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Article

# Electromagnetic Interaction Model between an Electric Motor and a Magnetorheological Brake

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**Abstract:** This article focuses on modelling and validating a groundbreaking magnetorheological braking system. Addressing shortcomings in traditional automotive friction brake systems, including response delays, wear, and added mass from auxiliary components, the study employs a novel brake design combining mechanical and electrical elements for enhanced efficiency. Utilizing magnetorheological (MR) technology within a motor–brake system, the investigation explores the influence of external magnetic flux from the nearby motor on MR fluid movement, particularly under high-flux conditions. The evaluation of a high-magnetic-field mitigator is guided by simulated findings with the objective of resolving potential issues. An alternative method of resolving an interaction between an electric motor and a magnetorheological brake is presented. In addition, to test four configurations, multiple absorber materials are reviewed.

**Keywords:** magnetorheological fluid; braking system; in-wheel motors; electromagnetic interaction; braking efficiency

## 1. Introduction

The surge in interest in electric vehicles (EVs) is propelled by their potential to mitigate fossil fuel dependency and reduce emissions, with a critical focus on the safety-centric aspect of EV design: the braking system. This paper investigates the integration of a novel magnetorheological (MR) braking system with an in-wheel hub motor, aiming to enhance dependability and efficiency. Magnetorheological brakes [1], utilizing magnetorheological fluid principles, hold promise for improved performance and control compared to traditional braking systems. Through an analysis of the characteristics and performance of these brakes placed within in-wheel hub motors, this study provides comprehensive insights into their viability as an advanced braking solution for EVs [2,3]. Examining the effectiveness of a magnetorheological fluid on a magnetorheological brake, this research addresses a gap in the widespread use of wheel hub motor–brake systems by diving into the limited research on its effects on magnetorheological brakes with radial orientation. The complexity of the case study analysis reflects the need to simulate the electromagnetic external behaviour of an electric motor whose data on the internal layout are not available. The goal is to represent, in the most realistic way possible, the electromagnetic emissions, as it is possible to evaluate their effects on a magnetorheological tool.

Bibliographically, multiple MR applications have been deployed over recent years and not only in the automotive environment. For example, multiple applications to seismic MR dampers have been proposed [4], and some of those present protections for server stations [5], where electromagnetic interaction analyses should be performed to ensure the expected behaviour during the magnetization periods. For this reason, it is important to describe the procedure for evaluating the electromagnetic interactions with an MR tool, as there is no such literature available.

This study investigates the electric motor’s influence on the magnetic field around the brake system and analyses the magnetorheological fluid, rotor, and other components. New



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technical advancements in engineering have spurred opportunities to optimize conventional braking systems in the automotive domain, particularly through the upgrading of these systems using magnetorheological operational braking systems. These systems offer reliability, with the magnetorheological fluid serving as the operational fluid. MR fluids, as a class of smart fluids, undergo apparent viscosity modifications under the influence of an applied magnetic field. Combining carrier fluid, magnetic particles, and additives, MR fluids exhibit dynamic behaviour. The MR fluid MRF-132-DG was selected for its low viscosity under a zero magnetic field and the high viscosity reached at maximum magnetization, conditions which are ideal for the chosen type of application.

The proposed novel braking system is composed of an MR brake attached to an electric in-wheel motor [6,7]. This combination of the two elements enables significant performance improvements regarding the control strategy of the thermal management of the system. Having the motor present close to the brake, the risk of a magnetic interaction between the two parts should be considered. It is necessary that the fluid is kept under a specific magnetic excitation level, so that no unwanted braking manoeuvres are encountered.

The chosen motor is Emrax 348 [8,9], as its dimensions and power characteristics are compatible with the automotive application needed. Representing this motor in detail is pivotal for indicating the correct motor–brake interaction. Unfortunately, due to having a limited amount of information regarding the geometry of the magnets and the coils inside the motor itself, simulating its behaviour [10] becomes very complex.

In this paper, multiple electric motor (EM) representative models have been taken into consideration to reproduce the realistic magnetic field intensity and direction of the actual EM for distinct stages of its functionality.

When determining the magnetic field's strength, the EMC Directive's maximum permitted for magnetic emission must be taken into account from a regulatory perspective. These regulations were found in the European General Directives (2014/30/EU) [11], as well as in the Low Voltage Directive (2014/35/EU) and Machinery Directive (2006/42/EC), along with relevant standards such as EN 60034-1:2010 [12], ISO 12100:2010, and EN 60529:1991/A1:2000/A2:2013 [13].

To accommodate the broad field range, an average electromagnetic field from 0 kHz to 1 MHz or an electromagnetic field flux from 0 to 1 tesla was considered. Altair Flux simulation software was then used to assess different values within this range, ensuring a thorough examination of electromagnetic field exposure. This comprehensive approach enhances the guidelines' relevance and accuracy in safeguarding human health amid the evolving landscape of telecommunications technology.

## 2. Electric Motor Representation

Due to their high torque-to-weight ratio, axial flux motors are promising for automotive and aerospace applications. Being able to imitate their behaviour is useful for conducting a variety of investigations. Two main possibilities to describe their electromagnetic behaviour were considered:

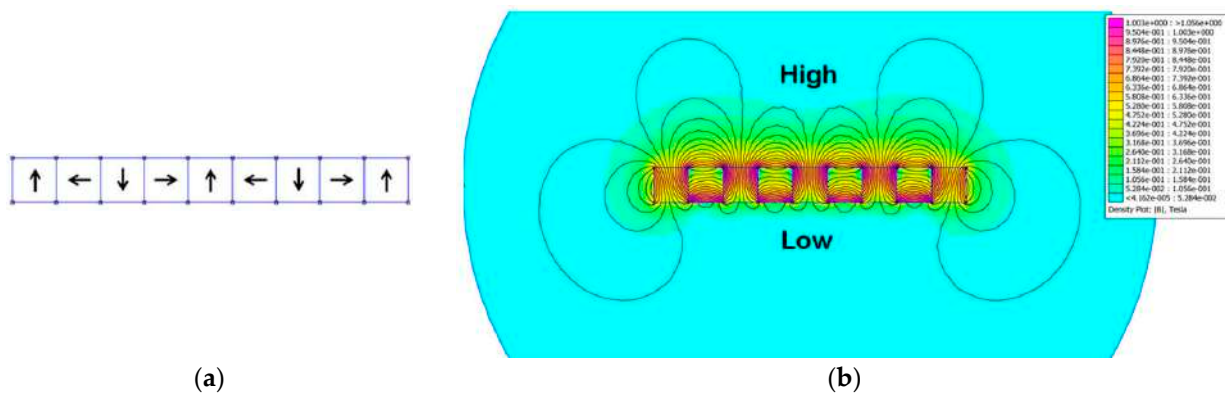
- (a) Halbach array.
- (b) Helmholtz coil.

A detailed comparison is conducted to determine which is the more comparable to the axial flux behaviour. By using a Helmholtz coil arrangement, the motor makes use of its capacity to generate a perpendicular magnetic field, guaranteeing electromagnetic coverage on all surfaces.

The goal of this calculated move is to fit the motor representation to the real motor behaviour in terms of field line direction and intensity growth.

### 2.1. The Halbach Array

According to [14,15], a Halbach array is a unique configuration of permanent magnets intended to strengthen the magnetic field on one side while cancelling it on the other via a spatially revolving pattern of magnetization (Figure 1).

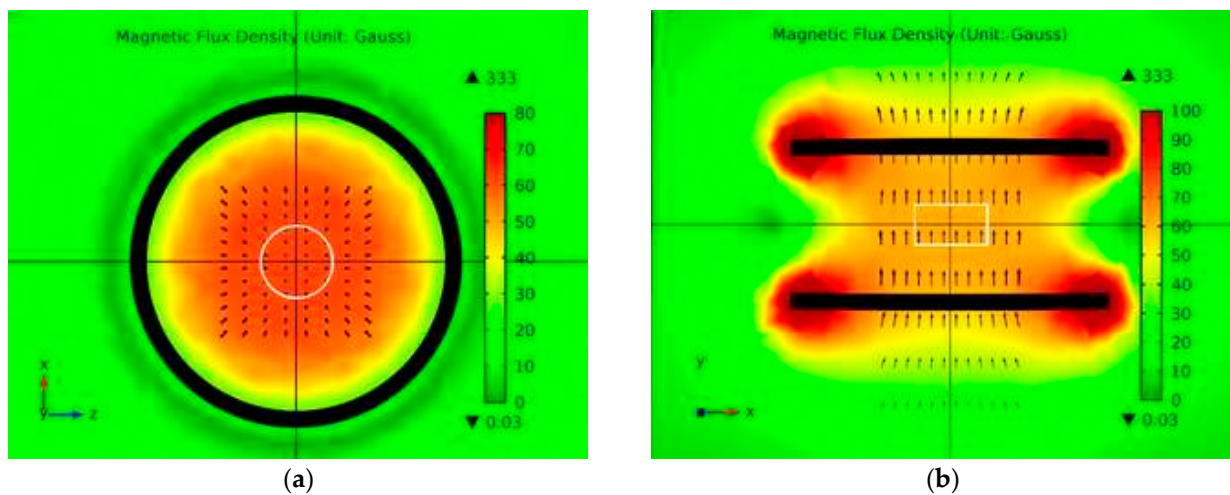


**Figure 1.** (a) Magnetic field configuration magnet array; (b) Simulation Analysis of a Halbach Array Model [16].

This arrangement provides benefits for applications such as the Emrax motors. This motor effectively directs flux inwards towards the axial arrangement of the rotor and stator through two exterior plates of Halbach array magnets. The steel housing of the motor is a crucial factor for future applications. The motor is constructed with discrete segments of steel lamination and winding, all fastened on an aluminium hub. One disadvantage of this configuration is that the magnetic elements are arranged in a direct or quasi-direct repelling position. This suggests that neighbouring magnets in the same array are demagnetizing each other, which might cause fluctuations in the magnetic field density along the surface.

*2.2. The Helmholtz Coil Configuration*

A Helmholtz coil, as described by Abbott [17] and shown in Figure 2, is a parallel pair of comparable circular coils positioned one radius apart and coiled in series, ensuring current flows in the same direction through each coil.



**Figure 2.** Magnetic field simulation of the Helmholtz coil comprising two 200 mm, 500500-turnelectric coils in air [18]: (a) Top view; (b) Side view.

Developed by Hermann von Helmholtz [19], these types of coils generate a homogeneous magnetic field at their core, making them valuable for studies requiring a regulated magnetic field, magnetic sensor calibration, and nullification of the Earth’s magnetic field. The strength of the magnetic field is directly influenced by the number of turns and current flowing through the coils, calculated using the equation for field strength based on desired size, radius/coil separation, and magnetic field strength. The Helmholtz coil system produces a uniform magnetic field parallel to the coils’ axes, allowing adjustment of the

applied current to generate a controlled, uniform magnetic field. Commercially available Helmholtz coils serve various purposes, and their construction is vital for investigating magnetic field sensing in fluxgate sensors [20]. In [20], a methodical optimization strategy is employed to maximize the magnetic field produced by the coils, utilizing a modified multi-objective and systematic [17] optimization technique effective for addressing electromagnetic design challenges with multiple variables and non-linear constraints [21]. In the pursuit of a stable magnetic field from a motor source, research efforts were directed towards modelling a magnetic source field that remains both constant and perpendicular to the brake. This specialized source was crafted to assess the impact of varying magnetic flux densities on the brake. Helmholtz coils, comprising a pair of identical thin coils positioned apart to optimize the uniformity of the magnetic field in the central volume, were employed for this purpose [22]. While alternatives like square, rectangular, or polygonal coils exist, the common configuration entails two circular coils separated by a distance equal to the radius. Helmholtz coils, as illustrated in Figure 2 displaying a magnetic field simulation, are renowned for creating known magnetic fields. Importantly, their versatility extends to sensing magnetic fields, capitalizing on the inverse relationship between a changing magnetic field and the voltage at the coil’s terminals [23]. The specific objective is to ascertain the magnetic field along the axis of symmetry. Achieving this, a Helmholtz coil has been positioned with defined radius, turns, and distance within a coordinate system, ensuring the coordinate origin aligns with the coil’s midpoint [24]. This approach enhances precision in evaluating the magnetic field’s impact on the brake under diverse conditions.

Taking the Biot–Savart law for a wire:

$$B(r) = \frac{\mu_0 I}{4\pi} \int_S \frac{r - R}{|r - R|^3} ds \tag{1}$$

where:  $B$  = magnetic flux density vector [T],  $\mu_0$  = relative permeability [H/m],  $I$  = current [A],  $r - R$  = coil radius difference [mm], and  $S$  = integration path.

Since there are two coils involved, the Biot–Savart law is split into two halves, each of which represents the magnetic field produced by the corresponding coil. Using the superposition principle, it is possible to add the two contributions together to obtain the total magnetic field 1.

$$B_1(r) = \frac{\mu_0 I}{4\pi} \int_{S_1} \frac{r - R}{|r - R|^3} ds \tag{2}$$

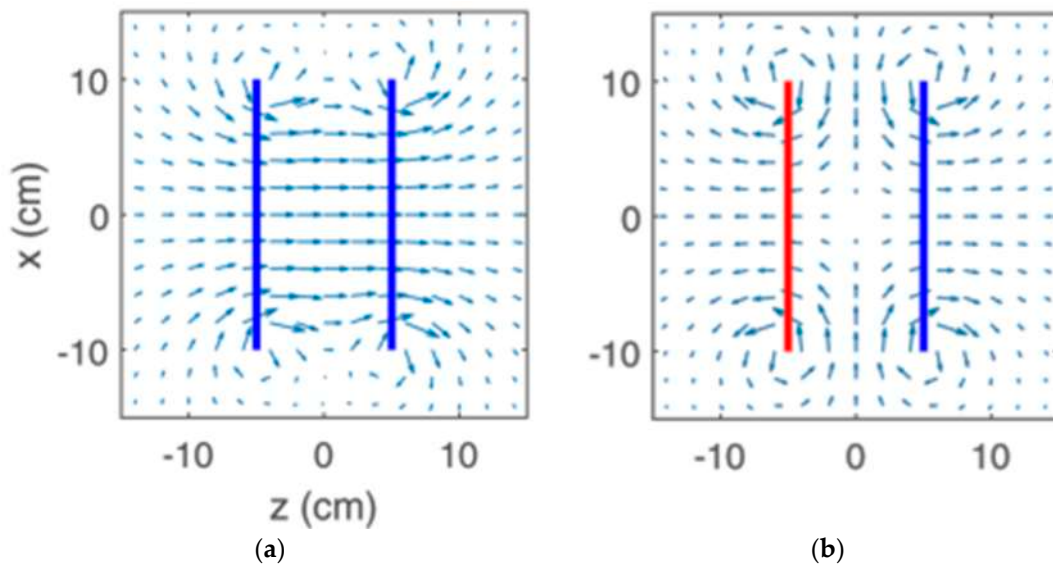
$$B_2(r) = \frac{\mu_0 I}{4\pi} \int_{S_2} \frac{r - R}{|r - R|^3} ds \tag{3}$$

After calculating, integrating by parts,  $S_1$  is the integration path around the first coil and  $S_2$  is the integration path around the second coil. The total path is:

$$S_1 + S_2 = S \tag{4}$$

The generation of a uniform magnetic field between coils depends on the direction of current flow. To ensure a linear magnetic field, both coils are connected so that the current flows in the same direction.

From Figure 3, it is possible to demonstrate these two configurations of magnetic field distribution around the two coils (represented by the arrows). In Figure 3a, the currents in the coils have the same direction and in the second they have two different directions. The flow needs to be as constant as possible throughout the whole Helmholtz coil setting. Therefore, the first configuration, shown in Figure 3a, is chosen for its alignment with this requirement, optimizing the desired magnetic field profile between the coils.



**Figure 3.** Coil configuration and simulation in two different directions [25]: (a) Same direction; (b) Opposite direction.

It is possible to compute the magnetic field of a Helmholtz coil along the axis of symmetry in 2 different settings:

- a. Same current direction.
- b. Opposite direction of current.

In Case (a), the final equation is:

$$B(r) = -\frac{\mu_0 I R^2 N}{2} \left[ \left( \left( z - \frac{d}{2} \right)^2 + R^2 \right)^{-\frac{3}{2}} - \left( \left( z + \frac{d}{2} \right)^2 + R^2 \right)^{-\frac{3}{2}} \right] \hat{z} \quad (5)$$

After simplifications, it is possible to obtain:

$$B(r) = \left( \frac{4}{5} \right)^{\frac{3}{2}} \mu_0 \frac{NI}{R} \quad (6)$$

To have a higher-flux field simulation, a constant  $k$  was added:

$$B(r) = \left( \frac{4}{5} \right)^{\frac{3}{2}} \mu_0 k \frac{NI}{R} \quad (7)$$

With:  $I$  = current [A],  $N$  = number of turns,  $R$  = coil radius,  $k$  = Helmholtz coil constant,  $\mu_0$  = relative permeability [ $4\pi \times 10^{-7} \frac{N}{A^2}$ ].

In summary, as has also been shown by [22,26], only defining a specific geometry for the motor allows implementation of the kind of arrangement of a Halbach array style. The Helmholtz coil arrangement was determined to be the optimum choice for mimicking the motor’s magnetic field in various setup configurations due to the array’s smaller and shorter magnetic field.

### 2.3. The Helmholtz Coil Geometry

To align the Helmholtz coil geometry with the desired magnetic field output of the chosen motor in the simulations, certain values are set, deviating from natural configurations. Simulating a 1 tesla flux field, for instance, would require an impractically substantial number of coil turns or an exceptionally high current. This anomaly for this kind of application can impact on the desired magnetic field uniformity. To address this, Equation (7)

introduces a constant denoted as ‘k’, facilitating the creation of a variable magnetic field in the Helmholtz coil solely for simulation purposes. Those values cannot be considered as real variables; however, they are useful to represent the real behaviour of a motor emitting such peaks for magnetic field. This constant assumes substantial values, ranging from 1 to  $10^8$ , so  $k = 1 \sim 10^8$ , allowing flexibility in adjusting magnetic flux diversity in calculations and simulations while keeping other parameters at a more natural level. The corresponding data for this modified geometry can be found in Table 1, coming from multiple previous analyses [22,23].

**Table 1.** Geometry of Helmholtz coil data.

Character	Name	Values		
$R$	Coil radius [m]		0.40	
$d/2$	Half distance from the centre [m]	0.01	0.09	0.20
$d$	Distance from the centre [m]	0.02	0.18	0.40
$A$	Rectangular coil section area [m <sup>2</sup> ]		$5 \times 10^{-4}$	
$N$	Number of turns per coil		100	
$\rho$	Resistivity [Wm]		$1.7 \times 10^{-8}$	
$FF$	Fill factor [ $0 < Sf < 1$ ]		0.71	
$V$	Volume of the coil [m <sup>3</sup> ]		$4.46 \times 10^{-5}$	
$R_{eq}$	Equivalent resistance [W]		24.07	
$k$	Helmholtz coil constant		$1 \sim 10^8$	

Having established the data parameters, the focus shifted to determining an optimal geometric configuration representative of the magnetic flux emitted by a motor. The coils, exhibiting a square section with dimensions of 5 mm in length and 5 mm in width, adhere to a resistivity consistent with the average for steel, as outlined in Table 1. The fill factor indicates the ratio between the actual and maximum obtainable power output average for the given material, and it was considered in the design. The equivalent resistance is contingent upon the arrangement of total resistance, whether in parallel or series. Consequently, the motor’s geometry mirrors that of a simplified motor top, a disc with the same radius of the brake, with a thickness of 8 mm, positioned 6 mm from the brake rotor. To ensure symmetry, boundary conditions were defined aiming to capture the essence of the motor’s magnetic flux characteristics within a well-defined and representative geometrical layout.

### 3. Model Description

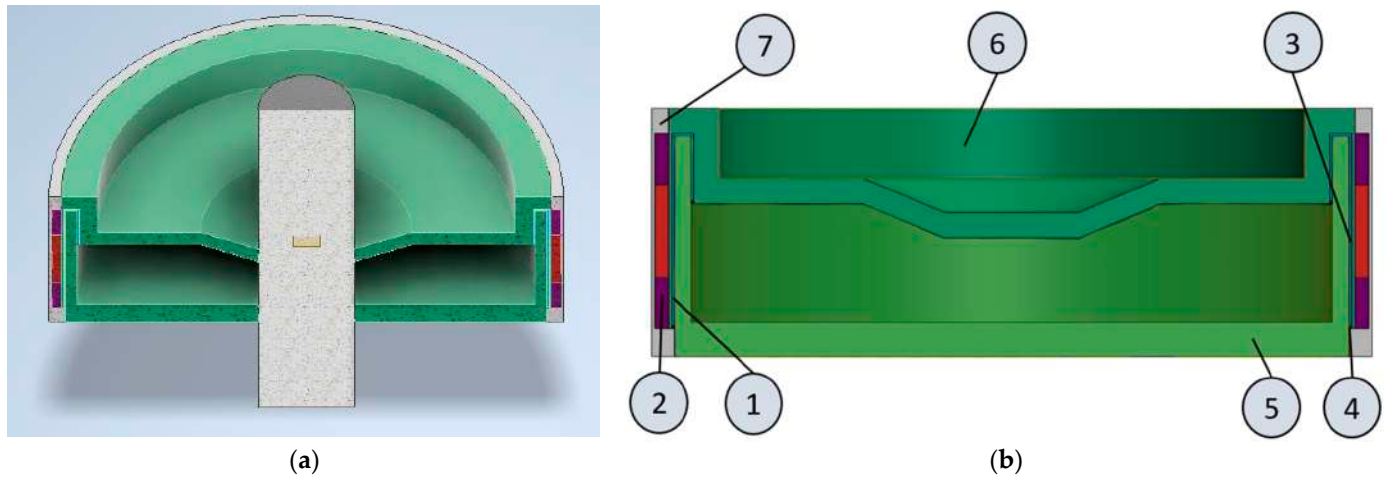
#### 3.1. The Brake

Autodesk Inventor was employed for geometric modelling and Altair Flux for the simulations. Following the resolution of issues related to the motor source field, attention now turns to the brake and its geometry. Simulations [27] explore the influence of the flux field on the brake components, specifically the magnetorheological fluid [28], and the rotor, which exhibit different magnetic field orientations—axial and radial coil configurations. These orientations, evaluated in prior studies [8], impact torque correlations. The strategies employed involve identifying electrical parameters that meet output specifications and appropriately configuring mechanical properties [28].

##### 3.1.1. Braking System Layout

The proposed brake shown in Figure 4 features a revolving disc covered by a static casing, injecting MR fluid into the space between the disc (5) and casing (6–7) as described by [6,7]. The coils (2), wrapping around each bobbin (3), create magnetic fields, causing the MR fluid in the gap (1) to solidify and produce necessary braking torque through shear friction. In fact, magnetorheological fluids are smart fluids, capable of changing their yield behaviour as a function of the magnetic field applied. Their yield stress is a function of the magnetic field. Magnetorheological (MR) fluid brake systems offer distinct advantages over

conventional counterparts, characterized by faster response times, enhanced durability, reliability, and the ability to dynamically adjust braking force in real time. Despite these benefits, the design and maintenance of MR fluid brake systems can be more intricate compared to traditional brake systems.



**Figure 4.** Brake geometry: (a) Brake section; (b) Brake parts: 1. MR Fluid Selection (blue), 2. Coils (purple), 3. Bobbins (red), 4. Lip Seals (black), 5. Rotor (light green), 6. Stator (dark green), 7. Cover (grey).

To facilitate experimentation with desired values, particularly in the context of a motor coil with a length of 400 mm, the imposition of a magnetic field aligns with the specific parameters essential for exploration and testing within this innovative braking system.

### 3.1.2. The Fluid Selection

MR fluid is often modelled as a Bingham solid that has yield strength [29]. For this model, the Bingham’s equation (Equation (8)) governs the MR fluid’s flow [30].

$$\tau = \tau_y(H) + \eta\dot{\gamma} \tag{8}$$

With:  $\tau$  = fluid shear stress,  $\tau_y$  = the field-dependent yield stress,  $\dot{\gamma}$  = the fluid shear rate, and  $\eta$  = the plastic viscosity. The most significant off-state characteristic of MRFs is the field-independent viscosity ( $\eta$ ). The related viscosity of the carrier fluid and the particle volume fraction have the most effects on the MR fluid viscosity.

Table 2 displays the physical properties of the chosen MR fluid.

**Table 2.** MRF properties [31,32].

	MRF-132-DG
Initial viscosity [Pa s] (at 25 °C)	0.2–0.5
Density [g/cm <sup>3</sup> ]	2.95–3.15
Magnetic field strength [kA/m]	150–250
Yield point [kPa]	50–100
Reaction time [ms]	15–25
Operating temperature [°C]	–40 to +130
Typical supply voltage [V]	2–25
Typical current intensity [A]	1–2

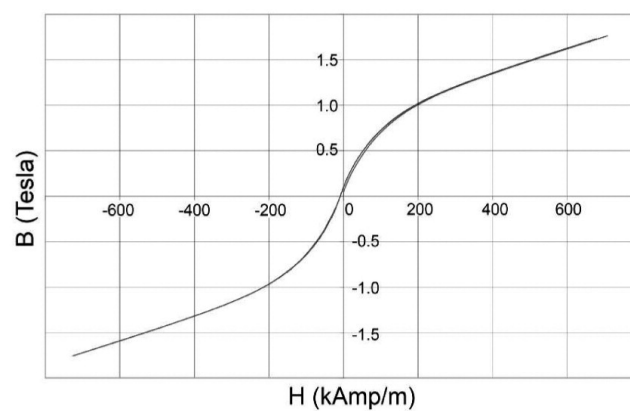
MR fluid exhibits distinctive non-Newtonian properties, with viscosity increasing as the particle volume percentage rises. The fluid, containing magnetic particles ranging from 1  $\mu\text{m}$  to 10  $\mu\text{m}$ , displays sedimentation tendencies that escalate with larger particle sizes. When diving into its magnetic properties through the hysteresis loop, the non-linear



relationship between induced magnetization ( $M$ ) and applied magnetic field ( $H$ ) becomes evident, highlighting the fluid's unique response to varying magnetic forces. These non-Newtonian characteristics make MR fluid [33] particularly intriguing for applications where dynamic viscosity alterations can be harnessed for enhanced control and adaptability [34].

### 3.1.3. Material Selection

According to their permeability values, materials used to design the brake fall into three categories—ferromagnetic, paramagnetic, and diamagnetic. Ferromagnetic materials, like iron and nickel, strongly attract magnetic fields (permeabilities  $> 1$ ), while paramagnetic materials, including iron salts and rare earth elements, exhibit mild attraction ( $1 < \text{permeabilities} < 1.001$ ). Ferromagnetic materials feature demagnetizing fields, inducing dimensional changes known as magnetostriction. It is important to underline the representation of the MR fluid in the software, performed by inserting its magnetization curve reported in Figure 5.



**Figure 5.** B-H curve for MRF [31].

Magnetic anisotropy, affected by production techniques, causes variations in magnetic characteristics based on measurement direction. Due to hysteresis, saturation, and non-linearity, accurate measurement of ferromagnetic materials requires costly and sensitive equipment. Material selection is crucial in magnetorheological brake (MRB) design, impacting structural, thermal, and magnetic circuits. The chosen materials can be found in Table 3 detailing their magnetic, structural, and thermal properties. For implementing it, after the definition of the application, it is important to take from the model database. The coils in the brake system are made of copper, consisting of four sets fixed axially, each with approximately 1100 turns. Given the utilization of magnetorheological (MR) fluid, crucial steps are needed to prevent leakage that could compromise braking efficiency. Sealing becomes a critical concern due to the presence of iron particles in MR fluids, posing a potential risk of braking loss. The seals, composed of steel and rubber, take the form of two lip rings strategically positioned at the ends of the MR fluid to ensure effective sealing. The primary components—the rotor, stator, and cover—are made of steel. Specifically, the rotor, located closest to the motor at the range of 6–8 mm, warrants careful consideration. The chosen distance allows for a subsequent assessment of the magnetic flux emanating from the motor, potentially necessitating the implementation of an electromagnetic absorber to counteract its influence on the brake system.

**Table 3.** Material properties.

Magnetic Properties	Aluminium	Copper	Steel	MRF-132-DG
Initial relative permeability	1	1	2500	3.798
Saturation magnetization [T]	-	-	2.5	2.1
Knee adjusting coefficient	-	-	0.5	0.4
Thermal conductivity [ $Wm^{-1}K^{-1}$ ]	0.52	0.92	-	-
Saturation flux density [T]	-	-	1.55	1.65

### 3.2. Simulation Methodology

CAD software Inventor 2023 was used to build the geometrical model and then it was imported into the finite element analysis (FEA) software Altair Flux 2022. Due to the deliberate selection of a Helmholtz coil for its capacity to accurately represent the comprehensive behaviour of the motor and brake system, it was decided to simulate the entire combination. It is important to remember, to reduce the computation time, that the simulations are conducted on a quarter or a half of the investigated geometry, taking advantage of the symmetry tools of the software.

Once the geometry is imported, an infinite box was imposed as a domain following the guidelines of generating an infinite box with double the dimensions of the entity of the simulation.

Before defining the physics of the system, the domain was meshed, and the physical application was defined as magnetostatic. The reason is that, although there are rotating parts in the real model, the magnetic field is active on the static parts and the differences between the motion of the ferromagnetic parts and their static behaviour are negligible.

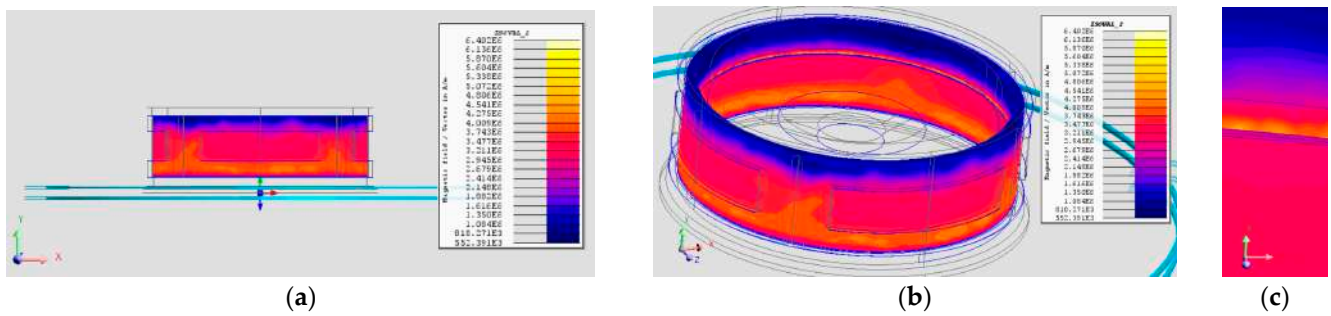
### 3.3. Simulation of Each Configuration

The following subsection specifies the restrictions and goal of the design optimization. Different Helmholtz coil layouts are used for checking the most realistic behaviour for the magnetic field direction and intensity out of the electric motor, considering the limitations previously described by the regulations [11]. To this end, different positions of the coils are defined, each having different magnetic flux behaviours around the area of interest and evaluating the one that best represents an electric motor’s behaviour. The goal is to represent in the most realistic way the electric motor’s magnetic effect on the surrounding area.

#### 3.3.1. Configuration 1

In this motor design, as shown in Figure 6, the plate’s proximity to the brake and the intentional non-uniform magnetic field contribute to computational insights. The setup envisions a denser field around the brake’s lower portion and a thinner field above, achieved by placing coils extremely close, spaced 20 mm apart. Parameters were kept constant, and the high value of  $k$  ( $k = 10^4$ ) emphasizes the irregular intensity of the field. A visual representation indicates a strong average magnetic field ( $4 \times 10^6 A/m$ ) with uneven density. The disproportionate magnetic field density is evident due to the Helmholtz coil rings representing the motor being close, resulting in an unusually high field at the brake’s bottom and almost zero field at the top.

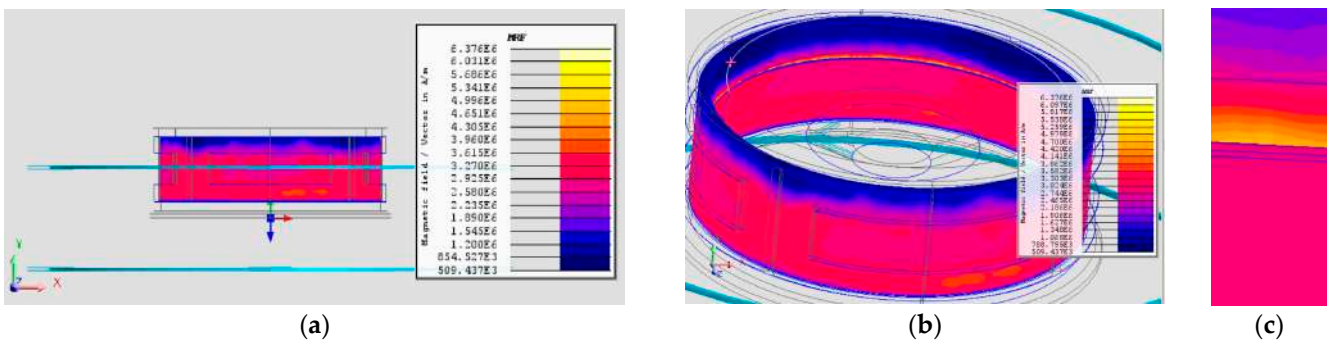
A close-up view of the MRF near the lip seals reveals potential influences from the magnetic conductivity of the seal material in response to the high field intensity.



**Figure 6.** Configuration simulation at  $k = 10^5$ : (a) Coil configuration side view; (b) Influence of coil configuration on the brake; (c) Close-up lip view.

### 3.3.2. Configuration 2

In configuring a coil with a 400 mm diameter, the optimal distance from the centre is set at 90 mm, with 180 mm between the coils. This arrangement shows details of a stronger magnetic field towards the centre of the brake. As shown in Figure 7, there is a greater flux field in the middle and a weaker one at the top and bottom. The Helmholtz coil rings representing the motor, shown in light blue, are 180 mm apart and the value of  $k$  is  $10^5$ .



**Figure 7.** Configuration 2 simulation at  $k = 10^5$ : (a) Coil configuration side view; (b) Influence of coil configuration on the brake; (c) Close-up lip view.

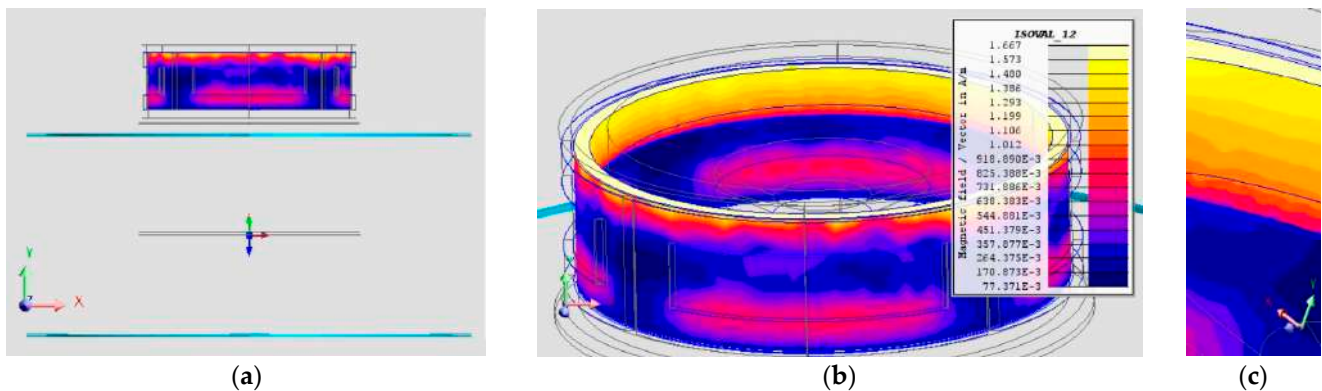
Although a constant field along the brake is not obtained, the change in density is slighter compared to configuration 1. Surprisingly, the magnetic field density, although more evenly distributed, remains disproportionately absorbed by the fluid. The average magnetic field persists at about  $4 \times 10^5$ , akin to the previous scenario.

### 3.3.3. Configuration 3

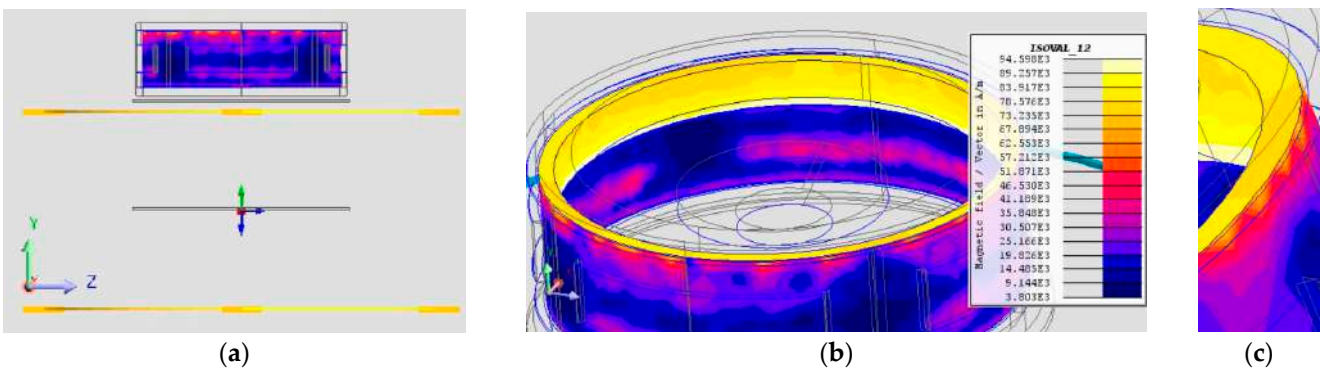
In this configuration, spacing of coils with a 400 mm diameter, positioned 200 mm apart, is employed to generate the desired magnetic field from the motor. Positioned outside the coil’s magnetic flux production, the brake anticipates a greater magnetic flux field at the rotor’s bottom and a weaker one at the brake’s top. With Helmholtz coil rings placed 200 mm from the centre, as it is possible to see in Figure 8, maintaining other settings constant, that this arrangement results in a constant, linear magnetic field with uniform density, typical for regular brake functioning ( $k = 1$ ). The purple colour suggests an influence from the rotor’s magnetic field. Additionally, near the lip seals, high values indicate material impact, emphasizing the importance of sealing. Exploring the extreme scenario ( $k = 10^5$ ), where the magnetic flux density is notably high, the simulations remain comparable, emphasizing consistent fluid behavior.

Configuration 3 concentrates maximum magnetic intensity at the top, emphasizing the significance of spatial positioning for optimal performance (Figure 9). Clearing the magnetic circuit of dynamic seals is crucial to prevent sealing failure during braking,

emphasizing the importance of surface coatings and sealing procedures to mitigate fluid contamination [35].



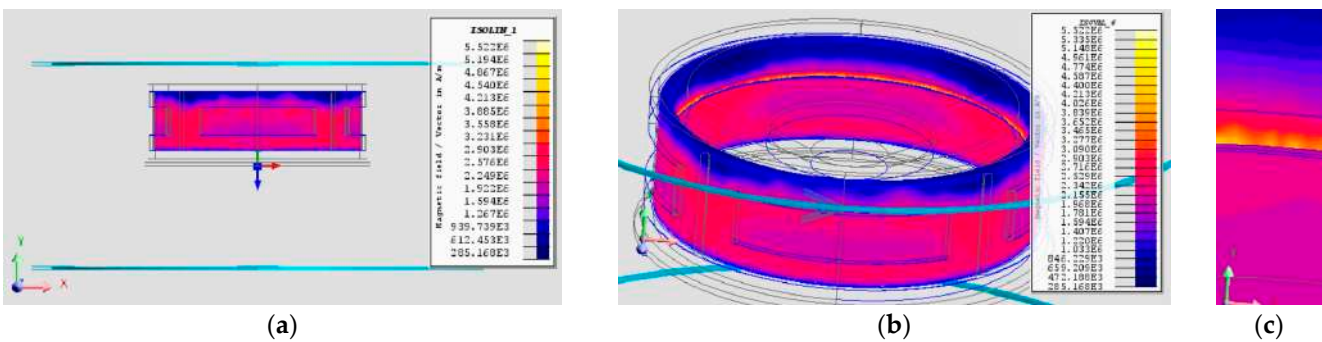
**Figure 8.** Configuration 3 simulation at  $k = 1$ : (a) Coil configuration side view; (b) Influence of coil configuration on the brake; (c) Close-up lip view.



**Figure 9.** Configuration 3 simulation at  $k = 10^5$ : (a) Coil configuration side view; (b) Influence of coil configuration on the brake; (c) Close-up lip view.

### 3.3.4. Configuration 4

In the last configuration, shown in Figure 10, the brake is fully immersed in the motor’s magnetic field, providing a unique analysis of its behaviour within the field. Submerging the brake leads to a homogenous (constant) magnetic field inside the coil when the distance equals the coil’s radius ( $d = R$ ). This configuration aims to achieve a consistent flow across the entire brake and its components.



**Figure 10.** Configuration 4 simulation at  $k = 10^5$ : (a) Coil configuration side view; (b) Influence of coil configuration on the brake; (c) Close-up lip view.

Despite the field’s uniformity, the values are higher at the bottom of the brake compared to most of its surface, echoing findings from similar cases [22]. Like previous

configurations, the magnetic field exhibits greater intensity at the bottom of the fluid and lower values on the top, creating a more blended distribution throughout. Once again, the region near the lip seals records the highest intensity, demonstrating the distinctive behaviour of the MRF in proximity to these components.

### 3.4. Brake Analysis Layout

Materials made of magnetic steel are used as the central parts of brakes, inductors, transformers, and motors. Since they lack ‘intrinsic’ magnetism, they will remain in an environment devoid of magnetic forces. The  $B$ - $H$  curve is frequently used to characterize the permeability of such materials when discussing their magnetic properties. Permeability is defined as:

$$\mu = \frac{B}{H} \quad (9)$$

where:  $B$  and  $H$  represent the magnetic flux density in Tesla (T) and the magnetic field intensity in amperes per meter (A/m), respectively. Examining the magnetic circuit in the magnetorheological brake, Ampere’s law is applied to calculate the correlation between magnetic field strength  $H$  and the applied current in the active zone gap of the MR fluid.

$$\sum H_0 I_0 = N_{coils} i \quad (10)$$

where:  $H_0$  and  $I_0$  represent the circuit’s link’s magnetic field strength and effective length, respectively.  $i$  is the applied current, while  $N_c$  is the coil’s number of turns. Equation (11) shows the magnetization parameter  $J$  correlated to the magnetic field strength  $H$  and relative magnetic permeability  $\mu_0$ :

$$J = B - \mu_0 H \quad (11)$$

It is then possible to calculate the magnetic field of a Helmholtz coil along the axis of symmetry.

$$\Phi = B_0 A_0 \quad (12)$$

where:  $\Phi$  is the magnetic flux,  $A_0$  is the cross-sectional area, and  $B_0$  is the magnetic flux density, described by:

$$B_0 = \mu_{sp} \mu_0 A_0 \quad (13)$$

where:  $\mu_{sp} = 4\pi \times 10^{-7} \text{h/m}$  is the constant magnetic permeability of free space and  $\mu_0$  is the relative permeability.

The magnetic brake parts are made of the same steel type:

$$N_c i = IH_{motor} + IH_{mrf} \quad (14)$$

$H_{motor}$  and  $H_{mrf}$  are the magnetic field in the steel and MR fluid links, respectively. Using the relations in Equations (12) and (13), it is possible to write:

$$H_{motor} = \frac{\Phi}{\mu_{sp} \mu_{motor} A_{motor}} = \frac{B_{mrf} A_{mrf}}{\mu_{sp} \mu_{motor} A_{motor}} \quad (15)$$

Substituting Equations (13) and (14) in Equation (15), it is possible to write:

$$H_{motor} = \frac{B_{mrf} A_{mrf}}{\mu_{sp} \mu_{motor} A_{motor}} \quad (16)$$

or

$$H_{motor} = \left( \frac{B_{mrf} A_{mrf}}{\mu_{motor} A_{motor}} \right) H_{mrf} \quad (17)$$

Now, transforming Equation (9):

$$B_{mrf} = \mu_0 \mu_{mrf} H_{mrf} \tag{18}$$

where:  $\mu_{motor}$  and  $\mu_{mrf}$  are the relative permeabilities of the motor, which is in the material of steel, and MR fluid, respectively, and  $A_{motor}$  and  $A_{mrf}$  are the effective cross-sectional areas of the corresponding relative steel material and MR fluid links.

The relative permeability of the magnetic fluid, MRF-132-DG, and the metallic component can vary with the magnetic field strength, with steel having a relative permeability around 2500, while that of MR fluids typically ranges around 2.5. Despite being treated as constants for ease of calculation, the model yields reasonably accurate outcomes. Table 4 presents essential characteristics of MRF-132-DG and the motor. The average magnetic field along the shear gap region, derived from six points of consideration, ranges from  $3.9 \times 10^5$  A/m for the lowest k to 0.2260 for the highest in the third configuration, resulting in an overall average of 0.1932 A/m.

**Table 4.** Average values needed for the calculation.

	MRF-132-DG	Motor (Steel)
Permeability $\mu$ [h/m]	3.798	2500
Cross sectional area $A$ [m <sup>2</sup> ]	0.00042	0.0012
Average magnetic flux density $B$ [T]	-	0.1932
Average magnetic field $H$ [A/m]	$0.2 \times 10^5$	-

#### 4. Analysis of the Results

Utilizing the data obtained from simulations, a numerical comparison is performed to assess the four configurations shown in Figure 11, which are represented in yellow, and the brake is presented in shades of blue. The subsequent presentation displays the reference configurations and their corresponding equations, enabling a detailed examination of solutions through numerical methods. Tables 5 and 6 depict magnetic field averages for the magnetorheological fluid and motor flux density across all constants for each configuration. It is crucial to acknowledge that variations in magnetic field density can influence values in configurations 1, 2, and 4.

**Table 5.** Magnetic field of the MRF for each configuration [A/m].

k	Magnetic Field of the MRF [A/m]			
	Configuration 1	Configuration 2	Configuration 3	Configuration 4
$1 \times 10^0$	$9.10 \times 10^{-5}$	$7.95 \times 10^{-5}$	$2.86 \times 10^{-6}$	0.03
$2 \times 10^3$	2.14	2.02	0.01	$0.72 \times 10^3$
$4 \times 10^3$	3.32	3.17	0.04	$1.39 \times 10^3$
$6 \times 10^3$	4.29	4.08	0.09	$1.97 \times 10^3$
$8 \times 10^3$	5.17	4.89	0.15	$2.43 \times 10^3$
$10 \times 10^3$	6.01	5.69	0.23	$2.76 \times 10^3$

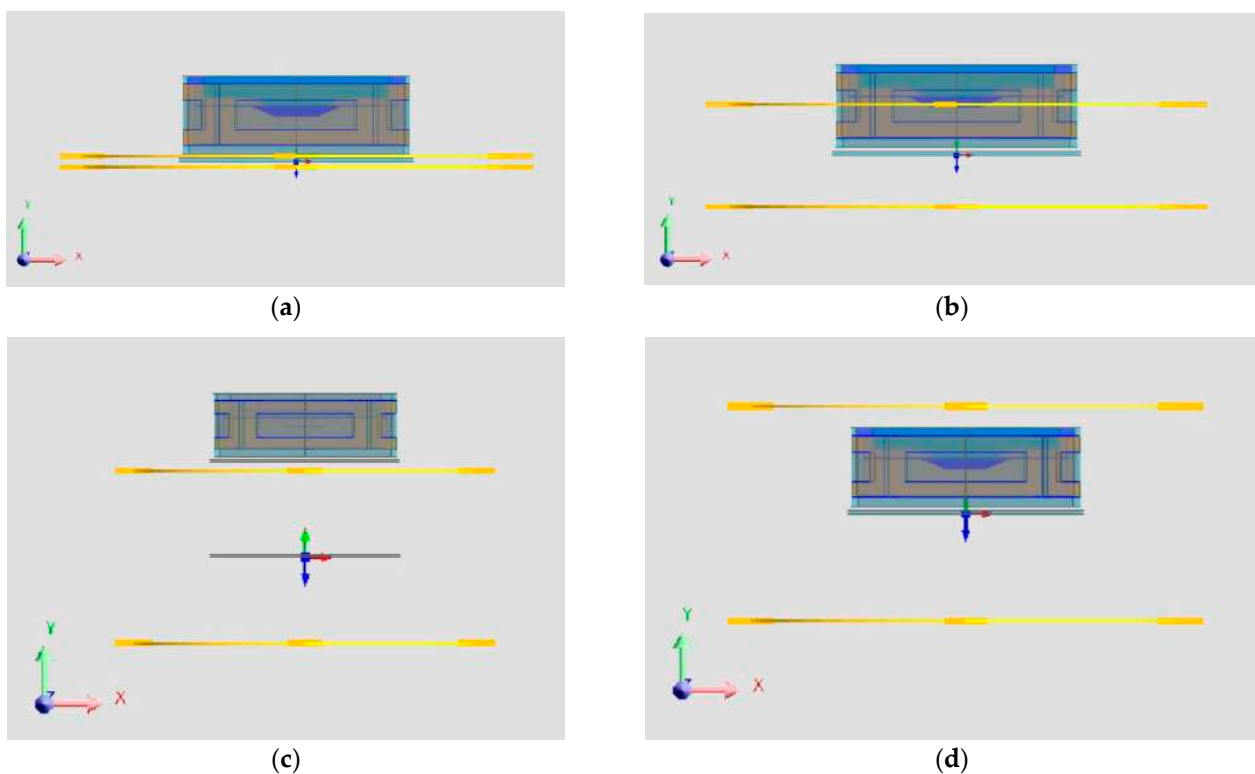
However, in the third case the Helmholtz coils are positioned in a way to ensure more accurate results. This configuration represents the most natural behaviour of the flux coming out from the surface of a motor, or a source field, also considering the Helmholtz coil configuration.

The Helmholtz coil presented in this configuration is designed in a way that can maximize the magnetic field produced by the coils. In this solution, the field is distributed uniformly and at a high magnetic field strength. The averages as seen in Tables 5 and 6, derived from Altair Flux simulations, are yet to be configured by magnetization equations.

In Figure 12a, it is possible to see that the curve of the fourth configuration is a short yellow line. This indicates that the average values of this type of placement are minor compared to Figure 12b.

**Table 6.** Magnetic flux density of the motor for each configuration [T].

Magnetic Flux density of the Motor [T]				
k	Configuration 1	Configuration 2	Configuration 3	Configuration 4
$1 \times 10^0$	$6.19 \times 10^{-4}$	$5.01 \times 10^{-4}$	$3.89 \times 10^{-5}$	$5.65 \times 10^{-5}$
$2 \times 10^3$	1.37	1.12	0.08	1.65
$4 \times 10^3$	2.41	2.06	0.16	2.72
$6 \times 10^3$	4.29	2.70	0.23	3.50
$8 \times 10^3$	3.02	3.14	0.31	4.18
$10 \times 10^3$	3.61	3.63	0.39	4.83



**Figure 11.** The four configurations of the Helmholtz coil: (a) Configuration 1; (b) Configuration 2; (c) Configuration 3; (d) Configuration 4.

The values shown in Tables 5 and 6 are the average magnetic fields and flux density, respectively, computed in the MRF surface. The configurations have similar behaviour with respect to each other. Figure 12b shows a closer representation of the values of each k for configuration 3, which is the configuration of interest. To obtain the non-linear characteristic B-H curves, the raw results from Tables 5 and 6 are applied to Equations (17) and (18). Through these calculations we obtain the graphs shown in Figure 13, where it is possible to see the B-H curves with the values of each configuration. The graphs for configurations 1 and 2 have a very similar tendency. In these two cases, the only difference lies in the distance between the Helmholtz coils; in particular, in the first configuration the coils are 40 mm apart while in the second they are 180 mm apart.

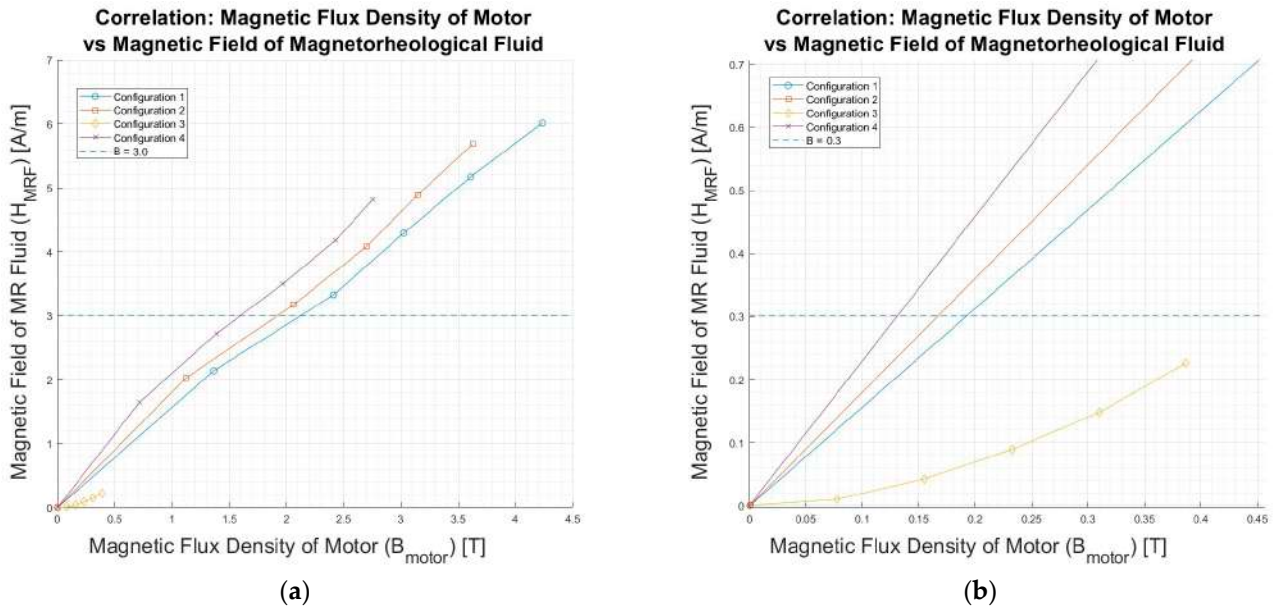


Figure 12. Magnetic Flux Density of the motor averages vs. Magnetic Field of the Motor: (a) B-H curves of all configurations; (b) Zoomed-in B-H curves of all configurations.

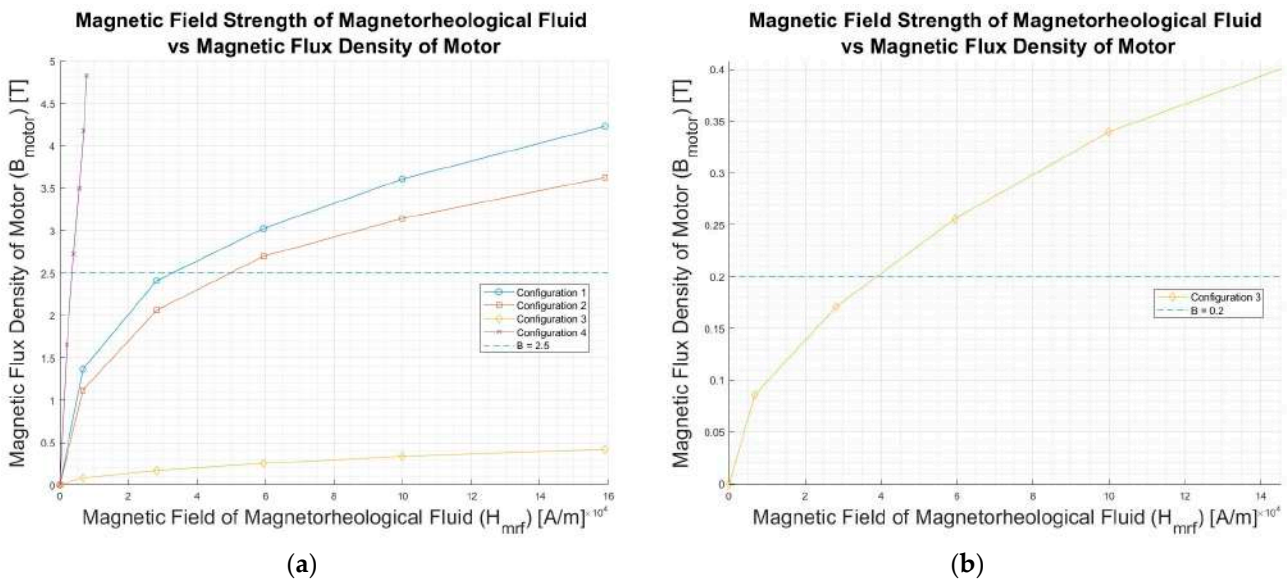


Figure 13. Magnetic Flux Density of the motor averages vs. Magnetic Field of the MRF: (a) B-H curves of all configurations; (b) B-H curves of Configuration 3.

The graphs in Figure 13 are inverted to examine any potential similarities between the magnetic field and the typical B-H magnetization curves of materials, as shown in Figure 5. In Figure 13a, we can note that configuration 4 has an unusually linear-looking graph because of completely immersing the brake in the field, causing the magnetic flux density on the MRB to be unusually high. On the other hand, the graph for configuration 3 shows lower values of the motor’s magnetic flux density. Figure 13b takes a closer look at this graph, showing how this configuration causes typical B-H curve magnetization characteristics. One can notice how the flux density rises in direct proportion to the field strength until it settles around a constant value even as field strength increases. This is because as the magnetic domains in the iron align, it constrains the flux density that the core can produce.

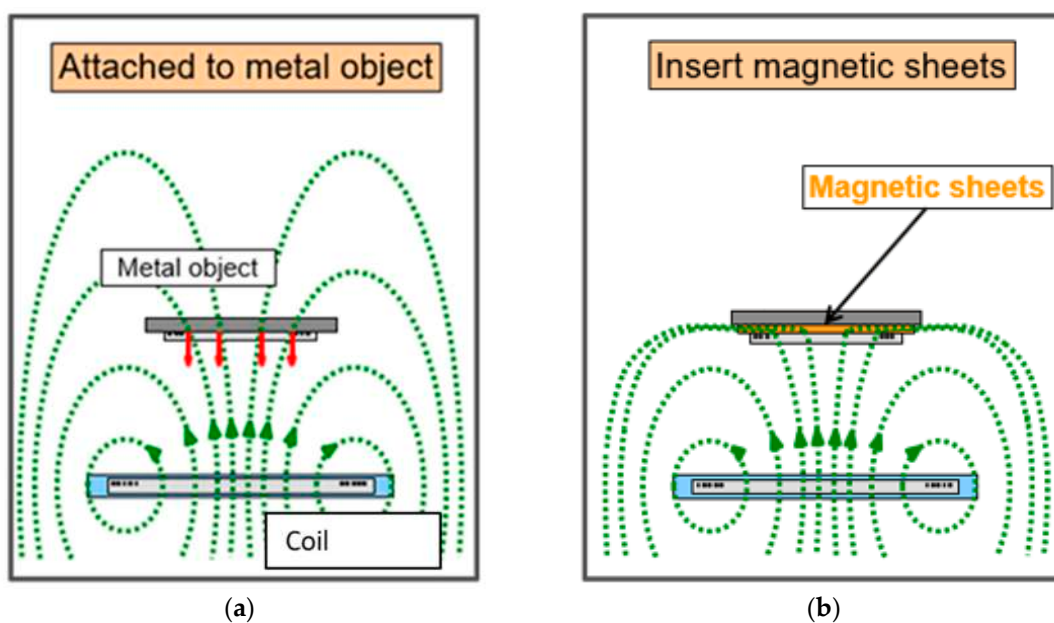


The point on the graph when the flux density reaches its maximum is the magnetic saturation, sometimes referred to as core saturation. As the small molecular magnets inside the material become 'lined up', saturation takes place because of the haphazardly random arrangement of the molecule structure within the core material changing. Any increase in the magnetic field strength caused by an increase in the electrical current flowing through the coil will have little or no impact because these molecular magnets become increasingly aligned as the magnetic field strength ( $H$ ) increases until they reach perfect alignment and produce the maximum flux density.

## 5. The Absorber Solution

### 5.1. Analysis of the Results

This section delves into the foundational theories of transmission line theory and Maxwell's equations to provide a comprehensive understanding of electromagnetic (EM) wave absorbers, as seen in Figure 14. The use of transmission line problems with analogous plane-wave behaviour simplifies the comprehension of plane-EM-wave problems without directly solving Maxwell's equations.



**Figure 14.** Magnetic field influence on a metal object and on a magnetic sheet [36]: (a) metal object without the absorber; (b) metal object after the insertion of the absorber.

Materials that absorb electromagnetic fields play a crucial role in mitigating the effects of electromagnetic radiation across various frequencies. Ferrite materials, including sheets and beads, prove effective in absorbing magnetic fields, particularly in the lower frequency range. Metal-based materials such as conductive foams and metamaterials exhibit excellent absorption capabilities for specific frequencies. Polymer-based materials like polyurethane foam and polystyrene foam are preferred in construction due to their flexibility and low weight.

Specialized materials, such as soft magnetic composites, contribute to radar signal absorption and reduction of magnetic field emissions [37]. Researchers have explored microwave absorption in hexaferrite–polymer composites, revealing enhanced absorption capabilities with increased ferrite concentrations in the polymer matrix within the frequency range of 0.2 to 12.4 GHz [38]. These diverse materials empower scientists and engineers to devise efficient solutions to challenges posed by electromagnetic fields across various applications.

5.2. The Materials

Configuration 3, equipped with a 6 mm steel absorber plate, exhibits slightly higher motor magnetic flux density compared to the normal configuration, attributed to the absorber’s proximity to the motor flux outlet. Notably, the magnetic field in the fluid decreases, indicating effective separation of the motor’s influence on the magnetorheological fluid’s magnetic field. The choice of absorber material, its thickness, composition, and distance contribute to these outcomes. The selected insulator, 5780-C5B from Holland Shielding Systems BV [39], composed of a magnetic powder and rubber composite, demonstrates efficient electromagnetic wave absorption and suppression capabilities.

Detailed material analyses, as presented in Table 7, reveal that the 5780-C5B absorber material outperforms steel and aluminium, reducing magnetic field density in the fluid. The comparative performance graph further emphasizes the superiority of the 5780-C5B absorber. B-H curve comparisons illustrate the absorbers’ similar characteristics, indicating a potential loss in magnetic qualities due to absorption, resulting in a high magnetic flux density ratio in the motor compared to the magnetic field strength in the fluid.

Table 7. Properties of 5780-C absorber.

5780-C5B Absorber	
Material	Magnetic powder + rubber
Initial relative permeability	250
Saturation magnetization [T]	Around 2
Knee adjusting coefficient	0.5
Mass density [kg/m <sup>3</sup> ]	4.4
Surface resistance	10 <sup>6</sup>

In Figure 15a,b, obtained by the results of Tables 8 and 9, it is possible to note that the average magnetic flux density on the motor decreases by: 33.44% for the steel material, 43.16% for the aluminium material, and 32.18% for the 5780-C5B absorber material.

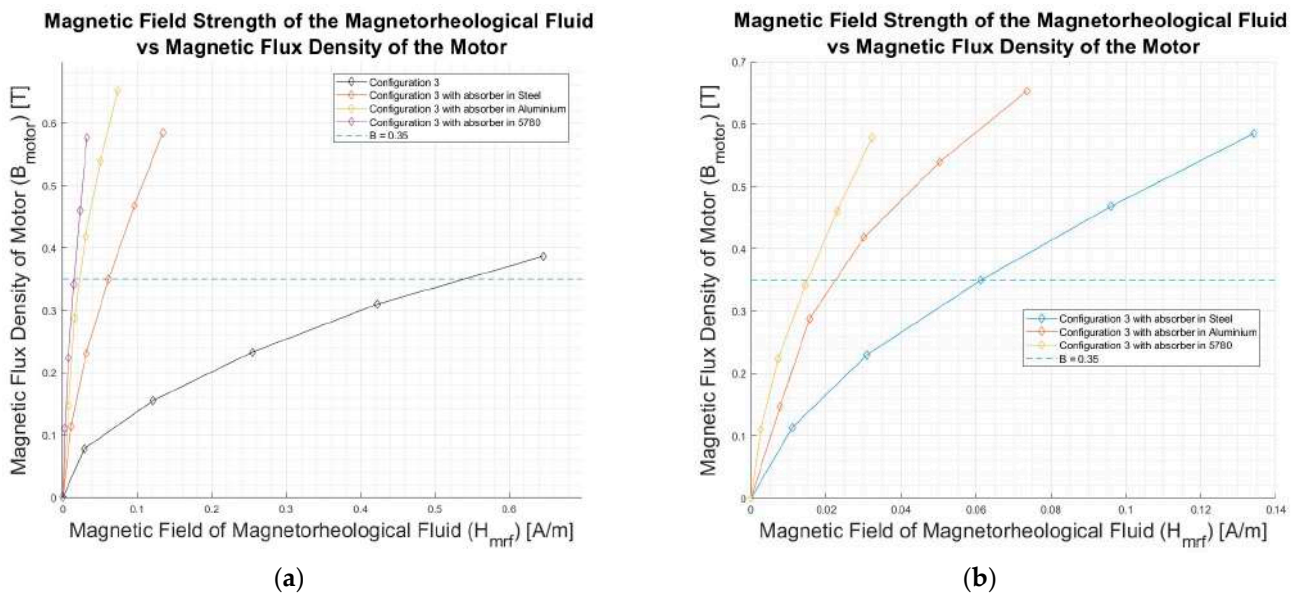


Figure 15. Magnetic field strength of MRF-132-DG vs. Magnetic flux density on Configuration 3: (a) Comparison of B-H curves between three absorbers; (b) Comparison of B-H curves with and without the absorber.

**Table 8.** Comparison of B values for configuration 3 with and without absorber.

Configuration 3—Magnetic Flux Densities on the Motor B [T]				
Coefficient k	Without Absorber	With Absorber in		
		Steel	Aluminium	5780-C5B
$1 \times 10^0$	$3.89 \times 10^{-5}$	$5.64 \times 10^{-5}$	$7.48 \times 10^{-5}$	$5.45 \times 10^{-5}$
$2 \times 10^3$	0.08	0.11	0.15	0.11
$4 \times 10^3$	0.16	0.23	0.29	0.22
$6 \times 10^3$	0.23	0.35	0.42	0.34
$8 \times 10^3$	0.31	0.47	0.54	0.46
$10 \times 10^3$	0.39	0.58	0.65	0.58

**Table 9.** Comparison of H values for configuration 3 with and without absorbers.

Configuration 3—Magnetic Field on the MRF-132-DG H [A/m]				
Coefficient k	Without Absorber	With Absorber in:		
		Steel	Aluminium	5780-C5B
$1 \times 10^0$	$2.70 \times 10^{-6}$	$1.62 \times 10^{-6}$	$1.02 \times 10^{-6}$	$1.51 \times 10^{-6}$
$2 \times 10^3$	$1.00 \times 10^{-2}$	$3.81 \times 10^{-3}$	$1.47 \times 10^{-1}$	$3.71 \times 10^{-3}$
$4 \times 10^3$	$4.24 \times 10^{-2}$	$1.08 \times 10^{-2}$	$2.22 \times 10^{-3}$	$1.02 \times 10^{-2}$
$6 \times 10^3$	$8.90 \times 10^{-2}$	$2.14 \times 10^{-2}$	$5.31 \times 10^{-3}$	$2.03 \times 10^{-2}$
$8 \times 10^3$	$1.48 \times 10^{-1}$	$3.36 \times 10^{-2}$	$1.76 \times 10^{-2}$	$3.21 \times 10^{-2}$
$10 \times 10^3$	$2.26 \times 10^{-1}$	$4.69 \times 10^{-2}$	$2.57 \times 10^{-2}$	$4.51 \times 10^{-2}$

This is obtained by the comparison with the normal state of the brake, without the absorber, as seen in Tables 5 and 6. Increasing the magnetic field strength makes slight changes to the flux density and the magnetic material is said to be saturated. This means that to produce a decrease in flux density a disproportionately large decrease in magnetic field strength is necessary. After the insertion of the absorber, the magnetic field strength on the MRF-132-DG decreases by 77.42% for the steel material, 61.58% for the aluminium material, and 78.35% for the 5780-C5B absorber material. In Figure 15b, the configuration with the absorber in 5790-C5B is linear. This trend occurs because the diminished influence of the magnetic field coming from the motor causes the fluid in a static state to lose magnetization and become more rigid. Similarly, in non-magnetic materials, the magnetization curve is a straight line passing through the origin.

**6. Conclusions**

This article investigates how magnetorheological brakes interact with electric motors. It examines them using a new analytical model, which differs from traditional designs by employing a simplified approach to understand their electromagnetic emissions. The brake design introduces a unique coil arrangement directly on its side housing, deviating from the traditional bobbin-coiled setup. On the other hand, the motor design explores four layouts, with a primary goal of minimizing magnetic field interference between the in-wheel motor and the brake, while remaining within the European directive limits. The two components were studied together through mathematical computations and various simulation analyses, which evaluated the impact of the motor’s magnetic field on the brake, leading to a non-traditional solution inspired by Helmholtz coil configurations. Using this solution, four potential motor–brake configurations are generated, and after thorough evaluation, the third configuration is selected. Simulations and numerical methods applied confirm its accuracy and viability for the intended application.

The behaviour analysed in this work is consistent with similar analyses in terms of FEA simulations of Helmholtz coils [40]. Furthermore, the results of the simulations are not only useful for underlining the effect of the magnetic emissions of the motor on the innovative braking system but also for correlating the Helmholtz coil similitude to real

electromagnetic emissions. The simulation strategy in the present paper is also verified by comparing the obtained direction and strength of the magnetic flux to those found in various FEA studies [41]. In this study, a time- and cost-effective solution is represented, enabling the simulation of how the motor interacts with a brake without the need for designing the entire motor.

A comprehensive study in the fifth section addresses excessive electromagnetic fields using absorbers made of varied materials. Despite minimal interference, the importance of absorbers is highlighted considering potential alterations based on torque and fluid magnetization variations. The proposed unique MRB design requires experimental validation to affirm its effectiveness.

Future works could start from analysing the interaction between the motor and the brake during dynamic braking manoeuvres and while there is an electromagnetic emission from both the motor and the brake. Other advancements include developing a comprehensive multi-physics simulation for magnetic, fluid flow, structural, and heat analysis, followed by experimentally evaluating the innovative MRB design. This article unveils a novel MRB design, navigating optimization complexities, motor selection, and absorber considerations, contributing to the efficiency and resilience of MRBs in diverse operational scenarios, advancing innovation in the field.

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