

Rockfall Hazard Analysis at Small Scale: A Numerical Study for the Estimation of Representative Slope Parameters

Original

Rockfall Hazard Analysis at Small Scale: A Numerical Study for the Estimation of Representative Slope Parameters / Castelli, Marta; Torsello, Giulia; Vallero, Gianmarco. - ELETTRONICO. - 2:(2021), pp. 431-438. (Intervento presentato al convegno 16th International Conference of the International Association for Computer Methods and Advances in Geomechanics 30 August - 2 September tenutosi a Turin (ITA) nel 30 August - 2 September) [10.1007/978-3-030-64518-2_51].

Availability:

This version is available at: 11583/2862592 since: 2021-01-21T11:11:16Z

Publisher:

Springer

Published

DOI:10.1007/978-3-030-64518-2_51

Terms of use:

This article is made available under terms and conditions as specified in the corresponding bibliographic description in the repository

Publisher copyright

Springer postprint/Author's Accepted Manuscript

This version of the article has been accepted for publication, after peer review (when applicable) and is subject to Springer Nature's AM terms of use, but is not the Version of Record and does not reflect post-acceptance improvements, or any corrections. The Version of Record is available online at: http://dx.doi.org/10.1007/978-3-030-64518-2_51

(Article begins on next page)

1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37

Rockfall hazard analysis at small scale: a numerical study for the estimation of representative slope parameters

Castelli M.^{1,*}, Torsello G.¹ and Vallero G.¹

¹ Department of Structural, Geotechnical and Building Engineering (DISEG), Politecnico di Torino
Corso Duca degli Abruzzi 24, 10129, Torino (Italy)
marta.castelli@polito.it

Abstract The identification of rockfall-affected areas depends on a large number of stochastic variables influencing both triggering and propagation phases. Rockfall hazard assessment presents huge uncertainties linked to the various scales of analysis: at the small scale (e.g. valley scale), a quick evaluation of rockfall hazard zones is generally required in order to highlight the most critical situations where more detailed analyses should be carried out. The Cone Method (Jaboyedoff and Labiouse, 2011), recently implemented by Castelli et al. (2019) in the QPROTO plugin for QGIS, allows to reach this goal with simplified geometrical considerations. In a 3D analysis, the energy line angle φ_p and the lateral spreading angle α define a cone of propagation whose apex is located in the rockfall source point. The most significant problem in using the plugin is the evaluation of this angles, which must be defined by the users to consider all the rockfall dissipative processes included in the energy line method (Evans and Hungr, 1993). In this paper a study concerning the influence of slope properties (i.e., forest coverage, inclination) and block characteristics (i.e., shape, volume) is proposed, in order to provide to the users of the plugin a preliminary dataset of calibrated angles.

Keywords: rockfall, hazard analysis, cone method, QGIS, QPROTO.

1 Introduction

Rockfalls are dangerous and widespread phenomena that can affect both natural and artificial slopes inducing damages on structure, infrastructure, economical activities and also killing people. The phenomenon starts with the detachment of a single block or a rocky cluster and can be characterized by large volumes, different block shape and high velocities (Rochet, 1987). Blocks, during their descent paths along the slope, can follow different types of movement such as sliding, rolling, bouncing and free-falling (Varnes, 1978). The complexity of the rockfall can be summarized into two main issues: i) difficulties in providing an exhaustive picture of the landslide causes and the consequent relationships between causes and their effects (i.e., temporal variability of the rockfall magnitude), and ii) modeling the runout phase to provide a spatial description of the expected rockfall scenarios in terms of intensity of the phenomenon (i.e., kinetic energy

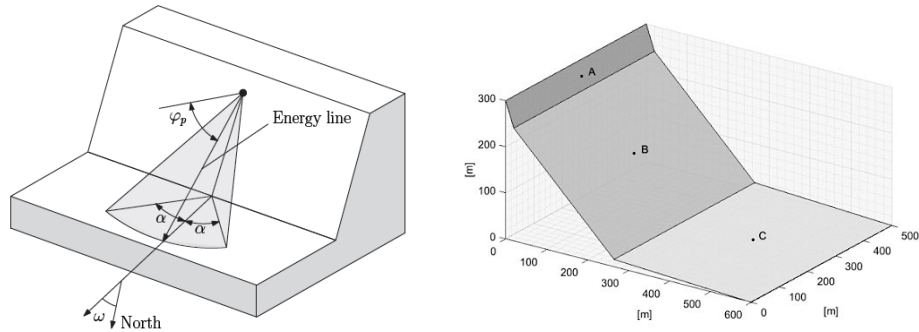
38 content). Over the years, a considerable number of methodologies, correlations and soft-
39 ware have been developed in order to provide more detailed procedures for the hazard
40 estimation, also with the aim of on-site and laboratory tests. Moreover, by using either
41 qualitative or quantitative methodologies, it is possible to assess the vulnerability of the
42 elements at risk within rockfall-prone areas for providing an estimation of the risk level,
43 in space and time components (Fell, 2005).

44 Within the wide set of methods for estimating the extent of rockfall-exposed zones, the
45 simplest ones are the empirical ones. For example, a simple 2D procedure to define the
46 runout area is the *fahrböschung approach* proposed by Heim (1932). This method relates
47 the horizontal length of the runout zone to the vertical height of the affected area by
48 defining an angle β that allows to identify the maximum distance travelled by falling
49 blocks. In 1993, the *fahrböschung* method was modified by Evans and Hungr (1993) in
50 the shadow angle one, by referring not to the source point but to the apex of the talus
51 slope in order to overcome the difficulties in determining the exact location of the source
52 point. Following the Heim's theory, Onofri and Candian theorized the cone method that
53 allows to evaluate the maximum distance covered by a block starting from the detach-
54 ment point (Onofri and Candian, 1979). The methodology was implemented by Ja-
55 boyedoff and Labiouse (2011) in the CONEFALL software. The basic idea is the concep-
56 t of the energy line that is empirically defined in the vertical plane by the straight
57 line connecting the source point with the farthest block stopping point. The inclination
58 of the energy line with respect to the horizontal, defines the angle φ_p that represents all
59 the energy losses suffered by the rock block along its descent path. The complex runout
60 phase can be thought as an equivalent sliding process along the energy line, in which
61 the φ_p angle assumes the meaning of an equivalent friction angle block-slope.

62 The cone method was recently implemented in the QPROTO plugin, developed for
63 QGIS 3.4 environment by Castelli et al. (2019). QPROTO allows to identify the inva-
64 sion area and to estimate the susceptibility and the time-independent (i.e. relative) haz-
65 ard given by a rockfall phenomenon, by conducting a viewshed analysis of the cliff. The
66 viewed areas represent the zones in which rockfall events could occur. Starting from a
67 set of predefined source points, the plugin computes as much visibility cones by adopt-
68 ing only two input parameters: the energy line angle φ_p and the lateral spreading angle
69 α that define the cone in the vertical and horizontal planes, respectively. The vertical
70 distance between the energy line and the topographical surface gives a measure of the
71 kinetic energy of the block in each point of the invasion zone (Fig. 1a).

72 Nowadays, the values of the cone method angles can be found through empirical meth-
73 ods available in literature which have a limited application field (Fratini et al., 2012)
74 restricted to cases where a detailed knowledge of all the parameters and boundary con-
75 ditions affecting a rockfall phenomenon (i.e. slope geometry, material properties, pres-
76 ence of vegetation, protection structures etc.) is available. Thus, the aim of the present
77 paper is to provide to QPROTO users a set of usable values for φ_p and α angles to carry
78 on reliable rockfall simulations. Therefore, a set of parametric analyses was carried out
79 through the software Rockyfor3D which allows to take into account a relevant number
80 of block and slope features (vegetation, volume and shape of the blocks) and also to
81 measure the energy line angle of the simulated trajectories (Dorren, 2015).

82



83

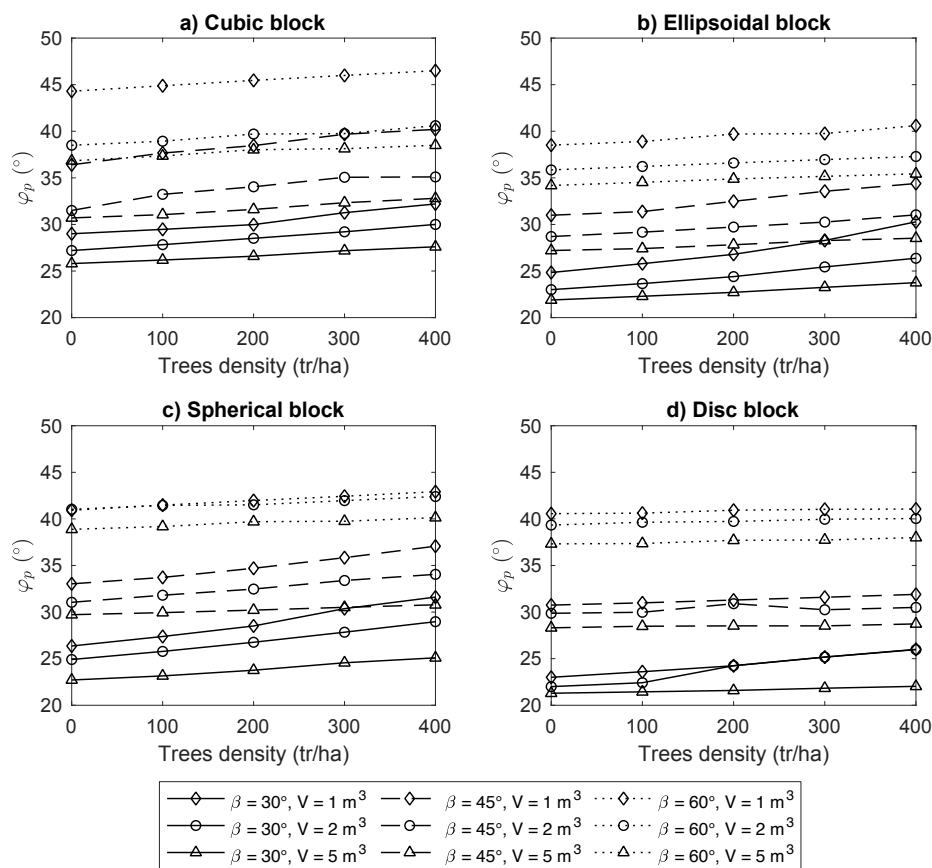
84 **Fig. 1** a) Representation of the parameters characterizing the cone method: the visibility cone is completely
 85 defined by the vertical angle φ_p and the horizontal angle, while the orientation is given by the
 86 aspect of the slope evaluated in the source point. b) Geometry of the synthetic slope: detachment zone
 87 (A), runout zone (B) and stopping zone (C).

88 2 Estimation of the input parameters for QPROTO plugin

89 QPROTO is a simplified tool for assessing the rockfall hazard. Its simplicity is linked
 90 to the few parameters required for carrying on its analyses. In particular, the φ_p angle is
 91 still a mechanical parameter including in its value all the variables that can potentially
 92 influence a rockfall process, i.e., morphological characteristics of the slope (steepness,
 93 length, trees density, roughness, presence of protection works, etc.) and rock block fea-
 94 tures (volume and size). In order to relate the above-mentioned elements to the corre-
 95 sponding φ_p values, a set of trajectographic analyses have been performed using the
 96 rigid body 3D probabilistic method implemented into the software Rockyfor3D (Dorren,
 97 2015). The analyses were carried out through the synthetic slopes which are obtained
 98 from the union of three planar surfaces (Fig. 1b): detachment zone (A), runout zone (B)
 99 and stopping zone (C) (Netti et al., 2016). The slopes have been generated using a con-
 100 stant value of the height, a different value of the inclination angle β (i.e., the inclination
 101 of the line connecting the source point with the cliff foot, β : 30° , 45° , 60°) and a semi-
 102 flat stopping area with an inclination of about 2° . In order to obtain comparable results,
 103 the morphological characteristics of the slopes are the same; the soil type used in the
 104 simulations is talus slope or compact soil with large rock fragments for both the detach-
 105 ment and runout zones (A and B) and fine soil material for the stopping zone (C)
 106 (Dorren, 2015).

107 Therefore, slopes are discretized by using Digital Terrain Model (DTM, hereafter) with
 108 cell size of 5 m: the source area is a single DTM cell with four different shapes (i.e.,
 109 cubic, ellipsoidal, spherical and disc), three different volumes (i.e., 1 m^3 , 2 m^3 , 5 m^3)

110 and a constant rock density of 2500 kg/m^3 . Rockyfor3D allows to take into account the
 111 effect of trees on the trajectories. Thus, five levels of vegetation density were consid-
 112 ered: 0, 100, 200, 300 and 400 trees/ha (i.e., 1 tree/DTM cell). Trees were placed only
 113 in the runout area and their essence was set 100% conifers, considering their least mech-
 114 anical resistance to rockfall impacts (Stokes et al. 2005, Dorren and Berger, 2005). A
 115 value of 35 cm for the breast-height diameter (DBH) was finally established.
 116 A total number of 20000 simulated trajectories for each combination of parameters was
 117 conducted and the final energy line angle was defined as the 2% ($\varphi_{p,2\%}$) of the empirical
 118 distribution function (EDF) i.e., the angle value that have the 98% of probability to be
 119 maximized. It is obvious that smaller angles relate to wider runout area and thus precau-
 120 tionary values have to be considered.



121

122 **Fig. 2** Energy line angle values sorted with reference to the block shape. a) Cubic shape gives the higher
 123 values of φ_p . b) and c) are related to ellipsoidal and spherical blocks, respectively. It can be seen that
 124 the corresponding angle are generally lower in this case because of the higher rotational inertia of these
 125 shapes. d) In disc shape case the minimum angles are obtained.

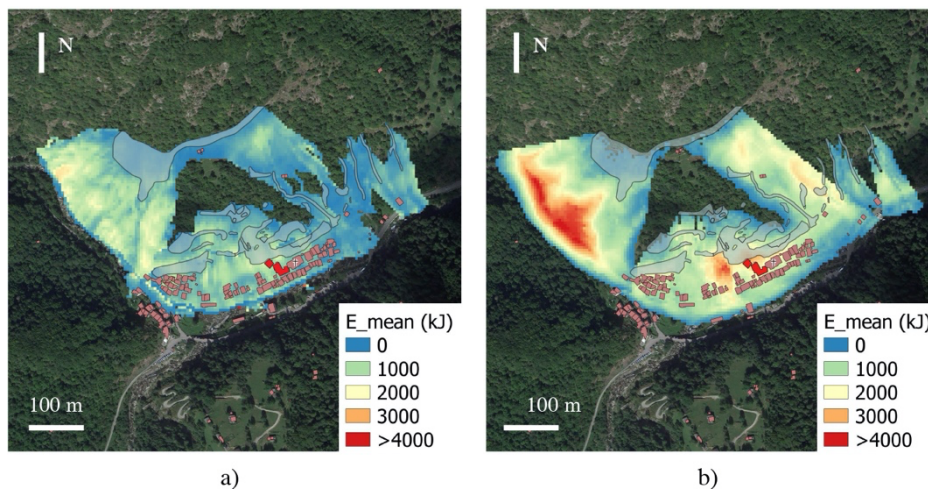
126 In order to analyze the results obtained from the synthetic slopes (Fig. 2) and to highlight
127 the most relevant aspects, it is possible to observe that a considerable increase of φ_p
128 angles is linked to the growing of the slope steepness (i.e., the β angle). This growing
129 is more relevant for smaller volumes while 5 m³ blocks have smaller energy line angles.
130 Limited slope steepness increases the rolling of the blocks also in the stopping zone of
131 the synthetic cliff, decreasing the corresponding energy line angles. The density of trees
132 increases the φ_p angles with a maximum difference of about 5°, especially in case of
133 cubic, ellipsoidal and spherical shapes. The disc shape is less influenced by the forest
134 because of its highest rotational inertia that provides longer descent paths to blocks. 5
135 m³ blocks are minimally influenced by trees allowing to conclude that this volume is the
136 maximum limit for trees to still play a protective role against rockfalls (Torsello, 2019).
137 The influence of shape is highly clear: cubic blocks give maximum energy angles while
138 minimum ones are due to disc shaped boulders.
139 Highest values of energy line angle can be found for a volume of 1 m³ and β angle of
140 30° for cubic, ellipsoidal and spherical blocks while smaller values can be found for disk
141 shaped blocks. A lower value of energy line angle φ_p corresponds to greater runout
142 lengths and to greater kinetic energies with a minor capacity to stop or decelerate blocks
143 by trees, according with the case study reported in Kobayashi et al. (1990) in which a
144 disk-shaped block smashed trees up to 0.6 m and followed a total horizontal travel dis-
145 tance of about 420 m.

146 **3 Case study: the Rassa site**

147 In order to test the reliability of the above described results, an application to a real case
148 study is reported in the following. The investigated area belongs to Rassa municipality,
149 which is located in the Sesia Valley, Western Italian Alps, at an altitude of 917 m a.s.l.
150 (UTM: 423539, 5068593, 32, T). Rassa is composed by four main hamlets: Bunadaccia-
151 Scarpie at West, San Giovanni-Concentrico at South, Torbe-Orello at Est and Piana
152 Giacchè at North. The inhabited area of San Giovanni-Concentrico is located nearby the
153 confluence of Gronda and Sorba creeks, at the basis of a steep slope that reaches a max-
154 imum altitude of about 1100 m a.s.l. The cliff is covered by a sparse mixed broad-leaved
155 forest. Different landslides phenomena have been affected the whole studied area: the
156 last rockfall event occurred after a huge rainfall event in October 2018, when a 0.1 m³
157 block reached the San Giovanni church without causing damages. In order to calibrate
158 the parameters, a back analysis of the 2018 event was performed, using Rockyfor3D
159 and adopting the DTM (5 x 5 m) provided by the Piedmont Region. The energy line
160 angle φ_p was estimated starting by this analysis and a value of 43° was found. This
161 value was therefore used within the QPROTO plugin as the input parameter to replicate
162 the October 2018 event.

163 Then, a forecasting set of analyses for the Rassa site was performed in order to estimate
164 the hazard level of the area. From geo-structural surveys of the rock face it has been
165 shown that the maximum magnitude scenario was related to a volume of 5 m³.

166 Therefore, a forecasting Rockyfor3D simulation was carried out with reference to this
 167 volume scenario (Fig. 3a). The analysis was computed by adopting a cubic block shape
 168 and a trees density of 400 trees/ha, evaluated on the basis of an on-site survey of the
 169 Rassa forest. The rockfall detachment niches were identified with the most fractured
 170 portion of the rock face. In order to test the reliability of the angle abacus described in
 171 this paper, a QPROTO simulation of the 5 m³ scenario was carried out. The energy line
 172 angle φ_p was 33°, obtained in correspondence of a trees density of 400 tree/ha, a cubic
 173 block shape and a slope angle of 45° (Fig. 2a). The results are reported in Fig. 3b. It can
 174 be seen that the QPROTO and Rockyfor3D invasion areas are the same while QPROTO
 175 kinetic energy values are higher than Rockyfor3D ones, especially in the Western por-
 176 tion of the area. This is due to the different starting hypotheses characterizing the two
 177 approaches. The quick nature of the cone method has to provide precautionary results
 178 able to highlight the zones in which most in-depth analyses should be carried on.



179 a) 180 **Fig. 3** Output of the two forecasting analysis for the 5 m³ scenario. The light grey area relates to the
 181 rockfall source zones characterized by the fractured rock face, the light red rectangles highlights the
 182 Rassa village while the red buildings are the structures interested by the 2018 event: a) Rockyfor3D
 183 simulation, b) QPROTO simulation.

184 4 Conclusions

185 In this paper the preliminary results of the calibration activity of energy line angles for
 186 cone method are reported. This work assumes a crucial importance in order to provide
 187 usable and reliable input data for carrying on quick hazard analysis by adopting the cone
 188 method and, especially, the QPROTO plugin. A series of parametric analyses were car-
 189 ried out to investigate the possible correlations between φ_p and both block and slope
 190 characteristics. Referring to the block features, the results show that the influence of the

191 volume and the size are evident. In particular, smaller angles are due to larger volumes
 192 and disc-shaped boulders. With reference to the slope, the steepness is the key topic and
 193 largest angles are given by steepest slopes. Also the forest density influences the results:
 194 smaller volumes (i.e., 1 and 2 m³) are associated to the maximum tree effect and the φ_p
 195 grows together with the increase of the density of trees. The lateral spreading angle α
 196 seems to have a small variability but further studies should be carried out in order to
 197 investigate the role of this parameter. In this preliminary work we suggest a value of
 198 lateral spreading angle in a range of $\pm 20^\circ$ around the dip direction of the slope.
 199 The results were tested in the case study of Rassa village. It can be seen that the esti-
 200 mated angles provide precautionary hazard maps with respect to the same ones com-
 201 puted by using a usual trajectographic software (Rockyfor3D). This is a good issue be-
 202 cause a quick method, such as QPROTO is, have to be sufficiently precautionary in
 203 order to supply preliminary rockfall hazard evaluations.
 204 The above described analyses have been conducted by adopting simplified hypotheses
 205 such as constant roughness values and absence of rockfall protection works along the
 206 synthetic slopes. These two aspects can considerably affect the results and further stud-
 207 ies are ongoing in order to overcome the limit of the present works.

208 **Acknowledgements** The Authors gratefully express their thanks to G. Cavagnino for
 209 the concession of the case study data and its willingness in providing all the required
 210 support for their interpretation. This work has been partially supported by the Italian
 211 Ministry of Education, Universities and Research in the framework of the Project of
 212 Relevant National Interest (PRIN 2015) on “Innovative Monitoring and Design Strate-
 213 gies for Sustainable Landslide Risk Mitigation”.

214 **References**

- 215 Castelli, M., Grisolia, M., Barbero, M., Vallero, G., Campus, S., Pispico, R. and Lanteri, L.
 216 (2019). A GIS-based procedure to estimate rockfall hazard at a small scale: the QPROTO tool.
 217 *Nat Hazards* (in preparation).
- 218 Dorren, L K A and Berger, F. (2005). Stem breakage of trees and energy dissipation during rainfall
 219 impacts. *Tree physiology* 26(1), 63-71.
- 220 Dorren, L.K.A. (2015) Rockyfor3D (v.5.2). Revealed-transparent description of the complete 3D
 221 rockfall model. *EcorisQ paper* (www.ecorisq.org).
- 222 Evans, G. S. and Hungr, O. (1993). The assessment of rockfall hazard at the base of the talus
 223 slope. *Canadian Geotechnical Journal* 30, 620-636.
- 224 Fell, R., Ho, S., Lacasse, S., Leroi, E. (2005). A framework for landslides risk assessment and
 225 management. *Landslide risk management: proceedings of the international conference on*
 226 *landslide risk management*, Vancouver, Canada, May 31-June 3, Taylor & Francis, London,
 227 33-26.

- 228 Frattini, P., Crosta, G.B., & Agliardi, F. (2012). Rockfall characterization and modeling. In J.J.
229 Clague, & D. Stead (a cura di), *Landslides Types, mechanisms and modeling*, Cambridge Uni-
230 versity Press, 267-281.
- 231 Heim, A. (1932). Bergsturz und Menschenleben. Beiblatt zur Vierteljahrschrift der Naturfor-
232 schenden Gesellschaft in Zürich 77, 1-127.
- 233 Jaboyedoff, M. and Labiouse, V. (2011). Preliminary estimation of rockfall runout zones. *Nat*
234 *Hazards Earth Sys Sci* 11(3), 819-828.
- 235 Kobayashi, Y., Harp, EL., Kagawa, T. (1990). Simulation of rockfalls triggered by earthquakes.
236 *Rock Mechanics and Rock Engineering* 23, 1-20.
- 237 Netti, T., Castelli, M., De Biagi, V. (2016). Effect of the Number of Simulations on the Accuracy
238 of a Rockfall Analysis. *PROCEDIA ENGINEERING* 158, 464-469.
- 239 Onofri, R. and Candian, C. (1979). Indagine sui limiti di massima invasione dei blocchi rocciosi
240 franati durante il sisma del Friuli del 1976: considerazioni sulle opere di difesa. Regione auto-
241 noma Friuli-Venezia-Giulia, *CLUET*, 1-42.
- 242 Rochet, L. (1987). Application des modèles numériques de propagation à l'étude des éboulements
243 rocheux (Application of numerical propagation models to the study of rocky landslides). *Bul-*
244 *letin Liaisons des Ponts et Chaussées* 150-151, 84-95.
- 245 Stokes, A., Salin, F., Kokutse, A. D., Berthier, S., Jeannin, H., Mochan, S., Dorren, L., Kokutse,
246 N., Abd.Ghani, M., Fourcaud, T. (2005). Mechanical Resistance of Different Tree Species to
247 Rockfall in the French Alps. *Plant and Soil* 278, 107-117.
- 248 Torsello, G. (2019). La modellazione del fenomeno di caduta massi a piccola scala: valutazione
249 dei parametri necessari per analisi speditive. *Politecnico di Torino*, Laurea Magistrale in Inge-
250 gneria Edile.
- 251 Varnes, D. J. (1978). Slope movement types and processes. Special Report 176: Landslides: Anal-
252 ysis and Control (Eds: Schuster, R. L. & Krizek, R. J.). *Transportation and Road Research*
253 *Board*, National Academy of Science, Washington D.C., 11-33.