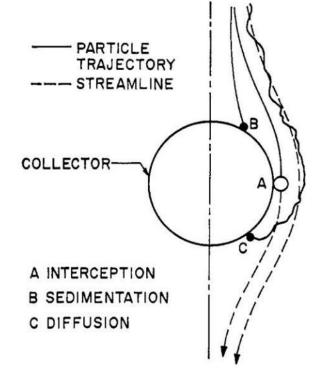
Source = $-K_d C$
 $K_d = \frac{3}{2} \frac{1 - \varepsilon}{\varepsilon} \frac{q}{D_g} \alpha \eta$

 η : <u>Collector Deposition Efficiency</u>

THEORETICAL BACKGROUND: PARTICLE DEPOSITION

DEPOSITION EFFICIENCY



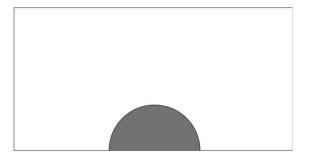


METHODOLOGY: MICROSCALE GEOMETRIC MODELS

INCREASING COMPLEXITY

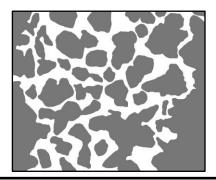
- SINGLE COLLECTOR
- CIRCULAR SHAPE

(under axial simmetry)



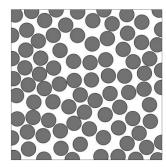
- IRREGULAR SHAPES
- REALISTIC μ -CT/SEM SCANS

(planar geometry)

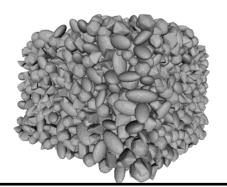


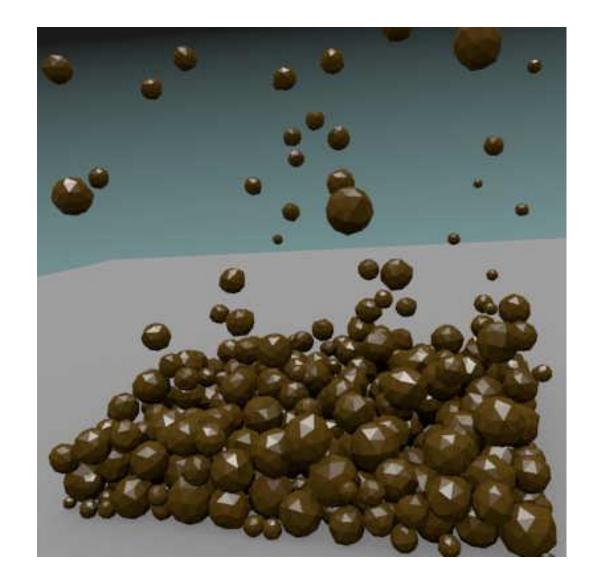
- CIRCULAR SHAPE
- ARTIFICIAL PACKING

(planar geometry)



- IRREGULAR SHAPES
- ARTIFICIAL PACKING





METHODOLOGY: OPERATING CONDITIONS

SOLVERS AND MESHING

• Finite volume CFD codes:

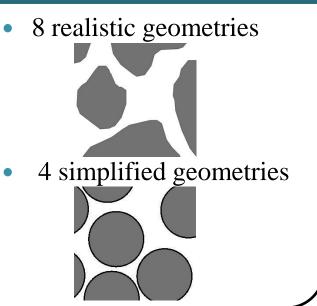
FLUENT, OPENFOAM

• Body-fitted meshers:

GAMBIT, SNAPPYHEXMESH

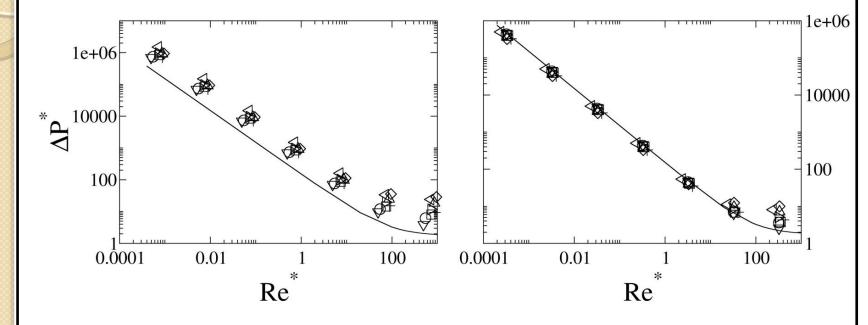
OPERATING CONDITIONS

- $D_g = 100 \text{ m} \div 300 \text{ m}$
- $= 0,3 \div 0,5$
- $q = 10^{-6}$, 10^{-5} , ..., 10^{-1} m s⁻¹
- Laminar model
- T = 293 K
- Viscosity = $0.00103 \text{ Kg m}^{-1}\text{s}^{-1}$



RESULTS: FLUID FLOW

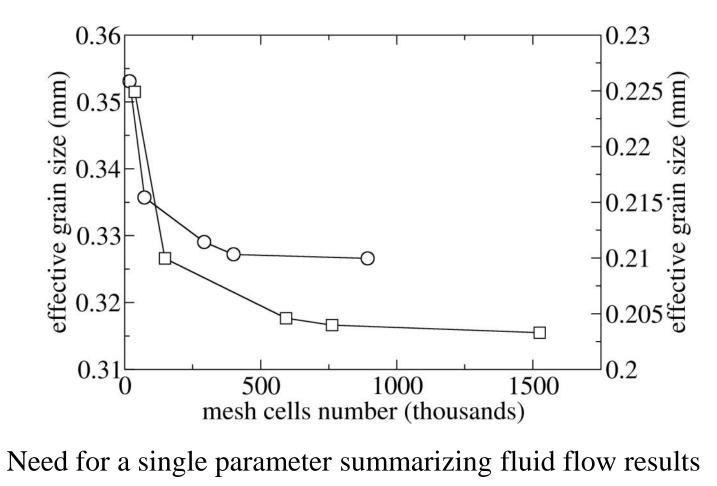
COMPARISON WITH ERGUN'S LAW



- Results show good agreement with Ergun's law
- Fitting on Ergun's law to obtain an <u>effective</u> grain diameter, D_g^*

RESULTS: FLUID FLOW

GRID INDEPENDENCE VERIFICATION



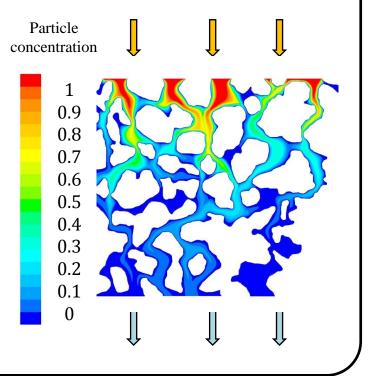
Grid independence assessed with changes in D_g^*

METHODOLOGY: OPERATING CONDITIONS

PARTICLES MODELING

- Particles are transported by convective and diffusive phenomena
- C = 1 at inlet
- C = 0 on grain surface
 - Assumed "perfect sink" condition
- Particle diameter

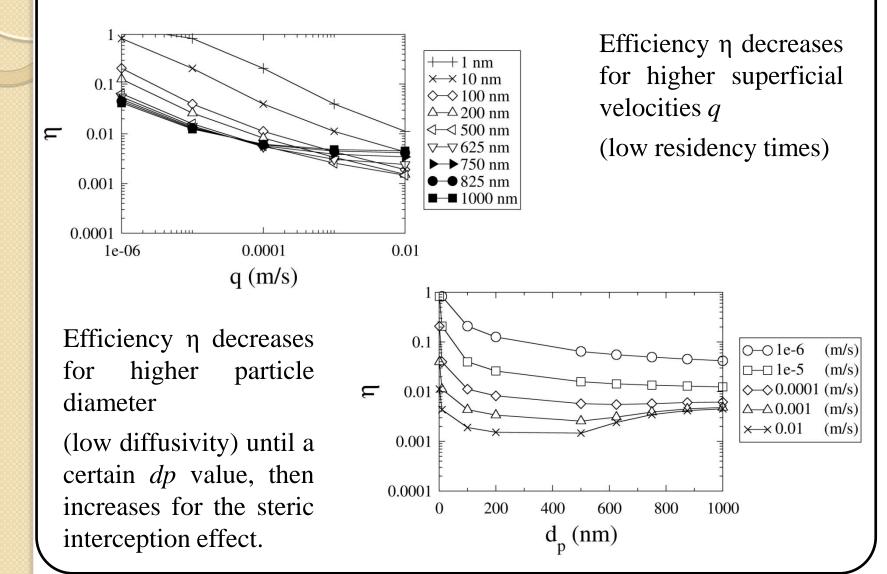
 $d_p = 1, 10, 100, 200, 500, 625, 750, 875, 1000 \text{ nm}$

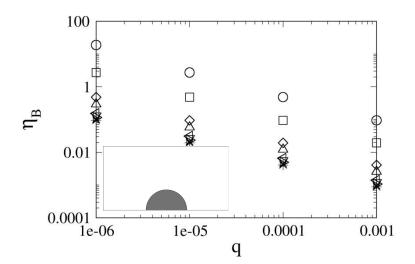


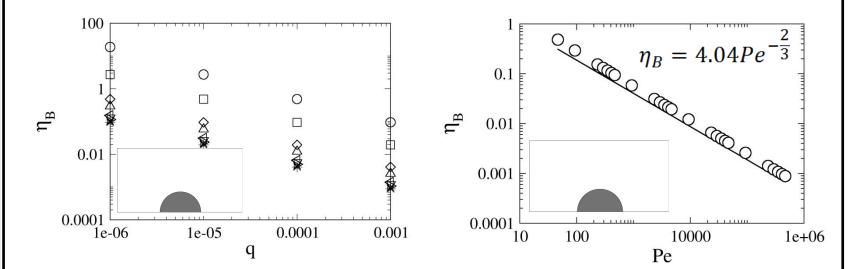
Collector deposition efficiency, η calculated with packed bed performance equation

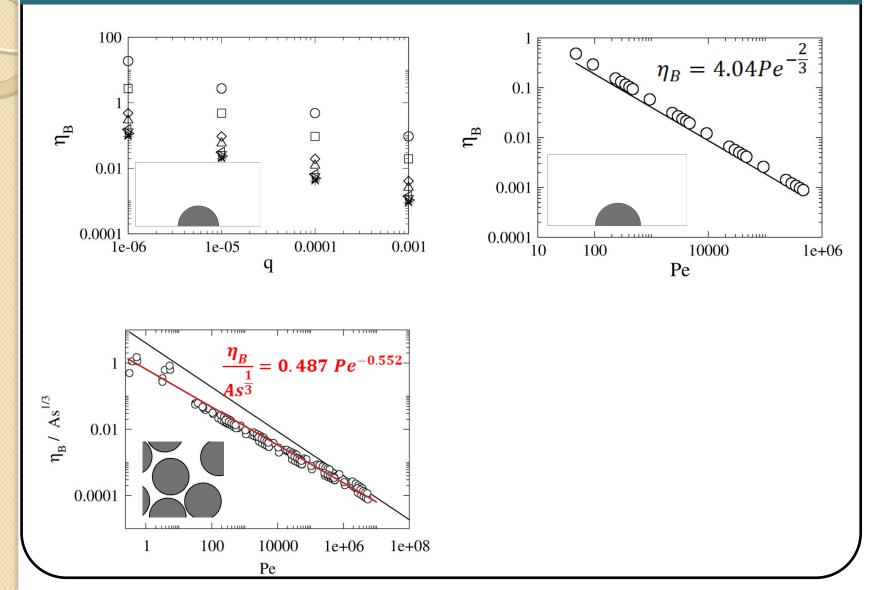
$$\frac{dC}{dx} = -\frac{3}{2} \frac{1-\varepsilon}{\varepsilon D_g} \eta C$$

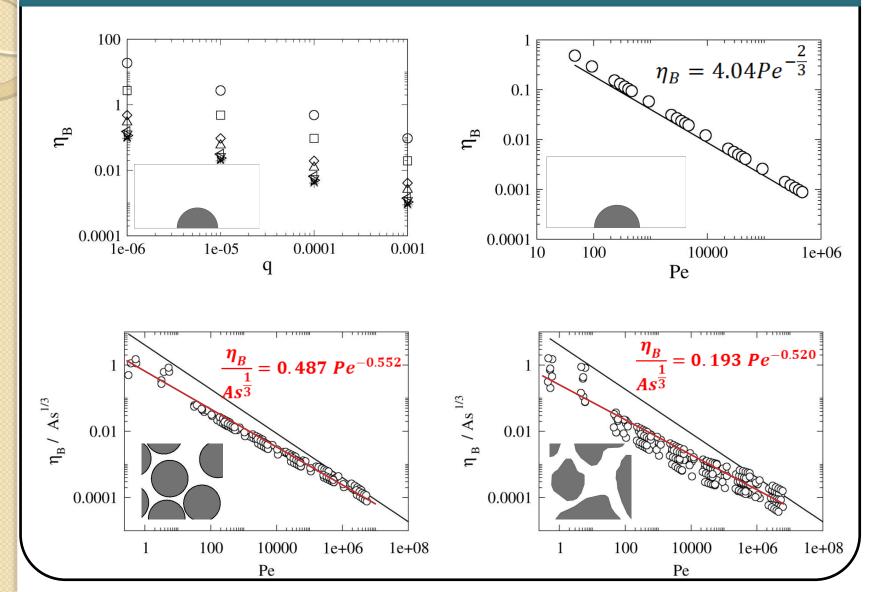
DEPOSITION EFFICIENCY: OVERVIEW



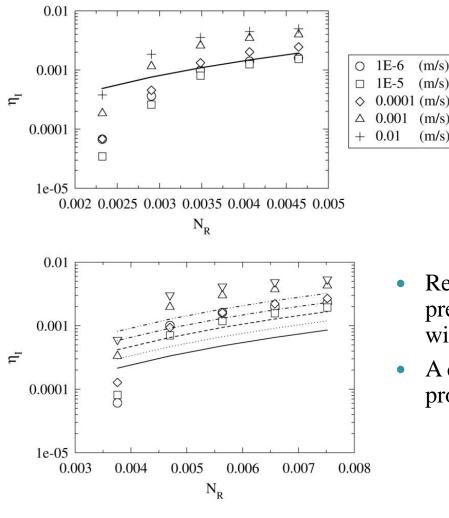








DEPOSITION EFFICIENCY: INTERCEPTION



Theoretical law:

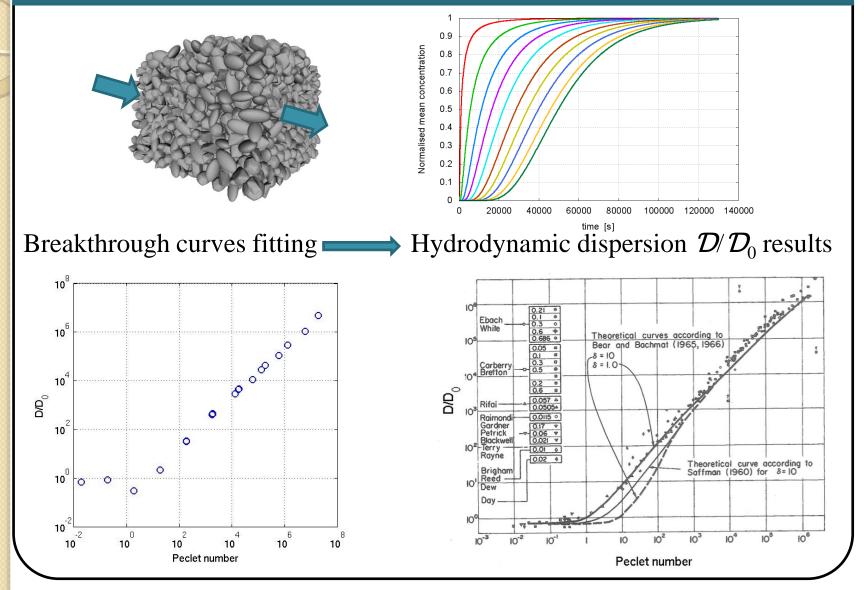
$$\eta_I = \frac{3}{2} As N_R^2$$

- Results appear in line with theoretical predictions but are strongly dispersed, with great variations at different *q*
- A dependency of η on q can be proposed

 $\eta_I = 3.377 \ As \ N_R^2 \ q^{0.145}$

CONCLUSIONS AND FUTURE WORK

FULLY 3D PARTICLE TRANSPORT SIMULATIONS



CONCLUSIONS AND FUTURE WORK

ACKNOWLEDGEMENTS

- AQUAREHAB (FP7, Grant Agreement no. 226565)
- PRIN Project 2008:

"Disaggregazione, stabilizzazione e trasporto di ferro zerovalente nanoscopico"

Thanks for your attention!

Any questions?