Quasiequilibrium lattice Boltzmann models with tunable bulk viscosity for enhancing stability

Original
Quasiequilibrium lattice Boltzmann models with tunable bulk viscosity for enhancing stability / P. Asinari; I.V. Karlin. - In: PHYSICAL REVIEW E, STATISTICAL, NONLINEAR, AND SOFT MATTER PHYSICS. - ISSN 1539-3755. - 81:(016702)(2010).

Availability:
This version is available at: 11583/2294914 since:

Publisher:
American Physical Society

Published
DOI:10.1103/PhysRevE.81.016702

Terms of use:
openAccess
This article is made available under terms and conditions as specified in the corresponding bibliographic description in the repository

Publisher copyright

(Article begins on next page)
Quasiequilibrium lattice Boltzmann models with tunable bulk viscosity for enhancing stability

Pietro Asinari$^{1,*}$ and Ilya V. Karlin$^{2,3,†}$

$^1$Department of Energetics, Politecnico di Torino, Corso Duca degli Abruzzi 24, Torino, Italy
$^2$Institute of Energy Technology, ETH Zurich, 8092 Zurich, Switzerland
$^3$School of Engineering Sciences, University of Southampton, SO17 1BJ Southampton, United Kingdom

(Received 12 June 2009; revised manuscript received 15 November 2009; published 12 January 2010)

Taking advantage of a closed-form generalized Maxwell distribution function [P. Asinari and I. V. Karlin, Phys. Rev. E 79, 036703 (2009)] and splitting the relaxation to the equilibrium in two steps, an entropic quasiequilibrium (EQE) kinetic model is proposed for the simulation of low Mach number flows, which enjoys both the $H$ theorem and a free-tunable parameter for controlling the bulk viscosity in such a way as to enhance numerical stability in the incompressible flow limit. Moreover, the proposed model admits a simplification based on a proper expansion in the low Mach number limit (LQE model). The lattice Boltzmann implementation of both the EQE and LQE is as simple as that of the standard lattice Bhatnagar-Gross-Krook (LBGK) method, and practical details are reported. Extensive numerical testing with the lid driven cavity flow in two dimensions is presented in order to verify the enhancement of the stability region. The proposed models achieve the same accuracy as the LBGK method with much rougher meshes, leading to an effective computational speed-up of almost three times for EQE and of more than four times for the LQE. Three-dimensional extension of EQE and LQE is also discussed.

DOI: 10.1103/PhysRevE.81.016702 PACS number(s): 47.11.–j, 05.20.Dd

I. INTRODUCTION

The lattice Boltzmann (LB) method has recently met with a remarkable success as a powerful alternative for solving the hydrodynamic Navier-Stokes equations, with applications ranging from large Reynolds number flows to flows at a micron scale, porous media, and multiphase flows [1]. The LB method solves a fully discrete kinetic equation for populations $f_i(x,t)$, designed in a way that it reproduces the Navier-Stokes equations in the hydrodynamic limit in $D$ dimensions. Populations correspond to discrete velocities $v_i$ for $i=0,1,\ldots,Q-1$, which fit into a regular spatial lattice with the nodes $x$. This enables a simple and highly efficient algorithm based on (a) nodal relaxation and (b) streaming along the links of the regular spatial lattice [2,3].

On the other hand, numerical stability of the LB method remains a critical issue [4]. Recalling the role played by the Boltzmann's $H$ theorem in enforcing macroscopic evolutionary constraints (the second law of thermodynamics), and crediting the latter as an essential condition for enhancing the stability of the method, pertinent entropy functions have been proposed, whose local equilibrium is suitable to recover the Navier-Stokes equations [5–9].

Other heuristic methods were proposed recently in order to enhance stability of LB. The rationale behind one of them, the matrix model [10] or, equivalently, the multiple-relaxation time (MRT) [11], is to execute a collision in the moment representation (different from the propagation in the populations representation) by relaxing different moments at a different rate. Optimal relaxation can be guided by linear stability analysis [12] (even though the actual performances may be effected by the nonlinearity). Even though it was not explicitly stated in the original papers [10–12], at least a part of the enhanced stability is due to increasing the bulk viscosity of the quasicompressible LB scheme, which can be viewed as a free parameter if the incompressible flow is the only concern. Moreover, the standard lattice Bhatnagar-Gross-Krook (LBGK) method can be written as a MRT, by performing the collisions in the moment representation and, conversely, MRT can be written as a LBGK by introducing a generalized equilibrium [13]. These observations suggest that increasing the numerical bulk viscosity by itself can be considered as a leading idea and it should not be concealed by a specific way in which collisions are performed.

In this paper, we take advantage of the recent crucial result concerning the closed-form generalized equilibrium (see Eq. (3) below and Ref. [14]), in order to derive a simple entropy-based quasiequilibrium model (see [8,15,16] for a general LB setting) with tunable bulk viscosity for enhancing stability. This approach differs from the MRT, and is in fact simpler, because no collision is actually performed in any moment space, even though it is based on recognizing the role of bulk viscosity for stability enhancement. The generalized equilibrium is the analog of the anisotropic Gaussian, and is a long-needed relevant distribution in the LB method [14]. This finding allows one to derive simple LB models with an additional free-tunable parameter for controlling the bulk viscosity, where the actual range is dictated by the entropy production inequality. In addition to the preliminary results reported in Ref. [14], this paper presents details of the basic steps of construction of these models and their numerical implementation, and provides numerical examples for measuring the stability improvement.

Before going any further, let us clarify the difference between the previous approach based on the discrete-time $H$ theorem (DTH) [6,17] and the present one based on the familiar continuous-time $H$ theorem (CTH). In this paper, only the latter will be used, but it is important to summarize the main analogies and differences.

$^*$pietro.asinari@polito.it
$^†$karlin@lav.mavt.ethz.ch
The key advantage of the DTH is the notion of unconditional stability of the corresponding entropic LB scheme (the entropy function becomes a global convex Lyapunov function of the entropic LB dynamics). Moreover the positivity is automatically enforced by the condition that the H function in a postcollision state is not greater than in the precollision state. However enforcing the discrete-time H theorem comes with the need of solving a nonlinear entropy estimate at each lattice site. The effect of the unconditional stability is the locally adaptive viscosity when the simulation is unresolved (similar to the eddy viscosity concept in large eddy simulation).

On the other hand, in the approach based on CTH theorem in the present paper, the unconditional stability is thus lost by the corresponding lattice Boltzmann time discretization. Stabilization mechanism here is not based on the DHT entropy estimate but is rather of the same nature as in the MRT models (although it is not identical to MRT as it is known in the cited literature), since the mechanism for enhancing stability is sought as increasing the bulk viscosity over the LBGK value. The CTH theorem in the present derivation is the standard one in kinetic theory (which is essentially the statement about the instantaneous entropy production inequality due to collisions), which gives a relation between the bulk and shear viscosities in this model. This is the only pertinent implication of the entropy production inequality here, it states that the bulk viscosity must be not smaller than the shear viscosity in order that the entropy production inequality remains negative, and which is consistent with the desired increase of the bulk viscosity above the shear viscosity (in LBGK they are equal). This is a simple yet useful implication of the CTH theorem (entropy production inequality), because without it the shear and bulk viscosity are only requested to be positive (but their relative magnitude is not defined) as follows from the asymptotic (Chapman-Enskog) analysis alone. The key idea is to increase the dissipation of the model for dumping the compressibility waves, which are irrelevant to the incompressible dynamics.

Summarizing, the H-function and their minimisers (equilibrium or quasiequilibria) are the same in both approaches. However these are static objects, defined irrespectively of the relaxation toward them. On the other hand, the H-theorem is always a statement about the relaxation toward these minima points, which can be differently implemented in the approaches respectively based on the DTH theorem and the CTH theorem, as shown here. The first approach ensures the unconditional stability by solving a nonlinear entropy estimate, while the second approach is much simpler but it is restricted by some stability thresholds. The interesting point is that the second approach allows one to explain clearly the link between the MRT models and the entropic models. Moreover, the CTH theorem can be used as a tool for deriving more general models on generic lattices [18].

The outline of the paper is as follows. First, for the sake of completeness, we remind the construction of continuous-time-space quasiequilibrium models, as briefly reported in Ref. [14]. In Sec. II the closed-form equilibria are discussed: in particular, in Sec. II A the generalized Maxwellian and in Sec. II B the constrained equilibrium. By means of the previous analytical results, in Sec. III the two proposed models are discussed: in Sec. III A the entropy-based model (EQE) and in Sec. III B the expanded (with regards to the local Mach number) model (LQE). The time and space discretization is done following the general procedure for quasiequilibrium LB models [8] the implementation details are reported in Sec. III C. Readers interested primarily in the practical applications can move directly to Secs. III B and III C. Numerical tests with the lid driven cavity flow are reported in Sec IV. These numerical tests suggest that the present approach is of the order of four times more efficient than the standard LBGK method with comparable accuracy. Finally, conclusions are drawn in Sec V. In the Appendix, the three-dimensional (3D) generalization of the model is presented.

II. CLOSED-FORM EQUILIBRIA

A. Generalized Maxwellian

For the sake of presentation and without any loss of generality, we consider the popular nine-velocity model, the so-called D2Q9 lattice, of which the discrete velocities are: \( v_0 = (0,0) \), \( v_i = (\pm c, 0) \) and \((0, \pm c)\) for \( i = 1-4 \), and \( v_i = (\pm c, \pm c) \), for \( i = 5-8 \) [3] where \( c \) is the lattice spacing. Recall that the D2Q9 lattice derives from the three-point Gauss-Hermite formula [19], with the following weights of the quadrature \( w(-1) = 1/6 \), \( w(0) = 2/3 \) and \( w(+1) = 1/6 \). Let us arrange in the list \( v_i \), all the components of the lattice velocities along the \( x \) axis and similarly in the list \( v_y \). Analogously let us arrange in the list \( f \) all the populations \( f_{\alpha} \). Algebraic operations for the lists are always assumed componentwise. The sum of all the elements of the list \( p \) is denoted by \( \langle p \rangle = \Sigma_{\alpha=1}^{\alpha=6} p_{\alpha} \). The dimensionless density \( \rho \), the flow velocity \( u \) and the second-order moment (pressure tensor) \( P \) are defined by \( \rho = \langle f \rangle \), \( \rho u_{\alpha} = \langle v_{\alpha} f \rangle \), and \( \rho P_{\alpha\beta} = \langle v_{\alpha} v_{\beta} f \rangle \), respectively. On the lattice under consideration, the convex entropy function (H function) is defined as [6]

\[
H(f) = \langle f \ln(f/W) \rangle,
\]

where \( W = w(v_{\alpha}/c)w(v_{\alpha}/c) \). The \( H \)-function minimization problem is considered in the sequel. It is well known [6] that the equilibrium population list \( f_M \) is defined as the solution of the minimization problem \( f_M = \min_{f \in S_M} H(f) \), where \( S_M \) is the set of functions such that \( S_M = \{ f > 0 : \langle f \rangle = \rho, \langle v_{\alpha} f \rangle = \rho u_{\alpha}, \langle v_{\alpha} v_{\beta} f \rangle = \rho P_{\alpha\beta} \} \). In other words, minimization of the \( H \) function (1) under the constraints of mass and momentum conservation yields [7]

\[
f_M = \rho \prod_{\alpha=x,y} w(v_{\alpha}/c) [2 - \varphi(u_{\alpha}/c)] \left[ \frac{2(u_{\alpha}/c) + \varphi(u_{\alpha}/c)}{1 - (u_{\alpha}/c)} \right]^{v_{\alpha}/c},
\]

where \( \varphi(z) = \sqrt{1 + 3z^2} \). A remarkable feature of equilibrium (2) which it shares with the ordinary Maxwellian is that it is a product of one-dimensional equilibria. In order to ensure the positivity of \( f_M \), the low Mach number limit must be considered, i.e., \( |u_{\alpha}| < c \).

It is possible to derive a novel constrained equilibrium, or
quasi-equilibrium [20], by requiring, in addition, that the diagonal components of the pressure tensor $P$ have some prescribed values [14]. Hence let us introduce a different minimization problem. The quasi-equilibrium population list $f_G$ is defined as the solution of the minimization problem $f_G = \min_{f_G} \mathbf{S}_G \cdot H(f)$, where $\mathbf{S}_G \subseteq \mathbf{S}_M$ is the set of functions such that $\mathbf{S}_G = \{ f > 0 : \langle f \rangle = \rho, \langle v \rangle = p \rho \}$. In other words, minimization of $H$ function (1) under the constraints of mass and momentum conservation and prescribed diagonal components of the pressure tensor yields

$$f_G = \rho \prod_{\alpha \in x,y} w(v_{\alpha} c) \frac{3(\epsilon^2 - P_{aa})}{2c^2} \sqrt{\frac{P_{aa} + c u_{\alpha}}{P_{aa} - c u_{\alpha}}} v_{\alpha}^2 c^2$$

(3)

To ease notation, we use $P = (P_{xx}, P_{yy})$ for a generic point on the two-dimensional plane of parameters. In order to ensure the positivity of $f_G$, it is required that $P \in \Omega$ where $\Omega = \{ P : c |u| < P_{xx}, c |v| < P_{yy} \}$ is a convex rectangular in the plane of parameters for each velocity $u$ (see Fig. 1).

Generalized Maxwellian (3) is the central result for the following derivations. It is interesting to note, that while equilibrium (2) is analogous to the ordinary Maxwellian (spherically symmetric Gaussian $f_M \sim \exp(-m(v-u)^2/2k_B\Theta_0)$, shifted from the origin by the amount of mean flow velocity $u$, and with the width proportional to the fixed temperature $\Theta_0 = c^2/3$), quasi-equilibrium (3) resembles the anisotropic Gaussian, $f_G \sim \exp(-1/2 \cdot (v-u) \cdot P^{-1} \cdot (v-u))$. The latter generalized Maxwellian corresponds to the ellipsoidal symmetry, and is among the only few analytic results on the relevant distribution functions in the classical kinetic theory. It is revealing that also in the LB realm the analog of the generalized Maxwellian has a nice closed form [Eq. (3)]. We note that explicit form of the quasi-equilibrium is possible due to a general result about a factorization symmetry of a certain class of quasi-equilibria for discrete velocity sets established as tensor products of one-dimensional velocities (we remind that the D2Q9 velocity set is a tensor product of two copies of one-dimensional sets $\{-c, 0, c\}$; details for a general case are given in [18]).

Moreover, it is possible to evaluate explicitly the $H$ function in the generalized Maxwell states [Eq. (3)], $H_G = H(f_G)$, the result is elegantly written

$$H_G = \rho \ln \rho + \rho \sum_{\alpha = x,y} \sum_{k = -\infty}^{\infty} w_{\alpha} a_{k}(P_{aa}) \ln(a_{k}(P_{aa}))$$

(4)

where $w_{\pm} = w(\pm 1)$, $w_{0} = w(0)$, $a_{\pm}(P_{aa}) = 3(P_{aa} \pm c u_{\alpha})/c^2$, and $a_{0}(P_{aa}) = 3(c^2 - P_{aa})/(2c^2)$ (see Fig. 1).

It is worth to analyze the moments of $f_G$. Clearly in a discrete velocity model, the number of linearly independent moments is equal to the number of discrete velocities $Q$. Hence the calculation of the moments can be performed by means of a linear mapping, namely $m = M f$, where $M$ is the nonorthogonal transformation matrix, namely,

$$M = \begin{bmatrix} 1, v_x, v_y, v_y^2, v_x^2, u_x v_y, (v_y)^2, u_y v_x, (v_x)^2, (v_x)^2 \end{bmatrix}^T$$

(5)

which involves proper combinations of the lattice velocity components. Applying this linear mapping yields

$$m_G = M \cdot f_G = \rho \begin{bmatrix} 1, u_x, u_y, P_{xx}, P_{yy}, u_x u_y, u_x P_{xx}, u_y P_{yy}, P_{xx}, P_{yy} \end{bmatrix}^T$$

(6)

This clearly shows that the quasi-equilibrium moments depend only on the constrained quantities, i.e., the conserved moments (mass and momentum) and the prescribed diagonal components of the second-order moment tensor ($P_{xx}$ and $P_{yy}$). As we see, for the whole five-parametric family of functions $f_G(\rho, u, P_{xx}, P_{yy})$ it holds that the off-diagonal component of the pressure tensor does not depend on $P_{aa}$, and is in the form required by the Maxwell-Boltzmann relation,

$$\langle f_G c_x c_y \rangle = p u_x u_y \quad \text{for any } P$$

(7)

The previous linear mapping $M$ was introduced with the intent to clarify the structure of the generalized Maxwellian with regards to some meaningful moments, but this does not
effect the derivation of \( f_G \) [Eq. (3)], which is done by means of entropic concepts only. In the next section, this result is used to derive the constrained equilibrium.

B. Constrained equilibrium

With the help of the function \( f_G \) [Eq. (3)], let us derive a constrained equilibrium \( f_C \) which brings the \( H \)-function to a minimum. Among all the population laws with a fixed trace of the pressure tensor \( T(P) = P_{xx} + P_{yy} \). In terms of the parameter set \( \Omega \), this is equivalent to require that the point \( C = (P_{xx}^C, P_{yy}^C) \) belongs to a line segment \( L_T = \{ P \in \Omega : P_{xx} + P_{yy} = T \} \), and the constrained equilibrium \( C \) is that minimizing the function \( H_G \) [Eq. (4)] on \( L_T \) (see Fig. 1). Since the restriction of a convex function to a line is also convex, the solution to the latter problem exists and is found by \( [(\partial H_G / \partial P_{xx}) - (\partial H_G / \partial P_{yy})]_{P_{xx} + P_{yy} = T} = 0 \), which yields a cubic equation in terms of the normal stress difference \( N = P_{xx}^C - P_{yy}^C \),

\[
N^2 + aN^2 + bN + d = 0,
\]

\[
a = -\frac{1}{2}(u_x^2 - u_y^2), \quad b = (2c^2 - T)(T - u_x^2),
\]

\[
d = \frac{1}{2}(u_x^2 - u_y^2)(2c^2 - T)^2.
\]

Let us define \( p = -\frac{c^2}{3} + 3b, \quad q = 2a^3/27 - ab/3 + d, \) and \( \Delta = (q/2)^3 + (p/3)^3 \). As long as \( \Delta \geq 0 \), which is well satisfied in the low Mach number limit, the Cardano formula implies

\[
P_{xx}^C = \frac{T}{2} \pm \frac{1}{2} \sqrt{\frac{q}{2} \pm \sqrt{\frac{q^2}{4} - \frac{p^3}{27}}},
\]

\[
r = 3 \sqrt{-\frac{q}{2} + \frac{\sqrt{\frac{q^2}{4} - \frac{p^3}{27}}}{2}},
\]

while \( P_{yy}^C = T - P_{xx}^C \) (note that a spurious root corresponding to \( -\Delta \) was neglected in Eq. (9)) as it does not satisfy the asymptotics at \( u_x = u_y = 0 \). Thus, substituting Eq. (9) into Eq. (3), we find the constrained equilibrium

\[
f_C = f_G(p, u, P_{xx}^C(u, T), P_{yy}^C(u, T)).
\]

Before proceeding any further, we mention that generalized Maxwellian (3) is consistent with and extends the previously known results:

(i) the point of global minimum of the function \( H_G \) [Eq. (4)] on \( \Omega \) is found from \( (\partial H_G / \partial P_{xx}) = 0 \). The corresponding solution \( \mathcal{M} = (P^M_{xx}, P^M_{yy}) \), where \( P^M_{xx} = c^2/3 + (2c^2 - 3)(13 + 3(u_x c^2/3)^2) \), recovers the equilibrium \( f_M \) [Eq. (2)] upon substitution into Eq. (3): \( f_M = f_G(p, u, P^M_{xx}(u), P^M_{yy}(u)) \).

(ii) In Ref. [8], a different LB equilibrium \( f_0 \) was introduced as the entropy minimization problem under fixed density, momentum and energy. That equilibrium was calculated exactly only for vanishing velocity in [8] while a series expansion was used for \( u \neq 0 \). The previous result reported above solves the problem of Ref. [8] exactly for any velocity: Substituting \( T = 2\Theta u^2 \) (two-dimensional ideal-gas equation of state, with \( \Theta \) the temperature) into Eq. (10), it is simply \( f_M(p, u, \Theta) = f_G(p, u, P^M_{xx}(u, 2\Theta + u^2), P^M_{yy}(u, 2\Theta + u^2)) \). Expanding the exact solution \( P^C_{xx} \) [Eq. (9)] in terms of the velocity \( u \) yields the approximate solution consistent with Ref. [8], namely,

\[
P^C_{xx} = \Theta + \left( \frac{\Theta + 1}{4\Theta} \right) u_x^2 + \left( \frac{3\Theta - 1}{4\Theta} \right) u_y^2 + O(u^4) \quad (11)
\]

We note that the present derivation of the exact solution at arbitrary values of \( u \) is exact and extends the previously known results to arbitrary \( u \). The extension to the three-dimensional case is straightforward and the details are reported in the Appendix. Moreover, in the next section, this result is used to introduce the proposed model with tunable bulk viscosity.

III. Quasiequilibrium kinetic models

A. Entropy-based kinetic model (EQE)

Let us introduce the entropy-based quasiequilibrium model (EQE model in the following) (see [8,15,16] for general LB setting) for the kinetic equation (time and space are both continuous)

\[
\partial f + c \cdot \nabla f = J(f)
\]

\[
J = -\frac{1}{\tau_s} (f - f_C) - \frac{1}{\tau_s} (f_C - f_M).
\]

It is straightforward to prove the \( H \) theorem for the previous model. For that, it suffices to rewrite

\[
J(f) = -\frac{1}{\tau_s} (f - f_M) - \frac{(\tau_s - \tau_f)}{\tau_f} (f - f_C).
\]

The entropy production \( \sigma = (\ln(\dot{f}) - W)/\sqrt{\dot{f}} \) becomes

\[
\sigma = -\frac{1}{\tau_s} (\ln(f/M) - (\tau_s - \tau_f) (\ln(f_C) - (f - f_C)),
\]

which is nonpositive \( \sigma \leq 0 \) and it annihilates at the equilibrium, i.e., \( \sigma(f_M) = 0 \), provided that relaxation times satisfy the time hierarchical condition.

\[
\tau_f \leq \tau_s.
\]
where the quasiequilibrium \( f_{\text{QE}} \) is defined as
\[
f_{\text{QE}}(\rho, u, T) = \frac{\tau_f}{\tau_s} f_M(\rho, u) + \left( 1 - \frac{\tau_f}{\tau_s} \right) f_c(\rho, u, T),
\]
and it is essentially a linear interpolation between the local Maxwellian \( f_M \) and the constrained equation \( f_c \) by means of the blending parameter \( \tau_f / \tau_s \cong 1 \). Hence the proposed model involves a quasiequilibrium with a tunable parameter (the ratio \( \tau_f / \tau_s \)) and it admits a \( H \) theorem as far as the free parameter is tuned such that \( \tau_f / \tau_s \cong 1 \). In the following, let us discuss how this parameter is related to the bulk viscosity, which is the main target of the present paper.

Recalling Eq. (14), the (truncated) moment system of equations is
\[
\frac{\partial}{\partial t} \rho + \frac{\partial}{\partial x} \rho u_x + \frac{\partial}{\partial y} \rho u_y = 0,
\]
\[
\frac{\partial}{\partial t} (\rho u_x) + \frac{1}{2} \frac{\partial}{\partial x} \rho (u_x^2 + T) + \frac{1}{2} \frac{\partial}{\partial y} \rho (u_x u_y) + \frac{\partial}{\partial x} (\rho P_{xy}) = 0,
\]
\[
\frac{\partial}{\partial t} (\rho u_y) + \frac{1}{2} \frac{\partial}{\partial x} \rho (u_x u_y) - \frac{1}{2} \frac{\partial}{\partial y} \rho (u_y^2 + T) + \frac{\partial}{\partial y} (\rho P_{xy}) = 0,
\]
\[
\frac{\partial}{\partial t} (\rho P_{xy}) + \frac{\partial}{\partial x} (\rho P_{xxy}) + \frac{\partial}{\partial y} (\rho P_{xyy}) = -\frac{\rho}{\tau_f} (P_{xy} - u_x u_y),
\]
\[
\frac{\partial}{\partial t} (\rho T) + \frac{\partial}{\partial x} (\rho u_x) + \frac{\partial}{\partial y} (\rho u_y) + \frac{\partial}{\partial x} (\rho Q_{xxy}) + \frac{\partial}{\partial y} (\rho Q_{xyy})
\]
\[
= -\frac{\rho}{\tau_f} (T - T_M),
\]
\[
\frac{\partial}{\partial t} (\rho N) + \frac{\partial}{\partial x} (\rho u_x) - \frac{\partial}{\partial y} (\rho u_y) - \frac{\partial}{\partial x} (\rho Q_{xxy}) + \frac{\partial}{\partial y} (\rho Q_{xyy})
\]
\[
= -\frac{\rho}{\tau_s} (N - N_M) - \left( \frac{1}{\tau_f} - \frac{1}{\tau_s} \right) \rho (N - N_C),
\]
\[
\frac{\partial}{\partial t} (\rho Q_{xxy}) + \frac{\partial}{\partial x} (\rho Q_{xxy}) + \frac{\partial}{\partial y} (\rho Q_{xyy})
\]
\[
= -\frac{\rho}{\tau_s} \left( Q_{xxy} - u_y \frac{T + N_C}{2} \right)
\]
\[
\frac{1}{\tau_s} - \frac{1}{\tau_f} \rho \left( Q_{xxy} - u_y \frac{T + N_C}{2} \right),
\]
\[
\frac{\partial}{\partial t} (\rho Q_{xyy}) + \frac{\partial}{\partial x} (\rho Q_{xyy}) + \frac{\partial}{\partial y} (\rho Q_{xyy})
\]
\[
= -\frac{\rho}{\tau_s} \left( Q_{xyy} - u_x \frac{T - N_C}{2} \right)
\]
\[
\frac{1}{\tau_s} - \frac{1}{\tau_f} \rho \left( Q_{xyy} - u_x \frac{T - N_C}{2} \right),
\]
Assuming the low Mach number limit and introducing the previous expression in Eq. (19), it is possible to recover approximated expressions for the nonconserved moments. In particular, the Chapman-Enskog asymptotic procedure yields the following approximations of the pressure tensor components at the leading order, indicated by the superscript (0),
\[
P_{xy}^{(0)} = u_x u_y,
\]
\[
T^{(0)} = D c_s^2 + u^2,
\]
\[
N^{(0)} = u_x^2 - u_y^2,
\]
for the approximations of third-order energy flux. Similarly, small deviations of the nonconserved moments from the previous approximations, indicated by the superscript [Eq. (1)], immediately follow
\[
P_{xy}^{(1)} = -\tau_s c_s^2 (\partial \mu_x - \partial \mu_y),
\]
\[
T^{(1)} = -\tau_s d \frac{c_s^2}{2} (\partial \mu_x - \partial \mu_y),
\]
\[
N^{(1)} = -\tau_s d c_s^2 (\partial \mu_x - \partial \mu_y). \tag{25}
\]
Grouping together leading-order approximations, i.e., \( P_{xy}^{(0)}, T^{(0)}, \) and \( N^{(0)} \) given by Eq. (23), and small deviations of the nonconserved moments, i.e., \( P_{xy}^{(1)}, T^{(1)}, \) and \( N^{(1)} \) given by Eq. (25), allows one to recover the hydrodynamic equations
\[
\frac{\partial}{\partial t} \rho + \frac{\partial}{\partial x} (\rho u_x) + \frac{\partial}{\partial y} (\rho u_y) = 0,
\]
\[
\frac{\partial}{\partial t} (\rho u_x) + \frac{\partial}{\partial x} (\rho u_x) + \frac{\partial}{\partial y} (\rho u_y) + \frac{\partial}{\partial x} (\rho P_{xy}) + \frac{\partial}{\partial y} (\rho P_{xy})
\]
\[
= -\frac{\rho}{\tau_f} (P_{xy} - u_x u_y) + \frac{1}{\rho} \left[ \frac{\partial u_x}{\partial y} \partial u_y - \frac{\partial u_y}{\partial x} \partial u_x \right] + \frac{2}{D} \left[ \partial \mu_x \partial \mu_y \right],
\]
where the transport coefficients are
\[ v = \tau c_s^2, \quad \xi = \tau c_s^2, \quad (27) \]

for the kinematic viscosity and the bulk viscosity, respectively. Thus, from Eq. (16), the bulk viscosity is larger than the kinematic viscosity in this model,

\[ \nu \leq \xi. \quad (28) \]

In particular, the parameter for enhancing stability is the ratio $\xi/\nu \geq 1$, as pointed out by the following numerical tests. Before proceeding with the numerical implementation, the next section reports a simplified version of the model, based on expansion with regards to the low Mach number limit.

**B. Expanded model (LQE)**

The goal of this section is to provide the basic details of a simplified version of the kinetic model, based on the expansion with regards to the Mach number (LQE model in the following). The simplification concerns the following three issues:

(i) first of all, recalling the compact form given by Eq.

\[ \frac{\partial}{\partial t}f + \nabla \cdot (u f) = -\frac{1}{\tau_e} f + \tau_e \left( f_{eq} - f \right), \quad (18) \]

it is possible to realize that the proposed quasiequilibrium $f_{eq}$ requires to compute twice the same generalized Maxwellian $f_G$ with different arguments, namely,

\[ f_{eq}(p,u,T) = \frac{\tau_e}{\tau_s} f_G(p,u,P^{M}_{xx}(u),P^{M}_{yy}(u)) \]

\[ + \left( 1 - \frac{\tau_e}{\tau_s} \right) f_G(p,u,P^{C}_{xx}(u),P^{C}_{yy}(u),T). \quad (29) \]

(ii) Second, the generalized Maxwellian $f_G$ given by Eq. (3) with generic arguments $(P_{xx}, P_{yy})$ can be expressed in a simpler equivalent way in terms of components, namely,

\[ f_{G(0,0)} = \frac{\rho}{c_4}(c^2 - P_{xx})(c^2 - P_{yy}), \]

\[ f_{G(0,1,0)} = \frac{\rho}{2 c^4}(P_{xx} \pm c u_{xx})(c^2 - P_{yy}), \]

\[ f_{G(0,0,1)} = \frac{\rho}{2 c^4}(P_{xx} \pm c u_{yy})(c^2 - P_{xx}), \]

\[ f_{G(1,1,0)} = \frac{\rho}{4 c^4}(P_{xx} \pm c u_{xx})(P_{yy} \pm c u_{yy}). \quad (30) \]

(iii) Finally, in the low Mach number limit, recalling that

\[ P^{M}_{xx} = -c_s^2 + 2c_s^2 \sqrt{1 + u_{xx}^2/c_s^2} \]

and recalling Eq. (20), the following expressions:

\[ P^{M}_{xx}(u) = c_s^2 + u_{xx}^2 + O(Ma^4), \]

\[ P^{M}_{yy}(u) = c_s^2 + u_{yy}^2 + O(Ma^4), \quad (31) \]

hold for the equilibrium moments, while the expressions

\[ p^{C}_{xx}(u,T) = \frac{T}{2} + u_{xx}^2 - \frac{u_{x}^2 + u_{y}^2}{2} + O(Ma^4), \]

\[ p^{C}_{yy}(u,T) = \frac{T}{2} + u_{yy}^2 - \frac{u_{x}^2 + u_{y}^2}{2} + O(Ma^4), \quad (32) \]

hold for the constrained moments, where the residuals $O(Ma^4)$ can be neglected in both cases. Equations (30) and (32) are generalized for the three-dimensional case in the Appendix.

It should be stressed that, while the results for the EQE model are exact for any $u$ (subject to the positivity constraint), the later restriction to the low Mach number expansion is a matter of convenience, and it leaves intact the overall accuracy (with respect to recovering hydrodynamic equations) of the proposed model. We concluded this section by pointing out the connection between the expanded model and the multiple-relaxation-time (MRT) collision operator [14]. First of all, as far as the hydrodynamic limit is concerned, the deviations of quasi-equilibrium moments from equilibrium values can be neglected for all orders strictly higher than the second. In other words, for third and fourth order moments, the equilibrium values can be substituted instead of the quasi-equilibrium values, without affecting the leading hydrodynamics. Hence it remains to discuss the second-order deviations. Combining the expressions given by Eqs. (32) yields

\[ p^{C}_{xx}(u,T) = \frac{P_{xx} + P_{yy} + P^{M}_{xx} - P^{M}_{yy}}{2}, \]

\[ p^{C}_{yy}(u,T) = \frac{P_{xx} + P_{yy} - P^{M}_{xx} + P^{M}_{yy}}{2}. \quad (33) \]

Recalling Eqs. (17) and (29), the second-order deviations become

\[ p^{0E}_{xx} - P_{xx} = \frac{\beta + 1}{2} (P^{M}_{xx} - P_{xx}) + \frac{\beta - 1}{2} (P^{M}_{yy} - P_{yy}), \]

\[ p^{0E}_{yy} - P_{yy} = \frac{\beta - 1}{2} (P^{M}_{xx} - P_{xx}) + \frac{\beta + 1}{2} (P^{M}_{yy} - P_{yy}), \quad (34) \]

where $\beta = \frac{\tau_{ci}}{\tau_{ei}} \leq 1$. Taking into account the previous expressions, the collision operator can be approximated by

\[ J'(f) = -A(f - f_{M}), \quad (35) \]

where $A = 1/\tau_{M}^{-1}AM$, $M$ is the linear mapping defined by Eq. (5) and the $9 \times 9$ matrix $A$ is

\[ \Lambda = \text{diag} \left[ \left[ 1,1,1, \beta_{+}, \beta_{+}, \beta_{+}, \beta_{+}, \beta_{+}, \beta_{+}, \beta_{+} \right], \left[ 1,1,1,1 \right] \right], \quad (36) \]

with $\beta_{+} = (\beta + 1)/2$. Operator $J'$ is a collision operator in a matrix form [4] with collision matrix $A$ (characterized by two relaxation times $\tau_{ei}$ and $\tau_{ci}/\beta = \tau_{ei}$), but it can be easily expressed as a MRT collision integral [22], by using the mapping $M$ for defining a moment representation.

In the next section, some details are reported concerning the numerical implementation in order to avoid the discrete lattice effects, i.e., numerical errors due to the spatial discretization (lattice Knudsen number), which may effect the expressions of the effective transport coefficients.
C. Lattice Boltzmann realization

Let us derive a lattice Boltzmann scheme from the kinetic model, Eqs. (17) and (18), following the general procedure of Ref. [8]. Kinetic Eq. (17) is integrated in time from \( t \) to \( t + \delta t \) along characteristics, and the time integral of the right-hand side is evaluated by trapezoidal rule to get

\[
f(x + v \delta t, t + \delta t) - f(x, t) = \frac{\delta t}{2} f(x + v \delta t, t + \delta t) - f(x, t) = \frac{\delta t}{2} \frac{\partial f}{\partial x} f(x, t) + \frac{\delta t}{2} \frac{\partial f}{\partial x} f(x, t).
\]

(37)

The latter expression involves implicit computations, which may be cumbersome to code. In order to avoid them, let us apply the following variable transform [8,23]:

\[
f \rightarrow g = g - \frac{\delta t}{2} J(f),
\]

(38)
to Eq. (37), which yields

\[
g(x + v \delta t, t + \delta t) = (1 - \omega_j) g(x, t) + \omega_j \beta_{QE}(\rho, u, T_{CN}),
\]

(39)

where \( \rho = \langle g \rangle \) and \( \rho_u = \langle u g \rangle / \langle g \rangle \), because mass and momentum are conserved, while

\[
T_{CN}(g) = \left( 1 - \frac{\omega_j}{2} \right) T(g) + \frac{\omega_j}{2} T_{M}(g),
\]

(40)

\[
T(g) = \langle u_i^2 + v_j^2 \rangle g,
\]

(41)

\[
T_{M}(g) = \frac{2c^2}{3} \left[ \sqrt{1 + 3 \frac{u_i^2}{c^2}} + \sqrt{1 + 3 \frac{u_j^2}{c^2}} - 1 \right]
\]

\[
= \frac{2c^2}{3} + u_i^2 + u_j^2 + O(Ma^4),
\]

(42)

and

\[
\omega_j = \frac{2 \delta t}{2 \tau_j + \delta t}, \quad \omega_s = \frac{2 \delta t}{2 \tau_s + \delta t}.
\]

(43)

In particular, using the first or the second expression reported in Eq. (42) depends on the considered model, i.e., if the entropy-based model or the expanded model is implemented respectively. By means of Chapman-Enskog asymptotic procedure, it is possible to prove that the previous lattice Boltzmann scheme recovers the Navier-Stokes equations up to the second order with regards to \( \delta x = c \delta t \), with the kinematic viscosity \( \nu = \tau_c c^2 \) and the bulk viscosity \( \xi = \tau_s c^2 \), as it happens for the continuous (in space and time) kinetic model.

A few comments on the above discretization scheme are in order. First, we remark that a simpler discretization of the kinetic equation using a forward Euler scheme, \( f(x + v \delta t, t + \delta t) - f(x, t) = \delta t \frac{\partial f}{\partial x} f(x, t) \) is only first-order accurate in the above sense. For \( \tau_c = \tau_s \) (that is, for the BGK case), the latter scheme can be interpreted as a second-order accurate with rescaled viscosity coefficients, as is well known. However, in general, such a reinterpretation is not straightforward if collision integral depends explicitly on the nonconserved moments (or, in other words, it depends explicitly on a quasi-equilibrium distribution rather than solely on the local equilibrium). This is the situation at hand when \( \tau_s < \tau_c \). Therefore, in order to avoid the reinterpretation step (which is somewhat arbitrary), we used a general method for quasi-equilibrium models available in the literature [8]. Second, the above scheme should not be confused with the entropic time stepping scheme (or the discrete-time \( H \) theorem) [5–9]. In the latter case, the entropy estimate of the collision step is applied after every advection step which guarantees the non-increase of the \( H \) function. In the present case, the continuous-time \( H \) theorem established above delivers the estimate for the parameters of the model (the relaxation time \( \tau_s \) and \( \tau_c \)), while the discrete-time \( H \) theorem is not implemented by scheme (39). Finally, both the methods [5–9] and the present one define equilibria and quasiequilibria as a minimum of the pertinent entropy function under corresponding constraints, with a further optional simplification at low Mach numbers.

In the next section, some numerical tests are reported in order to prove the effectiveness of the proposed scheme with enhanced stability.

IV. NUMERICAL VALIDATION BY LID DRIVEN CAVITY

The proposed scheme with enhanced stability has been already preliminary tested in Ref. [14] by means of the Taylor-Green vortex flow, in order to prove that even large bulk viscosities may be adopted without affecting significantly the numerical results at low Mach numbers. In this section, the effective enhanced stability is measured for the two-dimensional lid driven cavity test, and a relation between stability and accuracy is established. This test has been chosen because it is characterized by singularity of the pressure in the lid corners and hence it is suitable for testing the robustness of the scheme. In the following sections, the enhanced stability is investigated first and then the relation with the accuracy in terms of both vortex locations and global solution is studied.

A. Stability test

Let us solve the standard lid driven cavity flow by using the proposed entropic quasiequilibrium model. Let us consider a square domain \((x, y) \in [0, L] \times [0, L]\) and let us assume \( L = 1 \). Moreover the simulation time is \( t \in [0, t_0] \), where \( t_0 = 100 \), which is considered enough to reach the steady-state conditions for the considered Reynolds numbers (see next). The computational domain is discretized by a uniform collocated grid with \( N \times N \) points. The boundaries are located half cell away from the computational nodes. Let us denote \( x_0 \) the generic boundary computational node. Clearly, in all inner computational nodes \((x \neq x_0)\), Eq. (39) holds for any lattice velocity \( v_i \). In the generic boundary computational node \( x_b \), Eq. (39) holds for any lattice velocity \( v_i \) such that \( x_{b,i} + v_i \delta t \) is still a computational node. In case \( x_{b,i} + v_i \delta t \) is out of the computational grid, then the following boundary condition holds.
the postcollision distribution function defined as
\[ g_i(x_b,t+\delta t) = g_i^*(x_b,t) - 6f_{CM}(\rho,0)v_i \cdot u_b/c^2. \]  
where \( v_i = -v_i \) is the bounce-back lattice velocity, \( g_i^*(x,t) \) is the postcollision distribution function defined as
\[ g_i^*(x,t) = (1 - \omega_i)g(x,t) + \omega_i f_{EQ}(\rho, u, T_{CN}), \]  
and \( u_b \) is the boundary velocity (imposed half cell away from the boundary computational node \( x_b \)). In the following numerical simulations, \( u_b = (u_L,0)^T \) at the lid wall, where \( u_L \) is the lid velocity, and \( u_b = 0 \) for all the other walls. At the lid corners, the lid velocity is imposed, while for other corners the boundary conditions given by Eq. (44) are composed.

Since we are interested in the incompressible limit, the effect of the bulk viscosity \( \xi \), considered as a free tunable parameter, is analyzed. In Figs. 2 and 3, the numerical results are reported for the case of Reynolds number \( Re = u_L L/\nu = 1000 \). Concerning the streamlines, it is confirmed that even large ratios of \( \xi/\nu \) does not practically effect the result. However the limit on the pressure field is more strict because beyond \( \xi/\nu = 10 \) some slight effects on the pressure contours are found. Hence in the following, the bulk viscosity is fixed to \( \xi = 10\nu \).

First of all, let us analyze the pure stability enhancement of the proposed model. It is well known that, the lid driven cavity involves a singular pressure field, in the top lid corners of Fig. 3. For this reason, this numerical test is well suited for checking the actual stability of a numerical scheme in dealing with nonlinear Navier-Stokes equations. In particular, the singular pressure corners excite and promote compressible waves in the pressure field. The key of the entropic quasiequilibrium is to use large bulk viscosity to damp these pressure waves and attenuate them effectively. As reported in Table 1, this attenuation mechanism leads to a consistent enhancement of the stability performance of the scheme. Practically this means that the proposed scheme can deal with much smaller meshes (essentially one fourth of the minimum mesh required by the usual BGK scheme).

Introducing the Mach number \( \text{Ma}=u_L/c \), where \( u_L \) is the lid velocity and \( c \) is the lattice speed, recalling that \( c_s = c/\sqrt{3} \) and \( \nu = \tau c_s^2 \), and using the definition of the Reynolds number.

<table>
<thead>
<tr>
<th>Re</th>
<th>( \nu )</th>
<th>Min (N)</th>
<th>Max (Ma)</th>
<th>Max (Kn)</th>
<th>Min (N)</th>
<th>Max (Ma)</th>
<th>Max (Kn)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1000</td>
<td>1.0 \times 10^{-3}</td>
<td>50</td>
<td>0.2</td>
<td>0.020</td>
<td>25</td>
<td>0.4</td>
<td>0.040</td>
</tr>
<tr>
<td>2000</td>
<td>5.0 \times 10^{-4}</td>
<td>100</td>
<td>0.2</td>
<td>0.0100</td>
<td>50</td>
<td>0.4</td>
<td>0.0200</td>
</tr>
<tr>
<td>3000</td>
<td>3.3 \times 10^{-4}</td>
<td>150</td>
<td>0.2</td>
<td>0.0067</td>
<td>75</td>
<td>0.4</td>
<td>0.0133</td>
</tr>
<tr>
<td>4000</td>
<td>2.5 \times 10^{-4}</td>
<td>200</td>
<td>0.2</td>
<td>0.0050</td>
<td>100</td>
<td>0.4</td>
<td>0.0100</td>
</tr>
<tr>
<td>5000</td>
<td>2.0 \times 10^{-4}</td>
<td>250</td>
<td>0.2</td>
<td>0.0040</td>
<td>125</td>
<td>0.4</td>
<td>0.0080</td>
</tr>
</tbody>
</table>

TABLE I. Lid driven cavity stability test. Some numerical tests are reported for different kinematic viscosity \( \nu \) (and consequently Reynolds number Re) for both standard BGK and proposed entropic quasi-equilibrium model (EQE). The bulk viscosity is fixed to \( \xi = 10\nu \) and it is a pure numerical artifact. The minimum number min(N) of points along each coordinate for running stable simulations is reported. The latter corresponds to the maximum Mach number tolerated by the numerical scheme, namely max (Ma), where \( \text{Ma}=u_L/c \), \( u_L \) is the lid velocity, and \( c \) is the lattice speed. In the numerical simulations, \( \text{Ma}=0.01 \) Re Kn is adopted.
number $\text{Re} = u_L L/\nu$, it is possible to derive the following relation (analogous to the von Karman relation):

$$Ma = \frac{\tau}{3\partial t} \text{Re Kn},$$

(46)

where $\text{Kn} = \delta x L/1/N$ and $N$ is the number of grid points along length $L$ (the lattice Knudsen number). From the asymptotic analysis of the LB model based on the assumption that both Kn and Ma are small, it is possible to prove that there are two terms in the recovered macroscopic equations, in addition to those prescribed by the incompressible Navier-Stokes equations, which are respectively $O(\text{Kn}^2)$ and $O(\text{Ma Kn})$ [24]. Hence, two strategies are possible. In case one wants to obtain a second-order numerical method with regards to the space resolution, i.e., with regards to Kn, taking into account Eq. (46), $Ma \sim \text{Kn}$ must be selected, which means $\tau/\partial t \sim O(1)$, or equivalently keeping $\tau/\partial t$ fixed on different meshes. The latter corresponds to the so-called diffusive (or parabolic) scaling. On the other hand, in case of advective (or hyperbolic) scaling, one wants to keep $\text{Ma}$ independent of lattice $\text{Kn}$, then $\tau_j$ becomes constant independent of the considered mesh. Below we use diffusive scaling when setting up the parameters of various simulations.

In particular, in Table I, since $\text{Ma}/\text{Kn}$ becomes a constant in the diffusive scaling, then any (stability and/or accuracy) constraint on $\text{Kn}=1/N$ can be formulated also in terms of $\text{Ma}$. Hence in Table I, the enhancement of the stability performance of the scheme can also be expressed as the ability to deal with much larger Mach numbers, i.e., to perform much faster simulations. Obviously in this case, deviations from the Maxwell-Boltzmann equilibrium may spoil the accuracy of the numerical solutions.

Concerning the latter point, it is worth the effort to point out that the stability threshold appears quite earlier than the non-negativity condition for the generalized population list. Recalling the definition given by Eq. (3), it is easy to derive the positivity condition as $\text{Ma} \leq \sqrt{2}/3 = 0.8165$. However the instability for EQE model appears at roughly $\text{Ma}=0.4$. This means that, at least for the present test case, the stability region fits well into the non-negativity region, where the generalized Maxwellian given by Eq. (3) is defined.

**B. Stability and accuracy test with regards to vortex locations**

Clearly a fair comparison among the numerical schemes should take into account the actual accuracy as well. In fact, improving the bulk viscosity may allows one to adopt rougher meshes but reducing the recovered accuracy. In order to check this, let us consider the case $\text{Re}=5000$. For this Reynolds number, it is well known that four main vortexes appear in the lid driven cavity, namely, upper-left (U-L), mid-central (M-C), lower-left (L-L), and lower-right (L-R), see Fig. 4. It is possible to compute the actual “centers” of the vortexes as the local extrema of the stream function $\psi$, defined as

$$u_x = \frac{\partial \psi}{\partial y}, \quad u_y = -\frac{\partial \psi}{\partial x}.$$  

(47)

Let us denote $\mathbf{x}_q$ the location of the vortex $q$, according to the adopted numerical scheme and after postprocessing. Hence it is possible to introduce the following errors: the vortex error $E_q$ for the $q$th vortex, namely,

$$E_q = \frac{||\mathbf{x}_q - \mathbf{x}_q^*||}{||\mathbf{x}_q^*||},$$

(48)

where $||.||$ is the $L_2$-norm and $E_q$ is the (arithmetic) mean error. In Table II, the results of the numerical simulations are...
TABLE II. Lid driven cavity stability and accuracy test. The Reynolds number is $Re=5000$, the kinematic viscosity $\nu=0.0002$ and the bulk viscosity $\xi=0.002$. Different meshes are considered. For each numerical calculation, the locations of the four main vortexes (see Fig. 4) are computed by postprocessing on the same finer mesh $250 \times 250$ and compared with some reference values [25–28]. The error on the location of each vortex $q_i$, namely, $E_{xq}$, is computed by Eq. (48), while $E_{xq}$ is the arithmetic average among all the errors. All the models were run on same hardware. Actual run time is normalized to the run time taken by the EQE model on the $170 \times 170$ grid.

<table>
<thead>
<tr>
<th>Run time</th>
<th>Axis</th>
<th>M-C</th>
<th>L-L</th>
<th>L-R</th>
<th>U-L</th>
<th>Errors on vortex locations (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td>M-C</td>
</tr>
<tr>
<td>References [25–28]</td>
<td>NA</td>
<td>$x_q$</td>
<td>0.51393333</td>
<td>0.07040000</td>
<td>0.82213333</td>
<td>0.06460000</td>
</tr>
<tr>
<td>EQE 125×125</td>
<td>0.35</td>
<td>$x_q$</td>
<td>0.51004016</td>
<td>0.07630522</td>
<td>0.81124498</td>
<td>0.05220884</td>
</tr>
<tr>
<td>EQE 150×150</td>
<td>0.61</td>
<td>$x_q$</td>
<td>0.51807229</td>
<td>0.07630522</td>
<td>0.80321285</td>
<td>0.06425703</td>
</tr>
<tr>
<td>EQE 170×170</td>
<td>1.00</td>
<td>$x_q$</td>
<td>0.52208835</td>
<td>0.07228916</td>
<td>0.80321285</td>
<td>0.06508887</td>
</tr>
<tr>
<td>LQE 170×170</td>
<td>0.65</td>
<td>$x_q$</td>
<td>0.51004016</td>
<td>0.07228916</td>
<td>0.80722892</td>
<td>0.06425703</td>
</tr>
<tr>
<td>EQE 200×200</td>
<td>2.06</td>
<td>$x_q$</td>
<td>0.52208835</td>
<td>0.06827309</td>
<td>0.80722892</td>
<td>0.06425703</td>
</tr>
<tr>
<td>EQE 250×250</td>
<td>4.97</td>
<td>$x_q$</td>
<td>0.52208835</td>
<td>0.06827309</td>
<td>0.80321285</td>
<td>0.06425703</td>
</tr>
<tr>
<td>ELB$^b$ 320×320</td>
<td>NA</td>
<td>$x_q$</td>
<td>0.51750000</td>
<td>0.07730000</td>
<td>0.80560000</td>
<td>0.06640000</td>
</tr>
<tr>
<td>BGK 250×250</td>
<td>2.84</td>
<td>$x_q$</td>
<td>0.51807229</td>
<td>0.07630522</td>
<td>0.80722892</td>
<td>0.06425703</td>
</tr>
</tbody>
</table>

$^b$Reference [29].

reported. Essentially for the present test, EQE model is able to deal with a very coarse mesh 125×125, which is roughly one fourth of the minimum mesh for the BGK model, namely, 250×250. However, in terms of accuracy, this coarse mesh is not able to produce the same performance for computing the vortex locations, even though the numerical velocity field is interpolated on the same fine mesh. Hence the mesh of the EQE must be refined. It comes out that the EQE model, with a rougher mesh 170, which is roughly 50% faster than the EQE model, because the former avoids the cumbersome calculations due to the Cardano formula. Moreover, it is even more accurate than the full.

Finally, in Table II, the results obtained by the expanded model in the low Mach number limit (LQE) are reported as well for the mesh 170×170. First of all, the LQE model is roughly 50% faster than the EQE model, because the former avoids the cumbersome calculations due to the Cardano formula. Moreover, it is even more accurate than the full.

FIG. 5. Streamlines for the lid driven cavity flow with $Re=5000$, $\nu=0.0002$ ($\xi=0.002$ for the EQE model only). The reference locations $x_q^*$ for the four main vortexes are reported [25–28] (square markers). Moreover the computed locations $x_q$ based on the postprocessing are reported too for both BGK (circle markers) and EQE model (diamond markers).
entropy-based model (1.80% < 2.68%), because it involves a smaller number of operations and hence it is less affected by the round-off errors. It is worth to recall that the difference between LQE and EQE is $O(Ma^3)$, i.e., it is 2 orders of magnitude smaller than the accuracy of the numerical scheme in case of diffusive scaling, when the Mach number is selected proportional to the Knudsen number. For these reasons, use of LQE in practical simulations is recommended, even though more test cases need to be studied.

C. Stability and accuracy test with a global solution

Even though the computation of the vortex locations is a standard procedure for checking the accuracy of the considered numerical scheme, we also compared globally the recovered solutions with a reference solution. The computational domain and the physical parameters are identical to those considered in the previous section, i.e., $L=1$, $t_0=100$, $\nu=0.0002$, $\xi=10\nu$ (for EQE and LQE), $u_t=1$, $Re=5000$.

The reference solution has been obtained by means of a commercial computational fluid-dynamics (CFD) code FLUENT®, based on the finite-volume method (FVM), which is a quite popular tool in computational engineering. First of all, the reference solution was computed by using double precision representation, i.e., binary floating-point number format using 64 bits, for reducing the effects of the machine round-off precision. Concerning the spatial discretization, the second-order up-wind was considered for the discretization of the momentum fluxes. For the resolution of the discrete equations, a segregated approach was used; i.e., the continuity and momentum equations were solved alternatively by means of an iterative solution up to convergence. The SIMPLE algorithm [30] was used for the pressure-velocity coupling: essentially this algorithm is used to solve the Poisson equation coming out by combining the momentum equation with the divergence-free condition for the low Mach number limit. As a convergence criterion, it was required that all the residuals are smaller than $10^{-7}$, i.e., the imbalances in all the discretized equations summed over all the computational cells are smaller than $10^{-7}$ during the final convergence step. The reference solution is indicated by $(u'_x, u'_y, p')(x, y)$, where $u'_x$, $u'_y$ are the velocity components, $p'$ is the pressure and $x = (x, y)^T \in G(N)$ with $G(N)$ meaning the computational grid made of $N\times N$ homogeneously spanned (collocated) computational nodes. The values on the collocated grid are computed by interpolation because the commercial code uses a staggered grid (as popular for avoiding checkerboard instability in FVM). In particular, the grid $1025 \times 1025$ was used for computing the reference solution in the following calculations. The actual reference for a rougher mesh $N<1025$ was obtained by means of bicubic interpolation, i.e., cubic interpolations along both Cartesian axes.

In order to characterize properly the behavior of the proposed schemes, an extensive simulation plan has been defined. The Knudsen number, i.e., the spatial resolution, was selected such that $Kn \in \{1/128, 1/160, 1/192, 1/224, 1/256\}$ (linearly spanned), or equivalently the computational nodes along each Cartesian axis was selected such that $N \in \{128, 160, 192, 224, 256\}$. Taking into account Eq. (46) and adopting the diffusive scaling, the Mach number was tuned by means of the constant $\tau/\delta t$, which must be mesh independent. In particular, the Mach number was selected such that $Ma \in \{0.02, 0.04, 0.1, 0.2, 0.4\}$ (roughly logarithmically spanned). Finally, for each combination of the previous parameters, three schemes were tested: the standard lattice BGK, EQE, and LQE. This leads to a simulation plan made of a total $5 \times 5 \times 3 = 75$ runs.

The global errors were computed for different meshes, namely,

$$E_{ux} = \frac{1}{u_t} \sqrt{\frac{1}{N^2} \sum_{x \in G(N)} (u_x - u_x')^2}, \quad (49)$$
$$E_{uy} = \frac{1}{u_t} \sqrt{\frac{1}{N^2} \sum_{x \in G(N)} (u_y - u_y')^2}, \quad (50)$$
$$E_p = \frac{1}{u_t} \sqrt{\frac{1}{N^2} \sum_{x \in G(N)} (p - p')^2}, \quad (51)$$

where the pressure $p = c_s^2(p - p_0)$ has been normalized in order to have the same mean of the reference solution $p'$. The numerical results are reported in Table III. First of all, it is not surprising that an unstable behavior may appear for low values of the Mach number. In fact, recalling Eq. (46), the quantity $\tau/\delta t$ (mesh independent under the diffusive scaling), namely,

$$\frac{\tau}{\delta t} = 3 \frac{Ma}{Re Kn}, \quad (52)$$

becomes small when the Mach number is small. Consequently, taking into account Eq. (43), $\omega_t$ tends to 2, which is the upper stability threshold for the evolution Eq. (39), in terms of transformed distribution function $g$. Comparing different numerical schemes, EQE and LQE show a wider stability region since these schemes allow one to consider quite rough meshes up to $N=128$, while the standard BGK requires at least $N=256$. Moreover, EQE is characterized by better accuracy in recovering the global solution than LQE and, as expected, the discrepancy between these schemes increases as long as the Mach number increases. Considering the EQE scheme, it is possible to recover the same mean accuracy of the best lattice BGK simulation ($1/Kn=256$ and $Ma=0.20$), i.e., $E_m=1.2\%$, by using a rougher mesh with $1/Kn=192$ and $Ma=0.20$, which corresponds roughly to half of the previous mesh.

Finally, it is interesting to analyze the mean errors for EQE on the parameter plane given by $(Kn, Ma)$, as reported in Table IV, where the best results are shown in bold. For any mesh, i.e., for any numerical Knudsen number, there is an optimal Mach number which yields the most accurate results. Larger Mach numbers tend to violate the assumption used to derive the discrete local equilibrium, while smaller Mach numbers yield smaller dimensionless viscosities expressed in lattice units, which lead to more inaccurate numerical results. This optimal Mach number slightly increases for rougher meshes. The above systematic simulation plan
TABLE III. Lid driven cavity stability and global accuracy test. The Reynolds number is Re=5000, the kinematic viscosity $\nu=0.0002$ and the bulk viscosity $\xi=0.002$ (for EQE and LQE). Different meshes (and consequently different Knudsen numbers $N=1/\text{Kn}$ and different Mach numbers are considered. The global errors on the velocity components $E_{ux}$ and $E_{uy}$ and on pressure $E_p$ are computed by Eq. (49), while $E_m$ is the arithmetic average among all the previous errors. The label “unstable” means that the calculation could not be performed with that combination of simulation parameters.

<table>
<thead>
<tr>
<th>1/Kn</th>
<th>Scheme</th>
<th>Error</th>
<th>Ma</th>
<th></th>
<th></th>
<th></th>
<th></th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td>0.02</td>
<td>0.04</td>
<td>0.10</td>
<td>0.20</td>
<td>0.40</td>
</tr>
<tr>
<td>128</td>
<td>BGK</td>
<td></td>
<td>Unstable</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td>EQE</td>
<td></td>
<td>$E_{ux}$</td>
<td>Unstable</td>
<td>0.024998</td>
<td>0.019096</td>
<td>0.021838</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>$E_{uy}$</td>
<td>Unstable</td>
<td>0.025482</td>
<td>0.019629</td>
<td>0.021678</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>$E_p$</td>
<td>Unstable</td>
<td>0.022485</td>
<td>0.013274</td>
<td>0.008023</td>
</tr>
<tr>
<td></td>
<td>EQE</td>
<td></td>
<td>$E_{ux}$</td>
<td>Unstable</td>
<td>0.025654</td>
<td>0.021368</td>
<td>0.025859</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>$E_{uy}$</td>
<td>Unstable</td>
<td>0.026074</td>
<td>0.021697</td>
<td>0.027291</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>$E_p$</td>
<td>Unstable</td>
<td>0.022584</td>
<td>0.013853</td>
<td>0.011115</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>$E_m$</td>
<td>Unstable</td>
<td>0.024771</td>
<td>0.018973</td>
<td>0.021422</td>
</tr>
<tr>
<td>160</td>
<td>BGK</td>
<td></td>
<td>Unstable</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td>EQE</td>
<td></td>
<td>$E_{ux}$</td>
<td>0.020997</td>
<td>0.019602</td>
<td>0.017802</td>
<td>0.015361</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>$E_{uy}$</td>
<td>0.021505</td>
<td>0.020143</td>
<td>0.018389</td>
<td>0.016036</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>$E_p$</td>
<td>0.060736</td>
<td>0.036427</td>
<td>0.016648</td>
<td>0.010302</td>
</tr>
<tr>
<td></td>
<td>EQE</td>
<td></td>
<td>$E_{ux}$</td>
<td>0.021026</td>
<td>0.019723</td>
<td>0.018533</td>
<td>0.017777</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>$E_{uy}$</td>
<td>0.021532</td>
<td>0.020251</td>
<td>0.019038</td>
<td>0.018193</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>$E_p$</td>
<td>0.060735</td>
<td>0.036431</td>
<td>0.016770</td>
<td>0.010955</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>$E_m$</td>
<td>0.034431</td>
<td>0.025468</td>
<td>0.018113</td>
<td>0.017365</td>
</tr>
<tr>
<td>192</td>
<td>BGK</td>
<td></td>
<td>Unstable</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td>EQE</td>
<td></td>
<td>$E_{ux}$</td>
<td>0.017678</td>
<td>0.016956</td>
<td>0.015552</td>
<td>0.013709</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>$E_{uy}$</td>
<td>0.018232</td>
<td>0.017524</td>
<td>0.016141</td>
<td>0.014271</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>$E_p$</td>
<td>0.052492</td>
<td>0.029327</td>
<td>0.013544</td>
<td>0.008573</td>
</tr>
<tr>
<td></td>
<td>EQE</td>
<td></td>
<td>$E_{ux}$</td>
<td>0.017710</td>
<td>0.017083</td>
<td>0.016296</td>
<td>0.015929</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>$E_{uy}$</td>
<td>0.018260</td>
<td>0.017635</td>
<td>0.016820</td>
<td>0.016423</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>$E_p$</td>
<td>0.052491</td>
<td>0.029335</td>
<td>0.013680</td>
<td>0.009226</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>$E_m$</td>
<td>0.029487</td>
<td>0.021351</td>
<td>0.015599</td>
<td>0.013859</td>
</tr>
<tr>
<td>224</td>
<td>BGK</td>
<td></td>
<td>Unstable</td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td>EQE</td>
<td></td>
<td>$E_{ux}$</td>
<td>0.016072</td>
<td>0.015457</td>
<td>0.014431</td>
<td>0.012944</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>$E_{uy}$</td>
<td>0.016653</td>
<td>0.016004</td>
<td>0.014826</td>
<td>0.013269</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>$E_p$</td>
<td>0.045503</td>
<td>0.024187</td>
<td>0.011551</td>
<td>0.007471</td>
</tr>
<tr>
<td></td>
<td>EQE</td>
<td></td>
<td>$E_{ux}$</td>
<td>0.016105</td>
<td>0.015583</td>
<td>0.015152</td>
<td>0.015011</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>$E_{uy}$</td>
<td>0.016682</td>
<td>0.016120</td>
<td>0.015555</td>
<td>0.015426</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>$E_p$</td>
<td>0.045504</td>
<td>0.024199</td>
<td>0.011690</td>
<td>0.008124</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>$E_m$</td>
<td>0.026097</td>
<td>0.018634</td>
<td>0.014132</td>
<td>0.012854</td>
</tr>
</tbody>
</table>
allows one to recover a complete picture of the enhanced numerical stability of the proposed schemes, without neglecting the effects on accuracy as well.

V. CONCLUSIONS

Taking advantage of the analytically generalized Maxwell distribution function, a quasiequilibrium model (EQE) is proposed, which enjoys both the $H$ theorem and the additional free-tunable parameter for controlling the bulk viscosity and enhancing the stability of the model, when the incompressible limit is the only concern. A simpler model based on a proper expansion with regards to the low Mach number limit is derived as well (LQE). Because all the results above are derived in a closed form, numerical implementations of both models is straightforward, is not essentially different from the standard LBGK scheme, and the practical details are reported. Extensive numerical tests concerning the lid driven cavity are considered in order to verify the effective transport coefficients and the enhancement of the stability region.

Since the lid driven cavity test involves a singular pressure field, this test is particularly suitable for checking the stability of a numerical scheme dealing with incompressible limit. We started first by considering some specific features of the flow concerning the main vortexes. It comes out that the proposed EQE model, with a rougher mesh than that used by the BGK model, can achieve the same accuracy in computing the main vortex locations. This leads to an effective computational speed-up of 2.84 in terms of run time. The results are even more encouraging for the model expanded in the low Mach number limit (LQE). In this test, the LQE model is roughly 50% faster than the EQE model, because the first avoids the cumbersome calculations due to the Cardano formula. Moreover, it is even more accurate than the EQE model with the same mesh, because it involves a smaller number of operations and hence it is less effected by the round-off errors. For the previous reasons, the LQE model leads to an effective computational speed-up of 4.37 in terms of run time, with regards to the usual lattice BGK model.

<table>
<thead>
<tr>
<th>1/Kn</th>
<th>Scheme</th>
<th>Error</th>
<th>Ma</th>
<th>0.02</th>
<th>0.04</th>
<th>0.10</th>
<th>0.20</th>
<th>0.40</th>
</tr>
</thead>
<tbody>
<tr>
<td>256</td>
<td>BGK</td>
<td>$E_{ux}$</td>
<td>Unstable</td>
<td>0.014487</td>
<td>0.019473</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>$E_{uy}$</td>
<td>Unstable</td>
<td>0.014560</td>
<td>0.019406</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>$E_{p}$</td>
<td>Unstable</td>
<td>0.007048</td>
<td>0.007872</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>$E_{m}$</td>
<td>Unstable</td>
<td>0.012031</td>
<td>0.015583</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td></td>
<td>EQE</td>
<td>$E_{ux}$</td>
<td>0.015062</td>
<td>0.014615</td>
<td>0.013801</td>
<td>0.012247</td>
<td>0.016124</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>$E_{uy}$</td>
<td>0.015539</td>
<td>0.014948</td>
<td>0.013954</td>
<td>0.012617</td>
<td>0.015883</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>$E_{p}$</td>
<td>0.039344</td>
<td>0.020624</td>
<td>0.010162</td>
<td>0.006665</td>
<td>0.004403</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>$E_{m}$</td>
<td>0.023315</td>
<td>0.016729</td>
<td>0.012639</td>
<td>0.010509</td>
<td>0.012137</td>
<td></td>
</tr>
<tr>
<td></td>
<td>LQE</td>
<td>$E_{ux}$</td>
<td>0.015094</td>
<td>0.014738</td>
<td>0.014543</td>
<td>0.014439</td>
<td>0.019189</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>$E_{uy}$</td>
<td>0.015570</td>
<td>0.015073</td>
<td>0.014676</td>
<td>0.014592</td>
<td>0.019095</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>$E_{p}$</td>
<td>0.039345</td>
<td>0.020637</td>
<td>0.010309</td>
<td>0.007368</td>
<td>0.008023</td>
<td></td>
</tr>
<tr>
<td></td>
<td></td>
<td>$E_{m}$</td>
<td>0.023336</td>
<td>0.016816</td>
<td>0.013176</td>
<td>0.012133</td>
<td>0.015436</td>
<td></td>
</tr>
</tbody>
</table>

TABLE IV. Lid driven cavity stability and global accuracy test: parameter plane for EQE. The Reynolds number is Re=5000, the kinematic viscosity $\nu=0.0002$ and the bulk viscosity $\xi=0.002$. Different meshes (and consequently different Knudsen numbers) $N=1/Kn$ and different Mach numbers are considered. The arithmetic average $E_m$ among all global errors is reported and the best results are reported in bold. The label “unstable” means that the calculation could not be performed with that combination of simulation parameters.

<table>
<thead>
<tr>
<th>Ma</th>
<th>N=1/Kn</th>
<th>256</th>
<th>224</th>
<th>192</th>
<th>160</th>
<th>128</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.40</td>
<td></td>
<td>0.015436</td>
<td>0.012525</td>
<td>0.013098</td>
<td>0.014106</td>
<td>0.017180</td>
</tr>
<tr>
<td>0.20</td>
<td></td>
<td><strong>0.012133</strong></td>
<td><strong>0.011228</strong></td>
<td><strong>0.012184</strong></td>
<td><strong>0.013899</strong></td>
<td>0.017333</td>
</tr>
<tr>
<td>0.10</td>
<td></td>
<td>0.013176</td>
<td>0.013603</td>
<td>0.015079</td>
<td>0.017613</td>
<td>0.024322</td>
</tr>
<tr>
<td>0.04</td>
<td></td>
<td>0.016816</td>
<td>0.018549</td>
<td>0.021269</td>
<td>0.025391</td>
<td>Unstable</td>
</tr>
<tr>
<td>0.02</td>
<td></td>
<td>0.023315</td>
<td>0.026076</td>
<td>0.029467</td>
<td>0.034413</td>
<td>Unstable</td>
</tr>
</tbody>
</table>

016702-13
For investigating systematically these results, an extensive simulation plan has been defined, consisting of five values for the Mach number, five values for the numerical Knudsen number and comparing the standard lattice BGK with the proposed schemes (both EQE and LQE). Moreover the accuracy in recovering the global solution was considered too, by comparing the numerical results with a reference solution obtained by a popular commercial tool. It came out that EQE is characterized by better accuracy in recovering the global solution than LQE and, as expected, the discrepancy between these schemes increases as far as the Mach number increases too. Considering the EQE scheme, it is possible to recover the same mean accuracy of the best lattice BGK simulation $(1/\text{Kn}=256$ and $\text{Ma}=0.20)$ by using a rougher mesh with $1/\text{Kn}=192$ and $\text{Ma}=0.20$, which corresponds again roughly to half of the previous mesh. Hence also the systematic simulation plan confirms the previous results about some specific features of the flow.

ACKNOWLEDGMENTS

P.A. acknowledges support of EnerGRID project. I.V.K. acknowledges support of CCEM-CH.

APPENDIX: GENERALIZATION TO 3D CASE BY D3Q27 LATTICES

Since the quasiequilibrium is the product of one-dimensional functions in each direction [18], it is very simple to solve the minimization problem in the 3D case, namely, for the D3Q27 lattice,

\begin{align*}
 f_{G(0,0,0)} &= \frac{\rho}{c^6} (c^2 - P_{xx})(c^2 - P_{yy})(c^2 - P_{zz}), \\
 f_{G(\pm 1,0,0)} &= \frac{\rho}{c^6} (P_{xx} \pm cu_x)(c^2 - P_{yy})(c^2 - P_{zz}), \\
 f_{G(0,\pm 1,0)} &= \frac{\rho}{c^6} (c^2 - P_{xx})(P_{yy} \pm cu_y)(c^2 - P_{zz}), \\
 f_{G(0,0,\pm 1)} &= \frac{\rho}{c^6} (c^2 - P_{xx})(P_{yy} \pm cu_y)(P_{zz} \pm cu_z), \\
 f_{G(\pm 1,1,0)} &= \frac{\rho}{c^6} (c^2 - P_{xx})(P_{yy} \pm cu_y)(P_{zz} \pm cu_z), \\
 f_{G(0, \pm 1,1)} &= \frac{\rho}{c^6} (P_{xx} \pm cu_x)(P_{yy} \pm cu_y)(P_{zz} \pm cu_z), \\
 f_{G(\pm 1,0,1)} &= \frac{\rho}{c^6} (P_{xx} \pm cu_x)(P_{yy} \pm cu_y)(P_{zz} \pm cu_z).
\end{align*}

(A1)

In order to ensure the positivity of the latter $f_G$, it is required that $P \in \Psi$ where $\Psi = \{P : c|u_x| < P_{xx} < c^2, c|u_y| < P_{yy} < c^2, c|u_z| < P_{zz} < c^2\}$ is a convex box in the space of parameters for each velocity $u$. Note that, when setting $\Pi_z = 0$ in the nine populations, $f_{G(0,0,0)}$, $f_{G(\pm 1,0,0)}$, $f_{G(0,\pm 1,0)}$, and $f_{G(\pm 1,1,0)}$ [Eq. (A1)], we obtain the quasiequilibrium on the two-dimensional D2Q9 lattice, given by Eq. (30).

With the help of $f_G$ [Eq. (A1)], let us derive a constrained equilibrium $f_c$ which brings the H-function to a minimum among all the population schemes lists with a fixed trace of the pressure tensor $T(P) = P_{xx} + P_{yy} + P_{zz}$. In terms of the parameter set $\Psi$, this is equivalent to require that the point $C = (P_{xx}^C, P_{yy}^C, P_{zz}^C)$ belongs to a surface portion $A_T = \{P \in \Psi : P_{xx} + P_{yy} + P_{zz} = T\}$, and the constrained equilibrium $C$ is that minimizing the function $H_G$ [Eq. (41)] on $A_T$. Since the restriction of a convex function to a line is also convex, the solution to the latter problem exists and is found by

\begin{align*}
 \frac{dH_G}{dp_{xx}} & = \left[ \frac{\partial H_G}{\partial p_{xx}} - \frac{\partial H_G}{\partial p_{zz}} \right]_{p_{xx}=T-p_{yy}} = 0, \\
 \frac{dH_G}{dp_{yy}} & = \left[ \frac{\partial H_G}{\partial p_{yy}} - \frac{\partial H_G}{\partial p_{zz}} \right]_{p_{yy}=T-p_{zz}} = 0
\end{align*}

(A2) (A3)

where $T^r = T - P_{yy}$ and $T^r = T - P_{zz}$. It is possible to compute each of the partial derivatives involved in the previous expressions by the following rule:

\begin{equation}
 \frac{\partial H_G}{\partial p_{aa}} = \frac{\rho}{c^2} \ln (P_{aa} / u_{aa}) = \frac{\rho}{c^2} \ln \left( \frac{\sqrt{P_{aa}}}{\sqrt{c^2 - P_{aa}}} \right)^2
\end{equation}

(A4)

Each of Eqs. (A2) and (A3) yields to a cubic equation in terms of the normal stress difference $N^r = P_{xx}^C - P_{zz}^C$ and $N^m = P_{xx}^C - P_{yy}^C$ respectively. Each cubic equation admits a solution like that described by Eq. (9). In particular, in the low Mach number limit, as already done in Eq. (32), it is possible to approximate exact solutions by

\begin{align*}
 P_{xx}^C(u,T) &= \frac{(T - P_{yy}^C) + (u_x^2 - u_x^2)}{2} + O(\text{Ma}^4), \\
 P_{yy}^C(u,T) &= \frac{(T - P_{xx}^C) + (u_y^2 - u_y^2)}{2} + O(\text{Ma}^4), \\
 P_{zz}^C(u,T) &= \frac{(T - P_{xx}^C) + (u_z^2 - u_z^2)}{2} + O(\text{Ma}^4).
\end{align*}

(A5)

Clearly the previous conditions are not linearly independent, or equivalently the rank of the previous system of equations is actually equal to three, and it admits the following solutions:

\begin{equation}
 P_{aa}^C(u,T) = \frac{T}{3} + u_a + \frac{u_x^2 + u_y^2 + u_z^2}{3} + O(\text{Ma}^4),
\end{equation}

(A6)

which corresponds to Eq. (32) in the two-dimensional case. Further details about the three-dimensional case are reported in Ref. [18].


I. Karlin and P. Asinari, Physica A (to be published).


