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## Article

# Investigation of the Mechanical Properties of a Carbon Fibre-Reinforced Nylon Filament for 3D Printing

Flaviana Calignano <sup>1,\*</sup> , Massimo Lorusso <sup>2</sup> , Ignazio Roppolo <sup>3</sup>  and Paolo Minetola <sup>1</sup> 

<sup>1</sup> Department of Management and Production Engineering, Politecnico di Torino, Corso Duca degli Abruzzi 24, 10129 Turin, Italy; paolo.minetola@polito.it

<sup>2</sup> Istituto Italiano di Tecnologia, Center for Sustainable Future Technologies IIT@Polito, Corso Trento 21, 10129 Turin, Italy; massimo.lorusso@iit.it

<sup>3</sup> Department of Applied Science and Technology, Politecnico di Torino, Corso Duca degli Abruzzi 24, 10129 Turin, Italy; ignazio.roppolo@polito.it

\* Correspondence: flaviana.calignano@polito.it; Tel.: +39-011-090-7218

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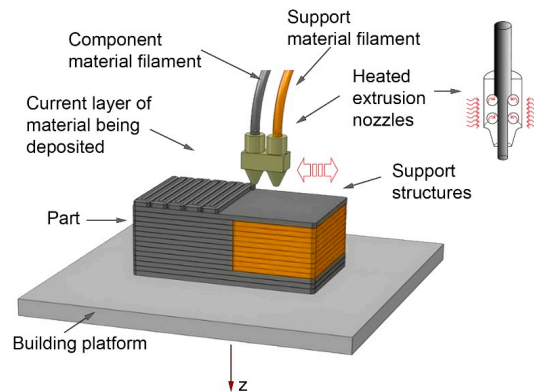
**Abstract:** Additive manufacturing (i.e., 3D printing) has rapidly developed in recent years. In the recent past, many researchers have highlighted the development of in-house filaments for fused filament fabrication (FFF), which can extend the corresponding field of application. Due to the limited mechanical properties and deficient functionality of printed polymer parts, there is a need to develop printable polymer composites that exhibit high performance. This study analyses the actual mechanical characteristics of parts fabricated with a low-cost printer from a carbon fibre-reinforced nylon filament. The results show that the obtained values differ considerably from the values presented in the datasheets of various filament suppliers. Moreover, the hardness and tensile strength are influenced by the building direction, the infill percentage, and the thermal stresses, whereas the resilience is affected only by the building direction. Furthermore, the relationship between the mechanical properties and the filling factor is not linear.

**Keywords:** additive manufacturing; 3D printing; fused filament fabrication; carbon fibre; mechanical testing

## 1. Introduction

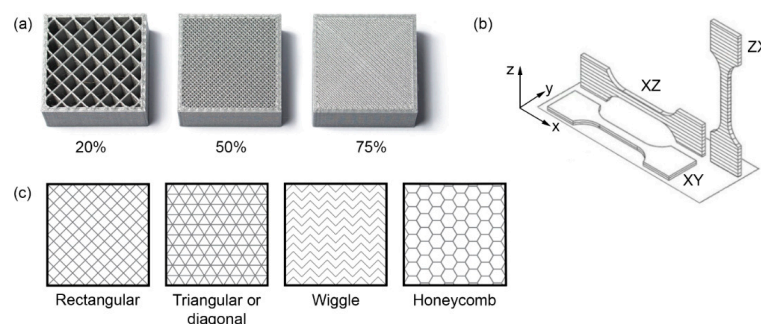
Additive manufacturing (i.e., 3D printing) is constantly evolving due to open source technologies [1–3] and the possibility of producing complex geometries with lower costs, faster production times, and less waste [4–6] than traditionally manufactured parts [7]. Moreover, with the increase in available materials, 3D printing has found applications in the aerospace and architectural industries (e.g., creating complex lightweight and structural models) [8,9], art fields [10,11], and medical fields (e.g., printing tissues and organs) [12,13]. However, most plastic 3D printed products are still used primarily as conceptual prototypes rather than functional components because of the poor mechanical and functional properties of the neat polymer used in 3D printing. The development of polymer composites solves these problems [14]. The incorporation of fibre and nanomaterial reinforcements into polymers allows the manufacture of polymer matrix composites, which are characterized by high mechanical performance and excellent functionality [14,15]. One process that has been extensively utilized in the fabrication of polymeric 3D printed parts is fused deposition modelling (FDM), which was developed by Stratasys Inc. In 2009, Stratasys's FDM printing patent expired, opening up the market for low-cost FDM 3D printers. For non-Stratasys 3D printers, this process is usually referred to as fused filament fabrication (FFF). In FFF, a thin filament wire is extruded through a heated nozzle (Figure 1).

The FFF head moves in the x and y directions, whereas the platform moves in the z direction. The part is manufactured by the sequential build-up of these layered depositions, during which each new layer fuses with material that has already been deposited. The final strength, quality, cost and production time of the parts fabricated by FFF are influenced by some process parameters, such as layer thickness, infill pattern, extruder uniformity and/or build-bed temperature, and by the presence of reinforcing materials (e.g., carbon fibres, glass fibres [16]).



**Figure 1.** Fused filament fabrication process.

Some researchers have correlated the build orientation (Figure 2b) to the mechanical properties of the part [17–22]. The variations in quality of the melt between adjacent filaments results in a degradation in mechanical properties (tensile strength, compressive strength, flexural strength, hardness, and elastic modulus), especially for parts tested perpendicular to the direction of layer construction. In addition to the orientation of the part on the building platform, the mechanical properties of FFF parts are also significantly influenced by the process parameters of inherent layering (Figure 2a,c), such as the layer thickness, raster angle, raster width, infill pattern and air gap [17,22–25]. Ahn et al. [23] determined that both the air gap and the raster orientation had significant effects on the resulting tensile strength, whereas these factors did not affect the compressive strength. A similar study was carried out by Sood et al. [17] with varying factors of layer thickness, build orientation, raster angle, raster width, and air gap: the tested factors influenced the mesostructural configuration of the built part and the bonding and distortion within the part. Lužanin et al. [26] studied the effects of layer thickness, deposition angle and infill percentage on the maximum flexural force in FFF specimens made of polylactic acid (PLA) and concluded that layer thickness has the maximum effect on the flexural strength followed by the interaction between the deposition angle and the infill percentage. Despite its advantages over conventional manufacturing processes, FFF parts often exhibit low mechanical properties. One of the possible methods to improve the strength of FFF parts is adding reinforcing materials, such as carbon fibres, into pure thermoplastic matrix materials to form carbon fibre-reinforced thermoplastic composites [27–29]. Several studies have been conducted related to FFF and carbon fibre (CF) composites. A list of various studies of FFF with chopped fibre-reinforced thermoplastics is given in Table 1.



**Figure 2.** Examples of (a) infill percentage, (b) build orientation and (c) infill pattern.

**Table 1.** A summary of some studies on FFF with chopped fibres.

Reinforcement	Matrix Material	Investigated Properties	Limitations	References
Carbon fibres	ABS	Tensile strength and tensile modulus	Porosity, weak interfacial adhesion between the fibres and the matrix and fibre breakage	[27]
Vapour-grown carbon fibres	ABS	Tensile strength and tensile modulus	Interlayer fusion, intralayer fusion, and a change from ductile to brittle behaviour	[28]
Carbon fibres	ABS	Strength, stiffness, thermal properties, distortion, and geometric tolerances		[30]
Carbon fibres	ABS	Tensile strength, Young's modulus, and flexural properties	Decreases in toughness, yield strength and ductility and increases in porosity with increased carbon fibre content	[31]
Carbon fibres	PLA	Tensile strength and tensile modulus		[32]
Carbon fibres	PLA	Fracture properties	Critical factors for the fracture toughness: bead layup sequence, fiber pullout, interfacial de-bonding, and void formation	[33]
Carbon fibres	PLA	Tensile strength	Tensile strength increases with infill density and low layer thickness	[34]
Carbon fibres	Nylon	Charpy impact testing	Toughness results show a severe anisotropy in toughness and high dependence on the infill strategy	[35]

Love et al. [30] showed that filaments made from CFs and acrylonitrile butadiene styrene (ABS) polymer significantly increase the strength and stiffness of the final parts: the tensile strength and stiffness of the composite sample were 70.69 MPa and 8.91 GPa, respectively, whereas these values for the pure ABS sample were 29.31 MPa and 2.05 GPa, respectively. They also demonstrated that the addition of CFs decreased the distortion of the printed ABS/CF, which was attributed to the 124% increase in thermal conductivity compared to unfilled ABS. Ning et al. [31] investigated the material properties of ABS polymer matrices with different CF contents. They concluded that compared with pure ABS specimens, adding CFS into ABS could increase the tensile strength and Young's modulus but may decrease the toughness, yield strength and ductility. Porosity became the most severe in the specimens with a 10 wt% carbon fibre content. Ivey et al. [32] analysed specimens produced using a commercial polylactic acid (PLA) filament and a PLA filament reinforced with short-carbon fibres (PLA/CF). The tensile properties of the PLA and PLA/CF filaments showed that the addition of carbon fibres to the PLA filament led to a significant increase in the elastic modulus of the FFF samples. The fracture properties (stress intensity factor and energy release rate) of PLA and its short CF reinforced composites have been studied by Papon and Haque [33]. Different CF concentrations were printed with two bead lay-up orientations using PLA and CF/PLA composite filaments. The most critical factors for the fracture toughness seem to be the bead layup sequence, fiber pullout, interfacial de-bonding, and void formation. Higher fiber contents did not show improvement in fracture toughness due to higher intra-bead voids, microcracks, and poor interfacial bonding. Yasa [35] pointed out that the build orientation has a significant influence of carbon-reinforced tough nylon. The impact toughness of specimens built vertically was reduced by 90% in comparison to other directions where the impact was not received in between deposited layers. In 2014, MarkForged© developed the first continuous carbon fibre composite 3D printer. Printed samples generated with MarkForged© printers have been characterized in previous studies [36–39]. A summary of some studies focused on the FFF of

continuous fibre-reinforced polymers is given in Table 2. These studies observed some discontinuities in the construction of samples: the carbon fibres were not completely continuous. Experiments showed that discontinuities in the fibres led to premature failure in areas where the fibres were absent, severely reducing the tensile strength of the sample.

**Table 2.** A summary of some studies on FFF with continuous fibres.

Reinforcement	Matrix Material	Investigated Properties	Limitations	References
Carbon fibres	Nylon	Tensile properties	Discontinuities of the fibres and porosity	[36]
Carbon, glass and Kevlar fibres	Nylon	Tensile properties	Poor bonding and porosity	[37]
Carbon, glass and Kevlar fibres	Nylon	Tensile and flexural properties	Weak bonding and porosity	[38]
Carbon fibres	PLA	Flexural strength and modulus	None reported	[39]

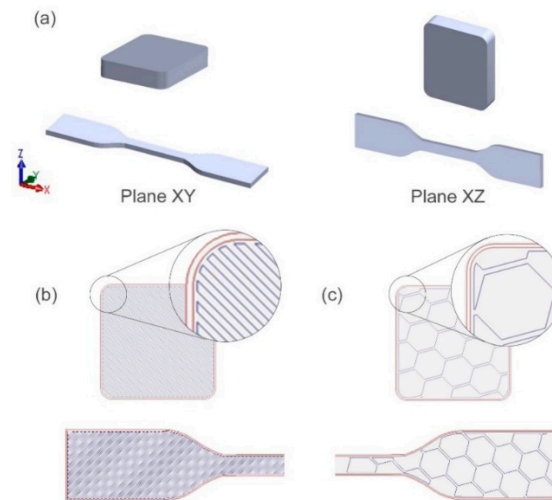
This study investigated the performance of parts produced with an FFF 3D printer from chopped carbon fibre-reinforced nylon filaments (nylon-carbon). This filament is composed of nylon 612 with 20% carbon fibres. Nylon 612 (Polyamide 612) gives high resistance to the filament (high impact strength; good resistance to greases, oils, fuels, hydraulic fluids, water, alkalis and saline; good stress cracking resistance; low coefficients of sliding friction; high abrasion resistance; and high tensile and flexural strength [40]), a relatively low water absorption and a high dimensional stability. The CFs add stability and rigidity, which makes the parts less likely to warp than standard nylon. Due to these characteristics, this filament is ideal for engineering parts, custom end-use production parts, functional prototyping and testing, structural parts, jigs, fixtures, and other tooling. Although the extrusion of preimpregnated fibres does not allow changes in the fibre volume fraction, this approach eliminates the problems associated with poor fibre/matrix interfaces if the impregnation is good and if adequate process parameters are selected. However, the high values of mechanical properties (e.g., tensile modulus of 500–8000 MPa, tensile strength of 54–110 MPa, and hardness of 110 MPa) found in the material datasheets from various manufacturers do not specify the construction conditions, i.e., orientation and filling. This is because some data is obtained by building specimens with other technologies, such as injection molding. In the last year alone, filament manufacturers have been trying to provide mechanical test data by making the specimens using FFF technology. Therefore, the purpose of this study is to analyse the actual mechanical characteristics of a nylon-carbon filament using a low-cost printer.

## 2. Materials and Methods

### 2.1. Fabrication of Samples

In this study, a nylon-carbon filament produced by Fiber Force Italy [41], which had a standard diameter of 1.75 mm, was used for 3D printing. The nylon-carbon filament is composed of nylon 612 with 20% carbon fibres (chopped fibres with a random orientation). Each fibre is approximately 10 µm in diameter and 30 µm in length. A Sharebot Next Generation printer with a 0.4 mm nozzle was used to print tensile and Charpy impact test specimens with a layer thickness of 0.20 mm and three different values of infill, 15%, 80%, and 100%, in two different planes, XY and XZ (Figure 3). Many of the samples produced on the ZX plane showed defects during construction due to problems regarding adhesion on the building platform. For this reason, these samples were not analysed. Choosing an infill pattern depends on the kind of model, the desired structural strength, and the print speed. In general, rectilinear, linear and honeycomb infill patterns are preferred. From a study conducted by Akhoundi and Behravesh [42], honeycomb was found to be the least favourable pattern at a filling

percentage of 100, whereas it provided better properties at a low filling percentage. The honeycomb pattern is more susceptible to creating small voids in the matrix, leading to a significant reduction in the specific tensile strength [42]. Therefore, filling with 15% of the material was realized with a honeycomb structure. The first four layers and the last four layers that enclose the part are filled with a solid layer. Linear filling was used for the samples with filling percentages of 80% and 100%. Table 3 shows the parameters of the 3D printing process.



**Figure 3.** (a) Sample building direction, (b) linear filling at 100%, and (c) honeycomb filling at 15%.

**Table 3.** 3D printing process parameters.

3D Printer	Filament	Value
Sharebot Next Generation	Diameter	1.75 mm
	Extruder temperature	230 °C
	Bed temperature	40 °C
	Perimeter print speed	35 mm/s
	Infill and support print speed	40 mm/s
	Layer height	0.20 mm

## 2.2. Mechanical Testing

The mechanical properties relevant for the sports, automotive and aerospace industries, such as the hardness, tensile and resilience of 3D printed nylon-carbon specimens, are evaluated via mechanical testing.

During the Brinell hardness test (ISO 2039-1, DIN 53456), an indenter comprising a hardened steel ball (diameter: 5 mm) is pressed into the top surface of the sample for a standard length of time (30 s) under a standard load of 49 N [43]. After removing the load, the circular indentation is then measured in two mutually perpendicular directions, taking the average of the two readings. The hardness  $H$  [N/mm<sup>2</sup>] is the ratio between the applied load and the surface area of the impression.

Tensile tests were conducted in accordance with ASTM D638 using an Instron 3366 dynamometer, which was equipped with a 10 kN load cell, at a strain rate of 10 mm/min. Five specimens for each set were tested, and the final results were obtained by averaging the data.

Charpy impact tests were performed with a Charpy Zwick Roell B513E to study the energy absorption of the different samples. The test was carried out in accordance with ISO179-1, and the unnotched specimen dimensions were 80 × 10 × 4 mm. The distance between the supports was 40 mm. Five samples for each set were tested. After the test, each sample was inspected, and the fracture surface was photographed.

### 3. Results and Discussion

#### 3.1. Hardness and Tensile Properties

In Table 4, the hardness values are reported. The results showed that the samples produced in the XY plane have a higher hardness than the samples produced in the XZ plane. This discrepancy is evident for the samples with 100% filling, whereas for the other samples with 15% and 80% filling, the effect is not as clear. The samples built in the XZ plane with 80% and 100% filling have similar hardness. Increasing the filling percentage results in an increase in the hardness in the XY plane but also increases material costs and lengthens production times.

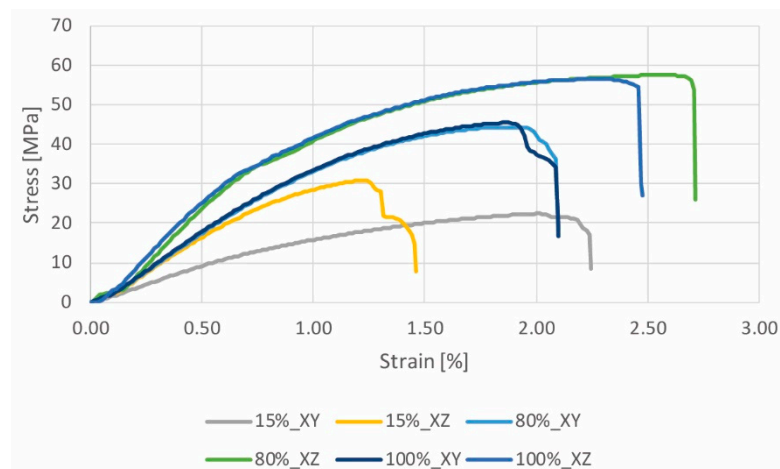
**Table 4.** Hardness values in N/mm<sup>2</sup>.

Number Indentation	Filling Percentage and Building Direction					
	15%, XY	15%, XZ	80%, XY	80%, XZ	100%, XY	100%, XZ
1	14.4	10.1	55.6	48.5	80.1	51.1
2	10.3	9.2	54.7	49.3	80.9	45.4
3	13.0	11.5	53.5	52.2	78.3	52.2
4	10.3	13.0	48.2	53.7	75.3	41.3
5	8.5	10.0	55.9	45	81.9	43.4
Average	11.3	10.8	53.6	49.7	79.3	46.7
Std. dev.	2.4	1.5	3.1	3.4	2.6	4.8

In Table 5 and Figure 4, the results from the tensile tests are reported. The results show that, in general, the specimens built in the XZ direction are stiffer than those built in the XY direction; the former exhibit higher Young's modulus and higher stress at break. In contrast, the energy at break is higher for the samples built in the XY direction.

**Table 5.** Tensile test results for the specimens printed on a Sharebot printer from a 1.75 mm filament.

Sample	Young's Modulus E [MPa]	$\sigma_Y$ [MPa]	$\sigma_{UTS}$ [MPa]	$\sigma_{break}$ [MPa]	Elongation at Break [%]	Energy at Break [mJ]
15%, XY	930 ± 77	17 ± 0.3	22 ± 0.7	21 ± 0.7	2.0 ± 0.2	202 ± 50
15%, XZ	1467 ± 21	26 ± 0.8	31 ± 0.6	25 ± 0.6	1.5 ± 0.1	76 ± 15
80%, XY	1552 ± 60	35 ± 0.4	44 ± 1.2	37 ± 1.2	2.2 ± 0.1	625 ± 194
80%, XZ	2294 ± 154	36 ± 1.8	57 ± 4.1	44 ± 4.1	2.6 ± 0.5	361 ± 119
100%, XY	1625 ± 64	39 ± 1.4	45 ± 1.9	38 ± 1.9	2.0 ± 0.1	464 ± 209
100%, XZ	2403 ± 95	42 ± 1.7	56 ± 3.9	45 ± 3.9	2.8 ± 1.0	163 ± 89



**Figure 4.** Stress-strain curves.



As previously reported by Rodriguez et al. [44], this means that building in the XZ direction leads to stiffer and more fragile components, whereas when an object is built in the XY direction, the object is softer but more resistant to failure.

Regarding the filling factor, as the filling percentage increases, the specimen stiffness increases. The choice of the type of infill pattern can influence the behaviour of the material, leading to a nonlinear relationship between the mechanical properties and the filling factor. For instance, the Young's modulus of the samples with a filling factor of 15% (honeycomb infill pattern) is approximately 60% of the average Young's modulus of the specimens with a filling factor of 100% (linear infill pattern), independent of the building direction. The modulus values with a filling factor of 80% (linear infill pattern) increase by up to 95%. A similar trend could be evidenced for the tensile strength at break  $\sigma_{\text{break}}$  (53% for a 15% filling factor and 97% for an 80% filling factor). This finding means that once the stiffness requirements for a component are established, important weight reductions could be implemented by using only the amount of material sufficient to satisfy the criteria and the most suitable infill pattern. On the other hand, the use of an exceeding amount of material could be even detrimental: the more material there is, the more defects generated during the printing process, leading to a decrease in the mechanical properties. Although 100% fill density can provide maximum strength, it can negatively affect the overall cost by increasing the print time and the amount of material consumed. For certain applications, it is not necessary to use a fill density of 100% due to the nature of the application itself, for example in the case of components not subjected to loads or stresses of certain amounts. Therefore, determining the required fill density based on the nature and application of the product would be very important for large-scale production lines to optimize resources. Obviously, the load capacity of the printed parts is a function of the filling density, the fraction of the volume of the fiber to the matrix and the quality of the chemical and mechanical bond between droplets/layers. Low fill densities can lead to an increase in gaps within the structure (i.e., an increase in porosity) and this can cause the strength of the part to decrease [45]. A filling percentage of 100% can cause raster overlap or a negative air gap size, which, in turn, negatively influences the strength of the material.

Regarding the mechanical properties in the XZ orientation, a filling percentage of 80% improves the material characteristics, among which the hardness slightly increases and the energy at break increases more substantially. In the XY orientation, the difference between the samples produced with the 15% honeycomb strategy and those produced with higher filling percentages (linear filling) is more consistent in terms of hardness than stiffness. This finding confirms that the combination of filling percentage and filling strategy has a high effect on the mechanical properties. Fernández-Vicente et al. [46] carried out a study that analysed the influence of the pattern and infill percentage: the density of the infill was a decisive factor in tensile strength, and the combination of a rectilinear pattern and a 100% filling percentage provided the greatest tensile strength. This result was not fully found in the present case. Samples with 80% and 100% filling percentages exhibited similar values for the Young's modulus and stress at break with differences of 4% and 5% in the XY and XZ planes, respectively. The greatest deviation is observed for energy at break: samples with 80% filling exhibited higher values (+35% and +121% in the XY and XZ planes, respectively) than those built with 100% filling. This finding can be explained by considering the following factors: thermal stresses during construction, random orientation of the fibres and filling percentage. Residual stresses induced in the layer-by-layer fabrication process of additive manufactured parts have a significant impact on their mechanical properties and dimensional accuracy [23,47]. Based on the coefficient of thermal expansion (CTE), the material is prone to shrinkage, which induces internal stresses due to the evolving material stiffness upon solidification and the bonds between the beads constraining the material. A fraction of these stresses is released due to viscoelastic relaxation and material deformations. During cooling, the crystallization reaction introduced additional strains that promote internal stresses and partial deformations. The combined behaviour of these factors simultaneously influences the mechanical properties. The random orientation of the fibres affects the thermal properties in different directions. Therefore, the fibres significantly increase the conductivity in the bead direction and other directions.



The thermal conductivity of the carbon fibres helps the already cooled bottom beads soften again after a hot bead is deposited on their upper surfaces, leading to improved packing and smaller gaps. This assertion would explain the smaller gap between the results for hardness and stiffness in the XZ plane for the two infill percentages of 80% and 100%. In the XY direction, the heating of the plate and the lower number of layers reduces the thermal stress, making the effect of the filling more obvious, thereby highlighting a greater difference in hardness between 80% and 100% infills and a lesser difference in the Young's modulus and stress at break. A 20% reduction in the infill percentage (from 100% to 80%) led to greater energy at break in both construction directions.

A comparison of the obtained values with those found in the material datasheets from the supplier and other manufacturers is shown in Table 6. The FFF samples exhibited higher mechanical property values than pure thermoplastic material (nylon) [48,49] but lower mechanical property values than the injection moulded samples [50]. Comparing the values reported for Nylon 12CF [48] with those obtained in this study with the same percentage of filling, it can be observed that the increase in carbon fibres from 20% (nylon-carbon) to 35% (Nylon 12CF) with the same construction orientation allows an increase in the tensile properties. Considering instead a reduction of 5% (CF112) [51] of the percentage of carbon fiber, the mechanical properties are reduced except the elongation at break considering what is declared by the manufacturer. The percentages and type of filling and orientation of the samples are not indicated. The values reported by the Fiber Force manufacturer show a certain difference compared to what was found in this study. The datasheet does not show the data relating to the type of infill used. The other process parameters used are the same as in this study. This therefore focuses on the fact that with the same filament and process parameters, the results determined with a tensile test are also conditioned by the geometry of the tested specimen. The ISO 527-1/-2 and ASTM D638 (used in the scientific literature) standards define test methods for tensile tests. Although technically equivalent, the tests carried out according to these standards do not provide fully comparable results, as the shape of the specimens, the test speed, and the determination of the results are different from each other in several respects [52,53].

**Table 6.** Comparison of the tensile test results.

Manufacturer Data	Young's Modulus E [MPa]	$\sigma_y$ [MPa]	$\sigma_{break}$ [MPa]	Elongation at Break [%]	Energy at Break [J]
Injection moulded–Nylon Carbon	6000	100	-	-	-
Nylon 12CF (Stratasys)	7515 (100%, XZ)	63.4 (100%, XZ)	76 (100%, XZ)	1.9 (100%, XZ)	-
Nylon Carbon (Fiber Force)	1844 (15%, XY)	-	33.7 (15%, XY)	5.7 (15%, XY)	5.45 (15%, XY)
	2758 (100%, XY)		66.3 (100%, XY)	6.7 (100%, XY)	12.2 (100%, XY)
CF112 (Fillamentum)	2200	52.4	37.7	8	-
Nylon (Stratasys)	1282 (100%, XZ)	32 (100%, XZ)	46 (100%, XZ)	3.0 (100%, XZ)	-
Nylon (Fiber Force)	881.9 (15%, XY)	-	20.7 (15%, XY)	13.94 (15%, XY)	10.48 (15%, XY)
	1529.0 (100%, XY)		41.1 (100%, XY)	31.30 (100%, XY)	49.70 (100%, XY)
Nylon (Markforged)	940	54			

### 3.2. Resilience

Figure 5 shows the test results for the specimens built on the XY plane and the XZ plane for each filling ratio. In general, the samples constructed on the XY plane have a resilience that is approximately 4.6 times, 3.1 times, and 2.9 times that of the samples built on the XZ plane with filling factors of 15%, 80%, and 100%, respectively.

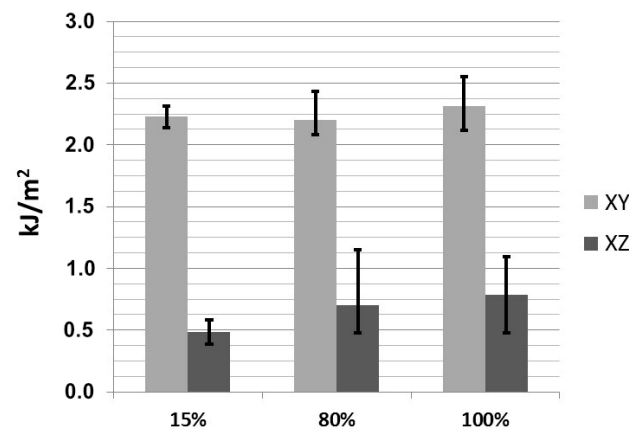


Figure 5. Charpy impact test results.

The filling factor does not have a strong influence on the resilience. The resilience of samples manufactured in the XY plane with a filling percentage of 100% is only 4% higher than the resilience of samples built on the same plane with a filling percentage of 15%. The resilience of samples built on the XZ plane with a filling percentage of 100% is 29% higher than that of samples with a filling percentage of 15%. It is evident that the effect of the building direction is more important than the influence of the filling factor. This finding indicates that if the layers are parallel to the mechanical test direction, the mechanical properties are lower than in the sample where the layers are perpendicular to the mechanical test direction.

Figure 6a shows that the fracture surface of the samples built on the XZ plane corresponds to the interlayer part. During the test, two samples constructed on the XY plane with a filling percentage of 15% were not broken: the last four layers were bent (Figure 6b,c), and the samples passed through the supports. The samples that did not break during the test were not considered in the evaluation of resilience.

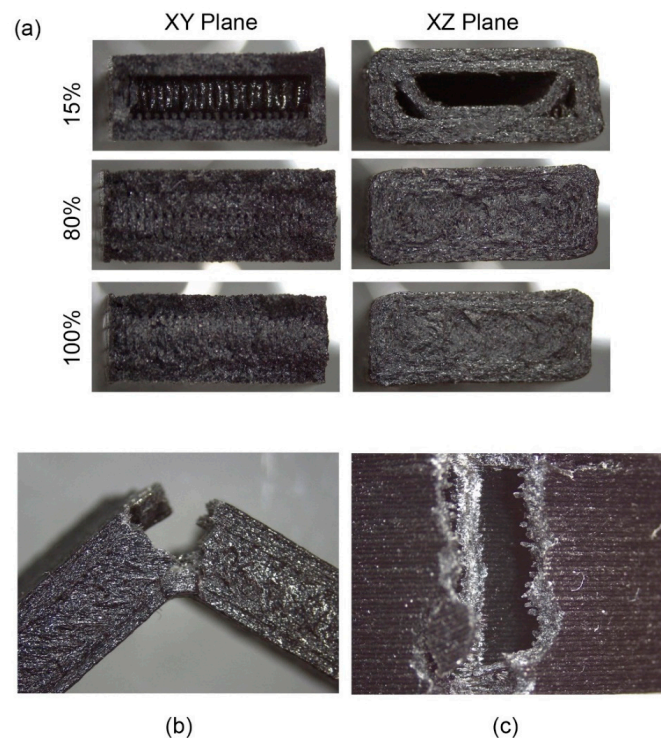


Figure 6. (a) Fracture surfaces from the Charpy impact test samples: (b) side view and (c) top view of the sample built on the XY plane with a filling percentage of 15% that has not been broken.

From the images of the fracture section (Figure 6), it is possible to observe greater compactness between the first and last layer and filling of samples in the XZ plane at 80% and 100% with respect to the XY plane. This may be due to the very principle of the additive process. Additive processes develop in layers. If it considers, for example, the specimen for Charpy tests, the number of layers varies from 20 layers for the XY plane to 50 layers for the one built in the XZ plane. Therefore, considering that the first and last 4 layers are solid, the specimen constructed on the XY plane will have 2.4 mm of infill at 15%, 80% or 100% and 1.6 mm (0.8 mm in the first 4 layers and 0.8 mm in the last 4 layers) of 100% filling; while the one built on the XZ plane will have 8.4 mm of filling at 15%, 80% or 100% and always 1.6 mm of full. Therefore, in the case of hardness and resilience, the components in the XY plane have higher values than those in the XZ plane having a reduced number of layers which reduces the percentage of defects. In the case of tensile test, on the other hand, the specimen has a thin section in the useful area that reverses the condition, i.e., it has more layers but with a reduced filling value, also considering the effects in the contour that decrease the percentage of votes in the transition area between outline and fill. The contours scanned around the part to be filled in every layer limited these porosities. Due to the fact that the specimens were quite thin, the effect of dense contours probably contributes to a higher Young's modulus [54].

#### 4. Conclusions

Although short fibre-reinforced composites offer better mechanical performance than their unreinforced counterparts, there is still a certain gap between the mechanical properties of preimpregnated fibre and conventionally manufactured fibre-reinforced polymer composites. Furthermore, the weight percentage of the carbon fibres and the selected process parameters can greatly influence the mechanical characteristics, as reported in the literature.

Based on the experimental results of this study, the following conclusions may be drawn:

- The samples produced in the XY plane have higher hardness than the samples built in the XZ plane. The samples built in the XZ plane with 80% and 100% filling have similar hardness values. At a filling percentage of 100%, the samples built in the XZ plane exhibit much lower hardness than those constructed in the XY plane.
- The specimens built in the XZ direction are stiffer than those built in the XY direction, in which the former exhibits higher Young's modulus and higher stress at break. In contrast, the energy at break is higher for the samples built in the XY direction. Furthermore, the relationship between the mechanical properties and filling factor is not linear.
- The ISO 527-1/-2 and ASTM D638 standards, although technically equivalent, do not provide fully comparable results
- The filling factor does not have a strong influence on the resilience on the XY plane.

**Author Contributions:** Conceptualization, F.C.; methodology, F.C.; validation, F.C., M.L., and I.R.; formal analysis, F.C., M.L., and I.R.; investigation, F.C., M.L., and I.R.; writing—Original draft preparation, F.C., M.L., I.R., and P.M. All authors have read and agreed to the published version of the manuscript.

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