

Reuse of shale gas flowback and produced water: Effects of coagulation and adsorption on ultrafiltration, reverse osmosis combined process

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1 Reuse of shale gas flowback and produced water:  
2 effects of coagulation and adsorption on  
3 ultrafiltration, reverse osmosis combined process

4 Revised for

5 *Science of the Total Environment*

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18

19

20 **Abstract**

21 The shale gas flowback and produced water (FPW) from hydraulic fracturing in the Sichuan  
22 province of China has relatively low to moderate levels of total dissolved solids (< 20 g/L) and  
23 organics (< 50 mg/L of dissolved organic carbon). As such, a combined ultrafiltration (UF),  
24 reverse osmosis (RO) system can be successfully applied to desalinate this feed water with the  
25 goal of reuse. However, the concentration of influent organic matter and particulates in the UF  
26 and RO stage is high, and the overall ionic and organics composition is highly complex, so that  
27 the membrane processes do not perform well, also due to fouling. To ensure the long-term and  
28 efficient operation of the UF-RO stages, a **combined** pretreatment of the FPW with coagulation  
29 and adsorption was investigated. The effect of different parameters on the performance on the  
30 system was studied in detail. Overall, the coagulation-adsorption pre-treatment greatly reduced  
31 fouling of the membrane processes, thanks to the high removal rate of turbidity (98.8%) and  
32 dissolved organic carbon (80.4%). The adsorption of organic matter by powdered activated  
33 carbon was best described by the Freundlich equilibrium model, with a pseudo second-order  
34 model representing the adsorption kinetics. Also, the various ions had competitive removal rates  
35 during the adsorption step, a phenomenon reported for the first time for FPW treatment. Also, an  
36 optimal dose of activated carbon existed to maximize fouling reduction and effluent quality. The  
37 overall treatment system produced a high-quality water streams, suitable for reuse.

38 **Keywords:** Flowback and produced water, Adsorption, Coagulation, Ultrafiltration, Reverse  
39 osmosis, Water quality

40

41

## 42 **1. Introduction**

43 Shale gas has attracted attention in the energy field as an unconventional natural gas resource  
44 with potentially low carbon footprint and globally abundant reserves (Butkovskyi et al., 2017;  
45 Estrada and Bhamidimarri, 2016; Howarth et al., 2011; Vidic et al., 2013). China has the world's  
46 largest shale gas reserves of 25.08 trillion cubic meters. The Sichuan Basin is China's largest  
47 storage of shale gas and includes the most productive commercial shale gas field (Zhang et al.,  
48 2019; Zou et al., 2018). However, a large amount of **flowback and produced water (FPW)** is  
49 produced during the process of mining shale gas, **ranging from 5,200 to more than 25,000 m<sup>3</sup> for**  
50 **each horizontal well (Chang et al., 2019a; Kondash and Vengosh, 2015; Zou et al., 2018).**

51 The hydraulic fracturing wastewaters are highly variable in their composition, **both spatially and**  
52 **temporally (Barbot et al., 2013; Chang et al., 2019a).** The high concentrations of particulates,  
53 colloids, hardness, salinity, organic matter, and radioactivity (Luek and Gonsior, 2017; Vengosh  
54 et al., 2014; Xiong et al., 2016), **require extensive and non-conventional FPW treatment for its**  
55 **possible reuse or direct discharge (Chang et al., 2017). Compared to the FPW typically generated**  
56 **in basins in the USA (Chang et al., 2019a), the FPW from Sichuan basin is not only estimated to**  
57 **contain a lower level of TDS (6906 – 28,900 mg/L) (Chang et al., 2019a; Chen et al., 2015; Guo**  
58 **et al., 2018; Huang et al., 2016), but it is also characterized by a lower amount of organic matter**  
59 **(total organic carbon (TOC) is approximately 78 mg/L) (Kong et al., 2017).** There are other  
60 important differences for the FPW from different regions, such as the types and mixture of ions,  
61 organic matters, and the presence of radioactive materials. **The FPW has** the potential to  
62 contaminate groundwater, soil, and air, posing great risks to human and ecosystem health in the  
63 case of improper management (Annevelink et al., 2016; Howarth et al., 2011; Shaffer et al.,

64 2013; Stoll et al., 2015). Therefore, for the Sichuan basin, China's shale gas mining areas, and  
65 the world at large, it is extremely urgent to create a process to manage a plethora of FPWs  
66 having each their own specific characteristics.

67 External reuse is a promising wastewater management approach for shale gas FPW  
68 (Butkovskiy et al., 2017; Chang et al., 2019a; Guo et al., 2018; Harkness et al., 2015). China, as  
69 well as the rest of the world, still lacks efficient processing technologies and rational systems for  
70 reuse of these streams in irrigation or for recycling in additional fracking operations. Reliable  
71 research on FPW reclamation is arguably the primary task of shale gas exploration at this stage.  
72 Membrane-based processes are certainly promising techniques for FPW recycling due to their  
73 high efficiency and excellent permeate quality (Chang et al., 2019a; Estrada and Bhamidimarri,  
74 2016; Shaffer et al., 2013), including microfiltration, ultrafiltration, nanofiltration, forward  
75 osmosis (FO), reverse osmosis (RO), or their combination. Among them, reverse osmosis is  
76 regarded as the most energy-saving and promising water desalination technology (Elimelech and  
77 Phillip, 2011). However, membrane fouling is still one of the critical difficulties in the  
78 implementation of membrane filtration processes (Chang et al., 2019a). Numerous studies have  
79 been conducted to control or reduce membrane fouling, including optimization of operational  
80 parameters and application of effective pretreatment (Amin Reyhania, 2015).

81 Coagulation is a relatively simple physical-chemical technique to treat FPW, reducing  
82 organics and thus alleviating membrane fouling. Rosenblum et al. confirmed that coagulation  
83 could remove 80% of total petroleum hydrocarbons and 90% of turbidity (Rosenblum et al.,  
84 2016). In a previous study, 33.6-62.0% and 33.6-42.6% of COD was removed by addition of  
85 aluminum sulfate or ferric chloride, respectively, and 64% and 84% of UF fouling was decreased  
86 by these coagulants under optimal dosage (Chang et al., 2019b). However, the use of coagulants

87 results in an increase in the concentration of aluminum or iron in the effluent water. Adsorption  
88 may be thus applied to further polish this stream before further treatment based on membranes.  
89 Activated carbon is an excellent adsorbent which remains widely used, mainly due to its high  
90 adsorption capacity, adsorption speed, good mechanical stability (Liu et al., 2012), although the  
91 effect of powdered activated carbon (PAC) on membrane fouling is still debated (Shao et al.,  
92 2017; Wang et al., 2016). Additionally, the PAC regeneration process and the post-treatment of  
93 the adsorbed substances may also increase the operational cost. When treating FPW, PAC  
94 achieved greater than 80% reductions of the total ion chromatogram, while dissolved organic  
95 carbon (DOC) removals were between 9.5 and 48.3% (Rosenblum et al., 2016). The combined  
96 process of coagulation and adsorption can greatly reduce the dissolved organics, turbidity, and  
97 ion concentrations (Rosenblum et al., 2016), while also reducing the consumption of activated  
98 carbon. However, little research has been performed on such combined process, and specifically  
99 on its role to optimize membrane filtration processes in the treatment of FPW.

100 The objective of this study is to evaluate the feasibility of a hybrid coagulation-adsorption-  
101 UF-RO system in assisting FPW reuse in Weiyuan shale gas operation. The performance of the  
102 system, the influence of coagulation and activated carbon on membrane performance and their  
103 effects in the removal of dissolved organics are systematically investigated. The results of this  
104 study allow the evaluation of coagulation-adsorption to alleviate membrane fouling and the  
105 applicability of this process for the treatment of FPW. Another objective of the study is to  
106 provide a better understanding of UF and RO fouling from FPW and discuss solutions that  
107 enable the use of membrane filtration in the recycling of wastewater produced during shale gas  
108 exploration.

109

110 **2. Materials and methods**

111 **2.1 Shale gas FPW samples**

112 The flowback and produced water sample utilized in this study was collected from a well site of  
113 the Weiyuan shale gas field located in the Sichuan province of China. The site includes 6  
114 horizontal wells that were hydraulically fractured on a single pad using similar fracturing fluid.  
115 Wastewater from previously completed wells and fresh water were mixed and stored in a storage  
116 pool. The stock samples were packed at the pool into plastic cylindrical containers and then  
117 transported to the lab. Its characteristics are summarized in Table 1. The containers were sealed  
118 and stored in a dark place to minimize variation of their characteristics in time.

119

120 **Table 1.** Quality of the influent water and of the effluents from each treatment step of the hybrid  
 121 system investigated in this study<sup>a</sup>

Constituent	FPW in Weiyuan	Coagulation	PAC <sup>b</sup> Adsorption	UF membrane permeate	RO membrane permeate
Turbidity (NTU)	187	15.8	2.1	0.08	0.07
UV <sub>254</sub> (1/cm)	0.137	0.077	0.015	0.016	0.003
TDS (mg/L)	16320	15715	15930	15410	224
Conductivity (mS/cm)	26.79	26.29	26.20	25.85	0.52
DOC (mg/L)	38.03	13.61	5.21	5.19	1.71
SUVA (L mg <sup>-1</sup> m <sup>-1</sup> )	0.36	0.46	0.21	0.22	0.17
pH	7.48	6.93	7.31	7.51	6.65
Na <sup>+</sup> (mg/L)	6151	6065	5920	5931	105
Ca <sup>2+</sup> (mg/L)	274.7	257.9	201.2	200.9	1.1
Mg <sup>2+</sup> (mg/L)	36.5	34.8	26.5	26.4	-
K <sup>+</sup> (mg/L)	255.1	246.2	175.7	173.3	2.5
Sr <sup>2+</sup> (mg/L)	66.3	57.3	28.9	28.4	-
Ba <sup>2+</sup> (mg/L)	94.4	90.2	63.9	61.3	-
NH <sub>4</sub> <sup>+</sup> (mg/L)	60.4	60.2	50.1	50.3	1.3
Cl <sup>-</sup> (mg/L)	9412	9275	9158	9133	149
NO <sub>2</sub> <sup>-</sup> (mg/L)	35.7	31.0	28.5	28.5	1.3
F <sup>-</sup> (mg/L)	12.6	11.5	9.4	9.3	0.2
Br <sup>-</sup> (mg/L)	97.9	94.2	89.8	89.8	1.7
NO <sub>3</sub> <sup>-</sup> (mg/L)	161.9	151.9	139.9	138.8	1.2

122 <sup>a</sup> The data in the table is the average of three replicate experimental data.

123 <sup>b</sup> Adsorption experiment at optimal dose of 300 mg/L of WP260.

124



125

## 126 2.2 Chemicals and materials

127 Aluminum sulfate octadeca hydrate ( $\text{Al}_2(\text{SO}_4)_3 \cdot 18\text{H}_2\text{O}$ ; Sigma Aldrich, analytical grade) was  
128 used as a coagulant. The reagents for chemical oxygen demand (COD) analysis were purchased  
129 from Lianhua Tech Co., Ltd. (Lanzhou, China). Concentrated sulfuric acid was obtained from  
130 Kelong Chemical (Chengdu, China). Three types of powdered activated carbon (WP260,  
131 PAC70X, DCL320) were purchased from Calgon Carbon Corporation (Moon Township, PA,  
132 USA). The detailed characteristics of the activated carbon samples are listed in Table 2. The size  
133 distributions of these adsorbents are shown in Fig. S2 of the Supporting Information.

134 **Table 2.** Characteristics of three different activated carbon products investigated in this study

Product name	Specific surface area ( $\text{m}^2/\text{g}$ )	Total pore volume ( $\text{cm}^3/\text{g}$ )	Avg pore diameter (nm)	Moisture wt%	Ash wt%	US mesh (<325) wt%	Iodine No. (mg/g)
WP260	1392	1.05	3.01	6	14	72	1023
PAC70X	882	0.44	1.99	5	15	84	732
DCL320	933	0.54	2.31	7	-	80	-

135

136 A polyvinylidene fluoride (PVDF) hollow fiber membrane (Litree Purifying Technology Co.,  
137 Ltd., Haikou, China) was employed for the UF treatment. This membrane (pore size in the range  
138 of 11.3-28.8 nm) had a molecular weight cut-off (MWCO) of 100 kDa, and the outside diameter  
139 of the fiber was 1.8 mm. In each UF test, a single fiber with a length of 20 cm was used, and the  
140 effective surface area was  $11.3 \text{ cm}^2$ . The SW21 from Vontron Membrane Technology Co., Ltd.

141 (Guiyang, China) was selected as RO membrane. The effective area of each RO membrane  
142 coupon was 14.6 cm<sup>2</sup>.

### 143 **2.3 Analytical methods**

144 The temperature and pH were measured using a mercury thermometer and a pH meter,  
145 respectively (PB-10, Sartorius Scientific Instruments Co., Ltd., Beijing, China). The turbidity  
146 was determined with a Hach TL2310 (Hach, Loveland, CO, USA) turbidimeter. An Ultrameter II  
147 6PFC (Myron L, Carlsbad, California, USA) portable multi-function instrument was adopted to  
148 determine the TDS and conductivity. The fast digestion-spectrophotometric method was utilized  
149 to measure the COD using a 5B-1F(V8) fast digestion instrument (Lianhua Environmental  
150 Protection Technology Co., Ltd., Lanzhou, China). UV absorbance at 254 nm was measured by  
151 UV-Vis spectrophotometry (Orion AquaMate 8000, Thermo Fisher Scientific Inc., MA, USA).  
152 The dissolved organic carbon (DOC) content was measured using a TOC analyzer L series  
153 (Shimadzu, Kyoto, Japan). SUVA<sub>254</sub> (L/mg·m), an indicator of aromatic dissolved organic  
154 matter, was defined as UV<sub>254</sub> absorbance divided by DOC concentration. The quantification of  
155 the concentrations of Cl<sup>-</sup>, Br<sup>-</sup>, F<sup>-</sup>, NO<sub>2</sub><sup>-</sup>, NO<sub>3</sub><sup>-</sup>, Na<sup>+</sup>, K<sup>+</sup>, NH<sub>4</sub><sup>+</sup>, Ca<sup>2+</sup>, Mg<sup>2+</sup>, Ba<sup>2+</sup>, Sr<sup>2+</sup> was  
156 performed using a Dionex ICS-1100 ion chromatographer (Thermo Fisher Scientific Inc., MA,  
157 USA). The techniques of scanning electron microscopy (SEM) and energy dispersive  
158 spectroscopy (EDS) (Regulus 8230, HITACHI, Tokyo, Japan) were used to investigate the  
159 morphology and elemental ratio of the membrane surface and fouling layers. Before SEM-EDS  
160 analysis, the membranes were coated with 2 nm of gold using a magnetron sputter (MSP-2S,  
161 IXRF Systems, USA). The Brunauer-Emmett-Teller (BET) specific surface areas and porosity  
162 were determined by means of nitrogen-sorption isotherms with a NOVA 2200e analyzer  
163 (Quantachrome, USA).

## 164 **2.4 Experimental procedures**

### 165 ***2.4.1 Treatment protocols***

166 The overall design of the proposed system (Fig. S1) is as follows: coagulation, activated carbon  
167 adsorption, ultrafiltration, and finally reverse osmosis. Unless otherwise specified, the  
168 operational temperature was  $293 \pm 1$  K for all the experiments. In the jar coagulation tests,  
169 aluminum sulfate was chosen as flocculant and the optimum dose was 600 mg/L according to  
170 our previous work.(Chang et al., 2019b) Experiments were conducted with the ZR4-6 jar-test  
171 equipment (Zhongrun Water Industry Technology Development Co., Ltd., Shenzhen, China).  
172 After adding the coagulant to a raw water sample, the experimental procedure consisted of two  
173 subsequent stages: a rapid mixing stage at 200 rpm for 1 min followed by slow mixing at 40 rpm  
174 for 20 min. The stirring was then stopped, and the mixture was allowed to settle for 30 min.  
175 Finally, the supernatant was removed from the beaker for analysis and subsequent experiments.  
176 For adsorption experiments, the three types of PAC were rinsed with ultrapure water to remove  
177 undesired surface compounds and dried at 377 K for 24 h. The raw water or the samples obtained  
178 from coagulation tests were treated by adsorption with the addition of PAC in the jar-test  
179 equipment mentioned above, while stirring at 80 rpm for different time intervals in the range 15-  
180 120 min. A series of PAC dosages (50, 150, 300, 800, and 1200 mg/L) were tested.

181 New UF and RO membranes were soaked in ultrapure water for at least 48 h and the water  
182 was replaced at least three times. A new membrane was used for each UF run and a filtration  
183 with ultrapure water for 1 h was performed to obtain a stable water flux. Then, multi-cycle UF  
184 tests with periodic hydraulic backwash were executed at a constant flux equal to  $50 \text{ L m}^{-2}\text{h}^{-1}$   
185 (LMH). The duration of each filtration and backwash step was 54 min and 3.5 min, respectively,  
186 for each cycle. The transmembrane pressure (TMP) was measured using a pressure sensor (Unik

187 5000, General Electric Company, USA) in constant flux mode, which was controlled  
188 continuously with a pressure gauge (1379 Duragauge, Ashcroft Inc., USA) connected to the  
189 peristaltic pump. The permeate solution tank rested on an electronic balance (Adventurer Pro  
190 CAV8101, Shanghai, China) and weight changes were recorded over time to determine the  
191 permeate flux.

192 The RO unit was operated using a dead-end stirred cell (HP 4750, Sterlitech Corp., Kent,  
193 WA, USA). These tests were carried out at the constant transmembrane pressure of 5.5 MPa (55  
194 bar). The solution in the filtration cell was kept under stirring at 200 rpm. The initial feed volume  
195 in the RO cell was 300 mL and the filtration was continued until a recovery rate of 50% was  
196 achieved (150 mL of permeate solution was collected).

#### 197 **2.4.2 Analyses and calculations**

198 Following adsorption, the DOC content of the supernatant solution was measured. The uptake of  
199 adsorbate by PAC,  $q_e$  (mg DOC/g), was calculated according to the following  
200 equation(Sontheimer et al., 1988):

$$201 \quad q_e = \frac{V(C_0 - C_e)}{m} \quad (1)$$

202 where  $q_e$  is the equilibrium adsorbent-phase concentration of adsorbate (mg adsorbate/g  
203 adsorbent),  $C_0$  and  $C_e$  are the initial and equilibrium liquid phase concentrations of the organic  
204 adsorbates (mg DOC/L), respectively,  $V$  is volume of the solution (L), and  $m$  is the weight of the  
205 PAC (g) adsorbent. Freundlich, Langmuir, and Temkin isotherm models were assessed to  
206 describe the mechanism of phase partitioning. The Freundlich isotherm model can be expressed  
207 by Eq. (2):(Cheng et al., 2015)

208 
$$q_e = K_F C_e^{\frac{1}{n}} \quad (2)$$

209 Eq. (2) can also be expressed in the linearized logarithmic form:

210 
$$\log(q_e) = \log(K_F) + \frac{1}{n} \log(C_e) \quad (3)$$

211 where  $K_F$  is the Freundlich adsorption capacity parameter, and  $1/n$  is the dimensionless  
212 Freundlich adsorption intensity parameter. The intercept and slope of the line in equation 3  
213 enable the determination of the isotherm constants. Langmuir isotherm model is expressed  
214 as:(Manz et al., 2016)

215 
$$q_e = \frac{Q_M K_L C_e}{1 + K_L C_e} \quad (4)$$

216 The linear equation of Eq. (4) is expressed as:

217 
$$\frac{C_e}{q_e} = \frac{C_e}{Q_M} + \frac{1}{K_L Q_M} \quad (5)$$

218 where  $K_L$  is the Langmuir adsorption constant, and  $Q_M$  is the maximum adsorbent phase when  
219 the adsorbent is saturated. The Temkin isotherm model contains a factor that explicitly takes into  
220 account the adsorbate-adsorbent interactions. This model assumes the following: (i) the heat of  
221 adsorption of all the molecules in the layer decreases linearly with coverage due to adsorbent-  
222 adsorbate interactions, and (ii) the adsorption is characterized by a uniform distribution of  
223 binding energies, up to a maximum binding energy(Angin, 2014). The Temkin isotherm model is  
224 presented in the following form:

225 
$$q_e = B \ln(K_T \cdot C_e) \quad (6)$$

226 Eq. (6) can be written in the linear form:

$$227 \quad q_e = B \ln(K_T) + B \ln(C_e) \quad (7)$$

228 where  $B$  is the Temkin constant related to gas constant, heat of sorption, and absolute  
229 temperature,  $K_T$  is the equilibrium binding constant (L/mg). The adsorption coefficients can be  
230 computed by plotting  $q_e$  values vs.  $\ln C_e$ .

231 In order to describe the speed of the adsorption process, pseudo first-order and pseudo second-  
232 order kinetic models were selected to assess the experimental data. The models were expressed  
233 with the following equations:(Cheng et al., 2015)

$$234 \quad \log(q_e - q_t) = \log q_e - \frac{k_1 t}{2.303} \quad (8)$$

$$235 \quad \frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{t}{q_e} \quad (9)$$

236 where  $q_e$  and  $q_t$  (mg/g) are the adsorbent capacities at equilibrium and at time  $t$  (h), respectively;  
237  $k_1$  ( $\text{h}^{-1}$ ) and  $k_2$  ( $\text{g}/(\text{mg}\cdot\text{h})$ ) are the pseudo first-order and pseudo second-order rate constants,  
238 respectively.

239 The total fouling index (TFI) was used to quantify the UF membrane fouling of different  
240 operational cycles and cleaning steps (Chang et al., 2016; Nguyen et al., 2011). **The derivation**  
241 **process for the TFI parameter is provided in the SI. And** the TFI was calculated by equation (10):

$$242 \quad (TFI)V_s = \frac{TMP_f}{TMP_0} - 1 \quad (10)$$

243 where  $V_s$  (L/m<sup>2</sup>) is the volume of filtered water per unit membrane area; the TMP at the  
244 beginning and end of the filtration is represented by TMP<sub>0</sub> and TMP<sub>f</sub> (kPa), respectively. This  
245 index was calculated by the least square linear regression approach.

### 246 **3. Results and discussion**

#### 247 **3.1 Adsorption processes**

##### 248 **3.1.1 Adsorption isotherms**

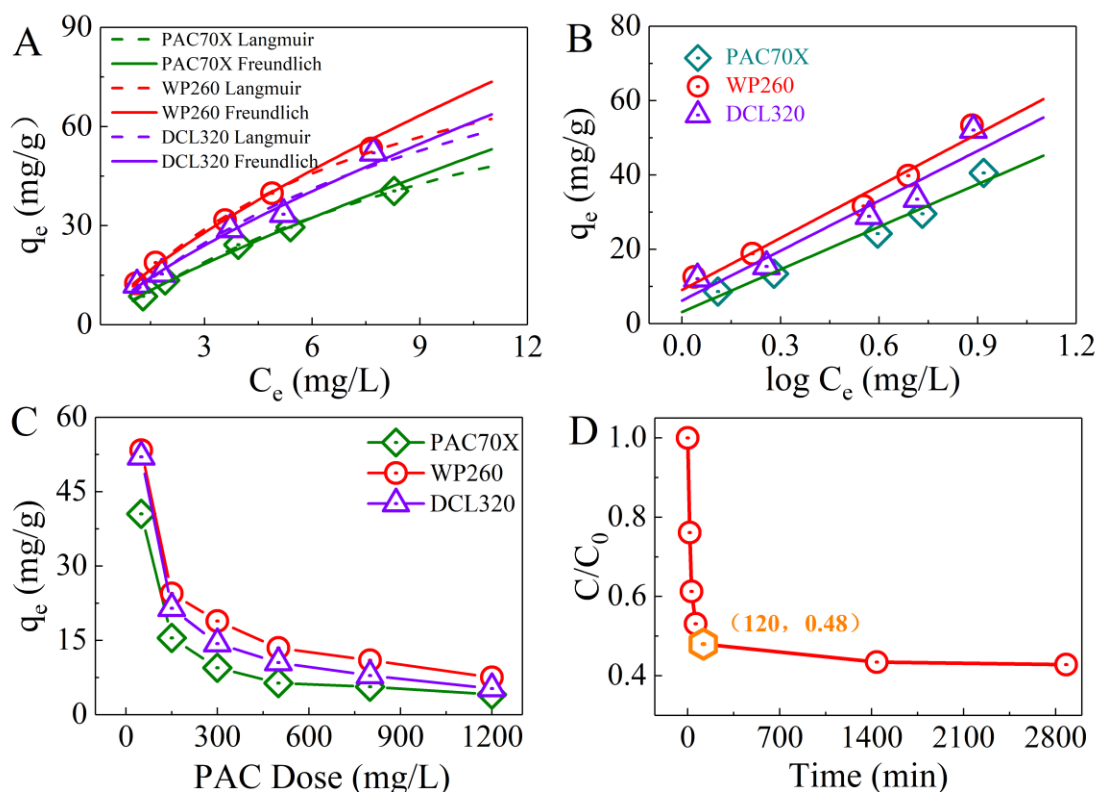
249 Fig. 1A-B depicts the isotherms for the adsorption of DOC onto PAC70X, WP260, and DCL320  
250 adsorbents. To evaluate the maximum adsorption capacities of three types of PAC toward DOC,  
251 the adsorption isotherms were obtained with the pH fixed at 7.5. The regression Freundlich,  
252 Langmuir, and Temkin constants are presented in Table 3. The Freundlich isotherm equation  
253 appears to be the most suitable one to describe the organic matter adsorption on PAC, yielding  
254 R<sup>2</sup> values above 0.995. In the Freundlich model, there exists a distribution of sites with different  
255 adsorption energies and more than one layer of adsorbates can adsorb onto the PAC. The value  
256 of  $n$  is between 1 and 5, indicating that all three activated carbons favorably adsorb organic  
257 matter from FPW. The value of  $1/n$  for WP260 is the smallest, confirming that this material is  
258 the most adequate one among the three options. In addition, a value below unity implies  
259 chemisorption process (Foo and Hameed, 2010). Fig. 1C shows the results of adsorption  
260 equilibria tests at 293 K. The value of  $q_e$  decreased sharply at low PAC content and approached  
261 very small values close to zero for a dose larger than roughly 300 mg/L, even though not the  
262 entire amount of DOC was removed from the liquid phase (see Table 1). This result is indicative  
263 of the fact that the active sites of the adsorbents were not fully utilized and that the limiting  
264 factor was not the dose or the type of PAC, but possibly the nature of the DOC in the system, a  
265 fraction of which did not follow an equilibrium-driven partitioning with the adsorbent phase.

266 Among the various PACs, WP260 possessed the highest organics adsorption efficiency,  
267 consistent with adsorption isotherms. Therefore, WP260 was selected for the hybrid system with  
268 the most appropriate dose of 300 mg/L.

### 269 **3.1.2 Adsorption kinetics**

270 Fig. 1D shows the adsorption kinetics of DOC onto WP260. The adsorption was relatively fast  
271 within the first two hours, reaching a relative DOC value of 0.48, while it slowed down  
272 significantly after this time. The rapid initial adsorption regime may be attributed to the high  
273 concentration gradient between the adsorbate in solution and that on the solid phase, as well as to  
274 the high number of sites available for adsorption. Later during treatment, the adsorption becomes  
275 diffusion-controlled and other phenomena, such as the aggregation of DOC molecules, may  
276 reduce the kinetics of adsorption (Crittenden et al., 2012). Also, the affinity with PAC of DOC  
277 fractions may be lower for organic molecules that are still in suspension at later stages of the  
278 adsorption treatment. The experimental data were simulated using pseudo first-order and pseudo  
279 second-order models to examine the controlling mechanism of PAC adsorption, e.g., physical  
280 adsorption, mass transfer, and chemical reaction. As shown in Fig. S3 and Table S1 of the  
281 Supporting Information, the adsorption kinetics of DOC on WP260 may be simulated well by a  
282 pseudo-second-order kinetics model (correlation coefficients,  $R^2 > 0.997$ ). The equilibrium  
283 concentration of DOC predicted by the pseudo second-order model agrees well with the  
284 experimental data, suggesting chemisorption as the rate-controlling step for the DOC adsorption  
285 onto WP260, consistent with what discussed above.





286

287 **Fig. 1.** Adsorption equilibria, kinetics, and models. (A) Adsorption isotherms of DOC adsorbing  
 288 from the coagulated FPW on different PACs (dose of 50 mg/L and total adsorption time of 48 h)  
 289 and best fittings with Freundlich and Langmuir models. (B) Adsorption isotherms of DOC  
 290 adsorbing from the coagulated FPW on different PACs (dose of 50 mg/L and total adsorption  
 291 time of 48 h) and best fittings with Temkin model. (C) Comparison of adsorption equilibria of  
 292 DOC from the coagulated FPW on different PACs for a total adsorption time of 48 h. (D)  
 293 Kinetics of adsorption of DOC from the coagulated FPW, with a dose of WP360 of 300 mg/L.  
 294 All the experiments were performed at pH 7.5 and at a temperature of 293 K.

295

296 **Table 3.** Isotherm fitting parameters for the adsorption of DOC from raw FPW onto WP260,  
 297 DCL320, and PAC70X powdered activated carbon

Specifications	Freundlich			Langmuir			Temkin		
	1/n	K <sub>F</sub>	R <sup>2</sup>	Q <sub>M</sub>	K <sub>L</sub>	R <sup>2</sup>	B	K <sub>T</sub>	R <sup>2</sup>
WP260	0.73	12.43	0.995	109.89	0.12	0.981	46.66	1.57	0.977
PAC320	0.75	10.54	0.987	120.48	0.09	0.758	44.75	1.38	0.913
DCL70X	0.82	7.51	0.992	112.36	0.070	0.960	38.23	1.21	0.981

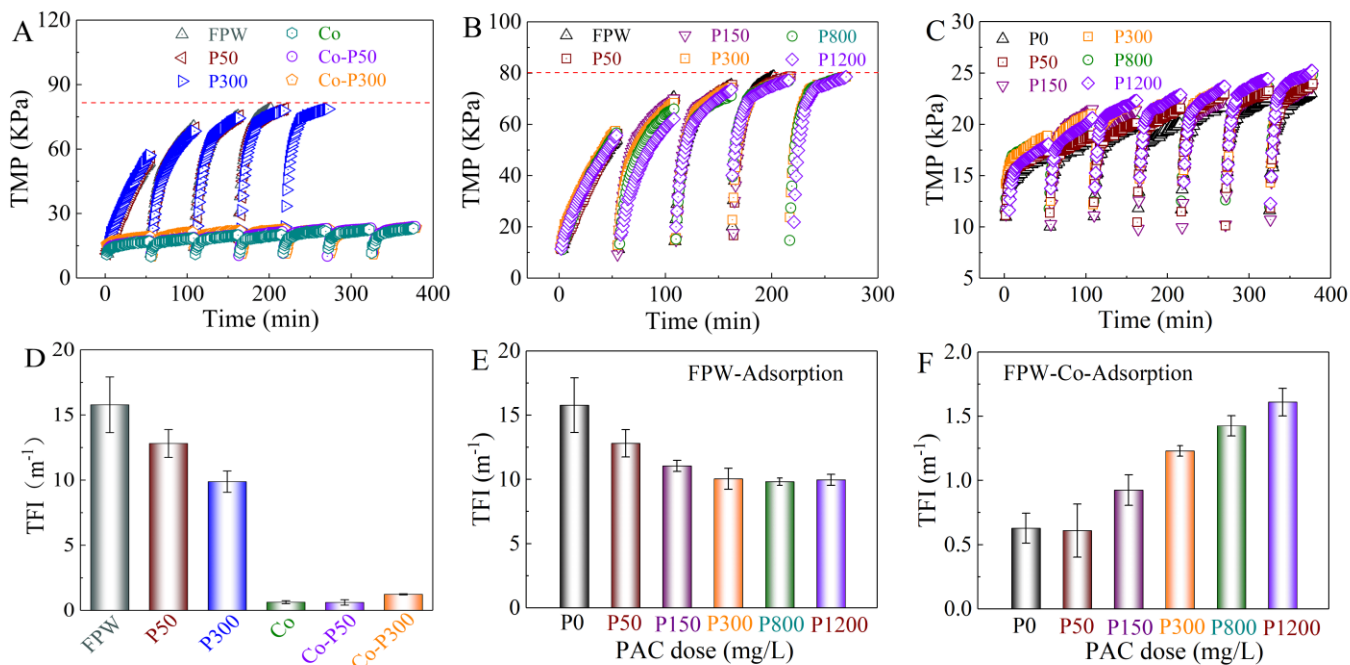
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### 299 **3.2 Effect of pretreatment on fouling in ultrafiltration**

300 Various effluents were fed to the UF system to evaluate their fouling propensity, thus the  
301 efficacy of feed pre-treatment. **In particular, different combinations of pre-treatment processes**  
302 **were assessed, including coagulation alone, PAC adsorption alone, and a sequence of the above,**  
303 **i.e., coagulation followed by adsorption.** The transmembrane pressure of the UF system during  
304 the constant-flux treatment of FPW was monitored over time as an indication of membrane  
305 fouling and is shown in Figure 2A-C. The same initial flux of 50 L m<sup>-2</sup>h<sup>-1</sup> was applied to all  
306 experiments. Obviously, as the operating time increased, TMP also increased because of fouling.  
307 The periodic hydraulic backwashing resulted in the discontinuous cycles shown in Figure 2. The  
308 TMP was maintained lower than 80 kPa, as above this value the UF performance can deteriorate  
309 (Jarzyńska and Pietruszka, 2011). As shown in Fig. 2A, the TMP increased significantly and  
310 rapidly while treating FPWs that had not undergone previous coagulation, suggesting that  
311 coagulation using aluminum coagulant can effectively reduce UF membrane fouling, which is in  
312 accordance with our previous research (Chang et al., 2019b). The growth rate of the measured  
313 TMP was also slowed down during the treatment of raw water filtered with a 0.45 μm pore-size  
314 filter (Fig. S4): the TFI was reduced by 49.4% compared to the TFI when the raw water was  
315 directly fed to the UF system. This result indicates that some large particulates and matter (>0.45

316  $\mu\text{m}$ ) can also increase the fouling of the UF membrane. Overall, the fouling rate decreased with  
317 the following order of feed water: raw FPW, FPW subject to adsorption only, FPW subject to  
318 microfiltration only, FPW subject to filtration and then adsorption, FPW subject to coagulation  
319 and then adsorption (Fig. 2D).

320       When the raw FPW was only pre-treated by PAC, the UF membrane fouling decreased with  
321 an increase in PAC dosage of 0-300 mg/L, as shown in Fig. 2B and E. Above the dosage of 300  
322 mg/L, comparable UF fouling was observed up to 1,200 mg/L.. On the contrary, the opposite  
323 effect with PAC dose was observed for FPWs that were first treated by coagulation (Fig. 2C, F).  
324 There, fouling effects were significantly less critical than those observed for feed waters that  
325 were only treated by adsorption without prior coagulation. However, the TMP increased slightly  
326 with the increase in PAC dose. Indeed, as the PAC dose increased from 0 to 1200 mg/L, the TFI  
327 increased from 0.63 to 1.61 (Fig. 2F). This observation may be rationalized as PAC particles and  
328 gels accumulated on the surface to contribute in the formation of the fouling layer, as others have  
329 previously reported (Cheng-Fang Lin 1999; Zhang et al., 2003 ). Therefore, while the  
330 coagulation treatment helps remarkably in fouling reduction, the PAC should not be overdosed in  
331 the following adsorption step. Coagulation removed particles and colloids in suspension (Kong  
332 et al., 2017), preventing the formation of large settleable flocs with PAC. As such, PAC  
333 remained in suspension and could foul the UF membrane, actually representing the dominant  
334 factor in membrane fouling under these conditions.

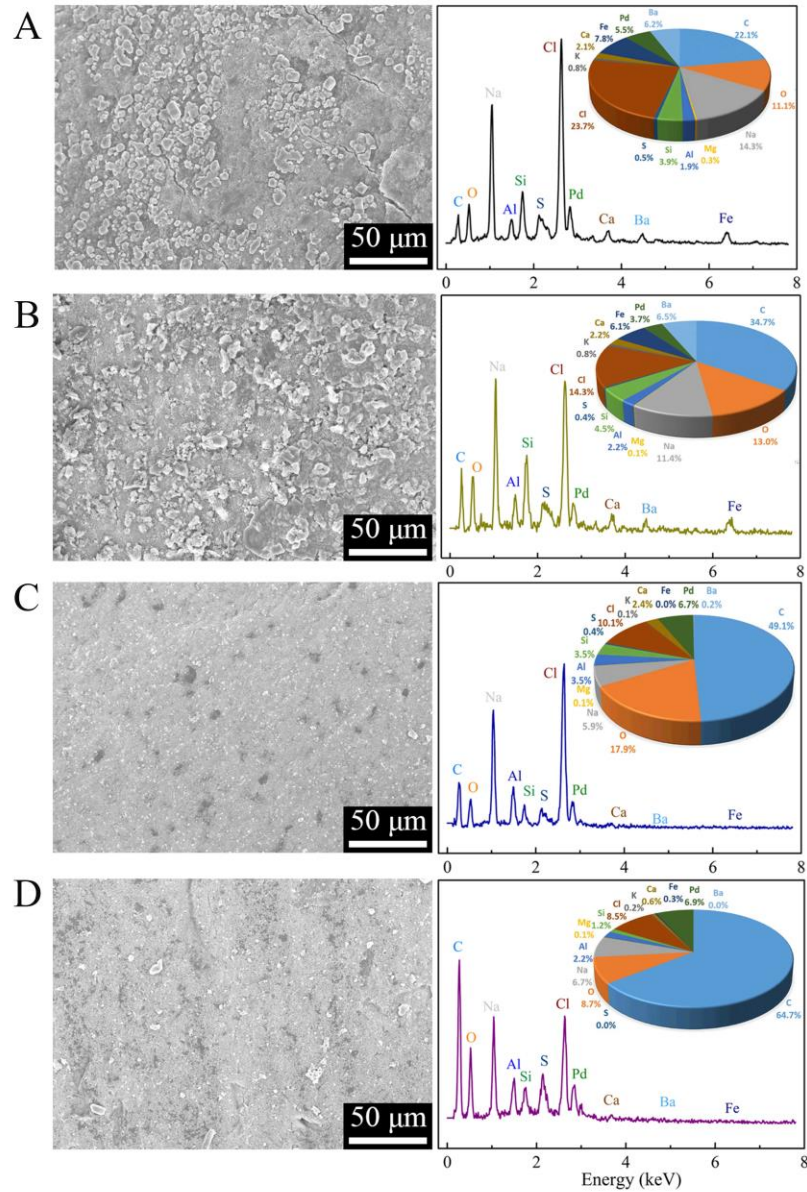


335  
 336 **Fig. 2.** UF membrane fouling expressed as transmembrane pressure (TMP) and total fouling  
 337 index (TFI). (A, B, C) TMP as a function of time and (D, E, F) TFI when the UF system was  
 338 applied to treat (A, D) effluents from different pre-treatment processes, (B, E) effluents treated  
 339 by PAC adsorption without prior coagulation for different doses of WP260, and (C, F) effluents  
 340 treated by coagulation followed by PAC adsorption for different doses of WP260. The labels  
 341 indicate the following: “FPW” for raw influent water, “Co” for coagulation only, “P” for  
 342 adsorption. The numbers in the labels refer to different PAC doses.

343  
 344 The FPW chemistry and fouling agents constantly change the membrane surface properties  
 345 and membrane-foulant interactions during fouling (Bellona et al., 2004). To improve the  
 346 understanding of UF performance with FPW, the fouled membranes and fouling layers were  
 347 characterized. SEM-EDS analyses confirmed that the UF membrane surface was covered with a  
 348 dense foulant layer following filtration of the raw FPW (Fig. 3A) or of FPW treated with

349 coagulation only (Fig. 3B). Specifically, the raw FPW created a thick and dense layer, consistent  
350 with the results presented by Chang et al.(Chang et al., 2019b) By contrast, when coagulated-  
351 adsorption water was treated in ultrafiltration (Fig. 3C, 3D), a thinner foulant layer covered the  
352 membrane surface and not its entirety was covered by foulants. Also, irregular particles appeared  
353 on the surface of the UF membrane when the adsorbent dose was 1200 mg/L compared to the  
354 adsorbent dose of 300 mg/L, suggesting the presence of PAC particles for high doses. This  
355 hypothesis is corroborated the relative content of carbon on the sample shown 4D (64.7%) was  
356 significantly higher than on that relative to 4C (49.1%). In general, the EDS analysis showed a  
357 large content of elements Cl, Na, C, and O, as well as high concentrations of Si, Ca, Mg, Al, S,  
358 Fe, Sr, and Ba on the fouled UF membrane surface, compared with the new PVDF membrane  
359 (Tab. S2). Although almost the same elements were detected on the surface of all the fouled  
360 membranes, the relative amounts of the various elements differed. The relative weight  
361 percentage of elements Mg, Ca, Fe, Ba decreased with the increase of WP260 dose, suggesting a  
362 larger removal for higher PAC concentrations during adsorption. Remarkably, almost no Ca, Ba,  
363 or Fe were detected on the surface of the UF membrane following treatment of water pretreated  
364 by both coagulation and adsorption (Fig. 3C, 3D). Comparing Fig. 2 and Fig. 3, the TFI values of  
365 the UF membrane were almost unchanged when fed with coagulation-adsorption treated water or  
366 only coagulation-treated water (Fig. 2), but the nature of the foulants on the surface of these  
367 membranes, provided by EDS analyses, is significantly different (Fig. 3). The results obtained in  
368 this study were similar to those found in the published literature (Chang et al., 2015; Remize et  
369 al., 2010). Although the total permeability could be almost completely restored, only part of the  
370 foulants were removed from the membrane, with a certain amount of foulants still deposited on  
371 the membrane surface.. In summary, the results presented in Fig. 3 and Fig. S5 of the Supporting

372 Information imply that coagulation combined with activated carbon adsorption has the potential  
 373 to greatly reduce fouling, in turn improving the membrane performance.



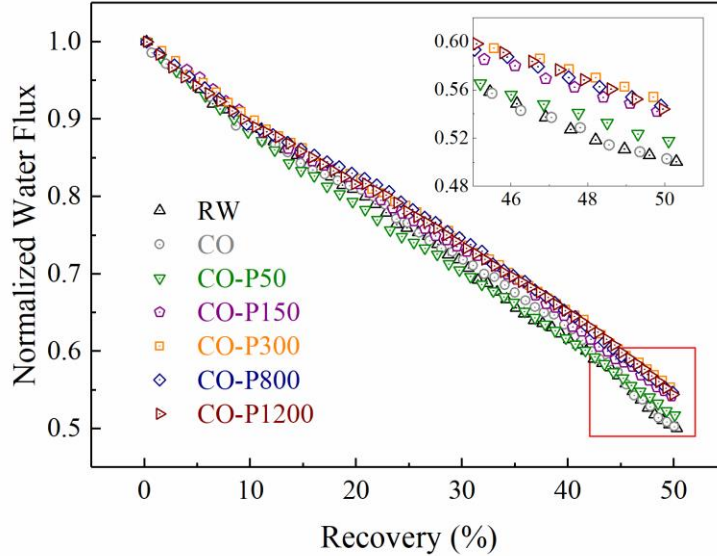
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375 **Fig. 3.** SEM-EDS analyses of the UF membrane surface after fouling following the filtration of  
 376 effluents that had been treated with different pre-treatment processes. UF filtration of the (A) raw  
 377 FPW; (B) effluent from coagulation; (C) effluent from coagulation and adsorption at the WP260

378 dose of 300 mg/L, and (D) effluent from coagulation and adsorption at the WP260 dose of 1200  
379 mg/L. All the experiments performed at constant flux of 50 LMH and temperature of 293 K.

### 380 **3.3 Effect of pretreatment on fouling in reverse osmosis**

381 The normalized water flux decline with different feed solutions of the RO process operating up  
382 to 50% recovery is presented in Fig. 4. The permeate flux decreased with increasing recovery,  
383 which is mainly due to the increase in the osmotic pressure of the retentate. In general, the  
384 measured flux across the membrane was higher for larger PAC doses applied in the adsorption  
385 pre-treatment. This effect was observed up to a PAC dose of 300 mg/L, above which the RO flux  
386 was not function of the adsorption conditions. Specifically, adsorption pre-treatment performed  
387 with 300 mg/L of WP260 reduced the fouling in RO and increased flux by 10.8%. **This was**  
388 **mainly due to the difference in the influent water quality of the RO. In terms of organic matter**  
389 **(DOC, UV<sub>254</sub>) and turbidity, PAC at a dosage of 300 mg/L could ensure that the influent water**  
390 **quality of the RO had basically the lowest concentration of pollutants, as discussed in detail in**  
391 **Section 3.4.** In addition, the positive effect of adsorption is expected to be even more pronounced  
392 for longer operating time and if cross-flow filtration is used instead of dead-end mode (Quay et  
393 al., 2018).



394

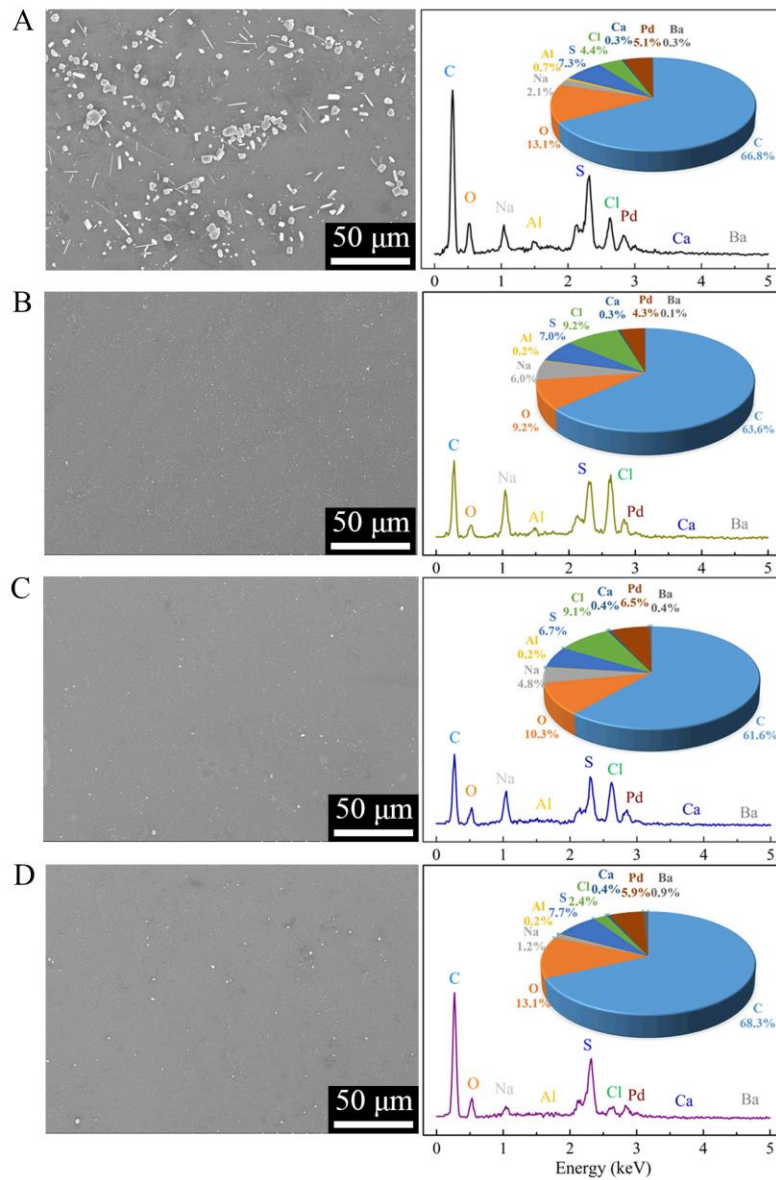
395 **Fig. 4.** Normalized water flux during RO desalination as a function of recovery for feed water  
 396 following UF treatment and that that had been subject to different pre-treatment processes. The  
 397 applied pressure was 5.5 MPa and the temperature during RO filtration was 293 K.

398

399 The surface morphology and elemental composition of the fouling layer was analyzed on RO  
 400 membranes following the treatment of effluents from the UF step that were subject to different  
 401 pre-treatments. The results from SEM-EDS analyses are shown in Fig. 5. C, O, and S are the  
 402 main elements observed on the surface of the RO membranes, similarly to the pristine membrane  
 403 (Tab.S2). Nevertheless, numerous particles of mostly  $\text{CaCO}_3$  and to a less extent of  $\text{BaCO}_3$  were  
 404 visible on the membrane fed with the raw FPW only treated by UF (Fig. 5A), as also shown in a  
 405 previous report (Guo et al., 2018). The presence and the size of these crystals was significantly  
 406 reduced when the water was pre-treated by coagulation (Fig. 5B). **This effect is caused by**  
 407 **coagulation, which reduced the pH and slowed down the precipitation of calcium carbonate.**  
 408 When PAC adsorption was applied, either at a concentration of activated carbon of 300 mg/L or



409 1200 mg/L, only trace amounts of Ca and Ba were present on the surface of the membrane. In  
 410 this case, the pH, alkalinity and Ca<sup>2+</sup> concentration were all key factors affecting the CaCO<sub>3</sub>  
 411 scaling of the RO membrane (Table S3). These observations confirm the effectiveness of  
 412 coagulation and PAC adsorption also to reduce scaling in the final RO step.



413  
 414 **Fig. 5.** SEM-EDS analyses of the RO membrane surface after fouling following the desalination  
 415 of UF effluents that had been treated with different pre-treatment processes. RO desalination of

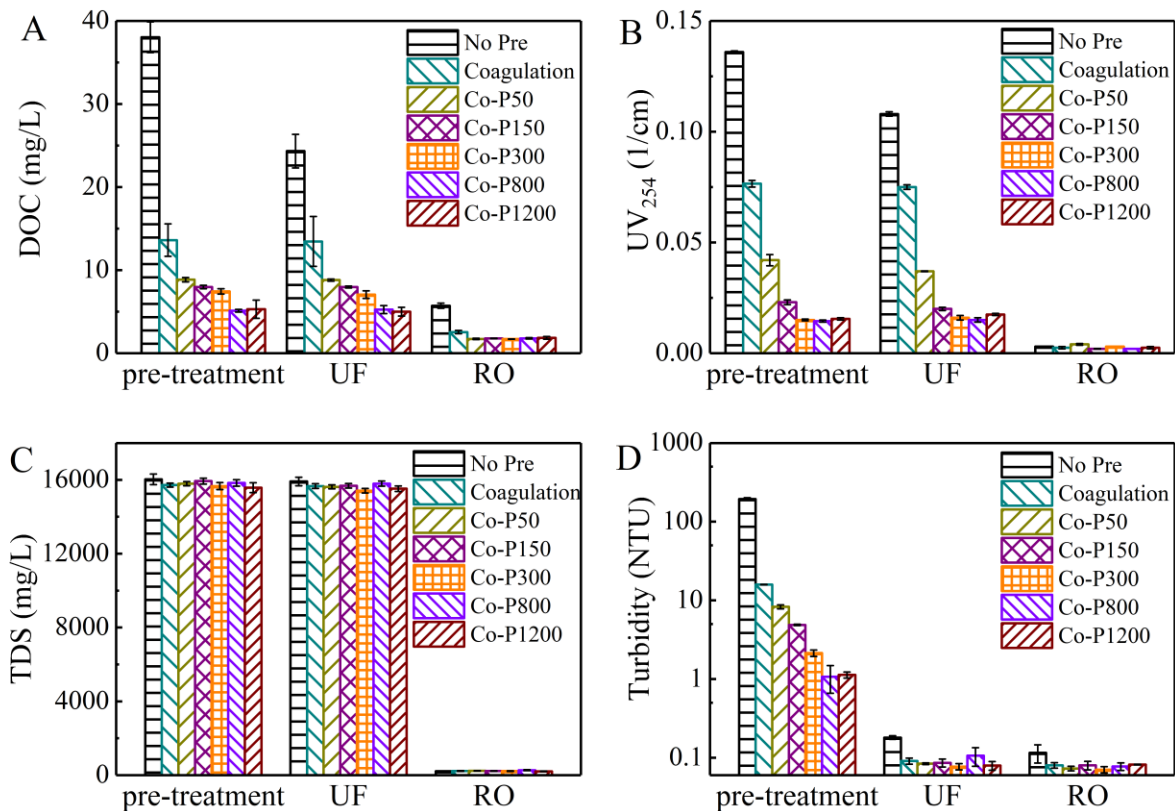
416 the UF permeate from the treatment of the (A) raw FPW; (B) effluent from coagulation; (C)  
417 effluent from coagulation and adsorption at the WP260 dose of 300 mg/L, and (D) effluent from  
418 coagulation and adsorption at the WP260 dose of 1200 mg/L. All the experiments performed at  
419 an applied pressure of 55 bar, final recovery of 50%, and temperature of 293 K.

420

### 421 **3.4 Quality of the effluents and of the final water stream**

422 Fig. 6 summarizes the removal rates of different classes of contaminants exiting the adsorption  
423 step, the ultrafiltration step, and the reverse osmosis steps, when the treatment units were  
424 challenged by waters pretreated by different processes. Coagulation reduced the DOC by 64.2%,  
425 and the addition of 300 mg/L PAC further reduced this parameter by 48.5%. In addition,  
426 coagulation had a good removal effect (91.6%) on turbidity. Adsorption following coagulation  
427 could further remove turbidity and reduce the turbidity of the effluent to a value below 10 NTU.  
428 The removal of DOC, UV<sub>254</sub>, and turbidity typically increased at higher dosages of PAC.  
429 However, very similar removals were observed for PAC amounts of 300 mg/L and 1200 mg/L,  
430 suggesting that 300 mg/L was the optimal dose for PAC adsorption of FPW, a result that is in  
431 complete accordance with the results of membrane fouling. The same organic removal rate  
432 previously observed by James et al. was achieved in this study but with roughly half the dose of  
433 PAC (Rosenblum et al., 2016). It should be noted that when the raw FPW was directly fed to the  
434 UF step, both the DOC and the UV<sub>254</sub> were significantly reduced in this step, possibly because  
435 the large particulates adhered to some organic matter, thus helping in its removal. However,  
436 feeding the UF directly with non-pretreated FPW is not a viable option, as discussed above and  
437 based on fouling results. As expected, UF abated the turbidity while it had negligible removal of  
438 ions. Finally, RO removed TDS very efficiently. Overall, the best system combining all the

439 treatment steps, i.e., coagulation followed by adsorption with 300 mg/L of PAC followed by UF  
 440 and RO, achieved a total ion reduction of more than 98.6%, and a DOC removal rate of 95.5%.  
 441 The quality of this effluent, also summarized in the rightmost column of Table 1, reached the  
 442 strict reuse standards for beneficial drilling applications and irrigation (Alzahrani and  
 443 Mohammad, 2014). **In addition, the cost data for each process unit (Table S4) are presented in**  
 444 **the SI based on the relevant literature.** The cost of the coagulation-adsorption-UF-RO process is  
 445 lower than other FPW treatment schemes including, for example, FO or mechanical vapor  
 446 compression. Therefore, the scheme proposed here has potential for the treatment of shale gas  
 447 FPW in China in the future.



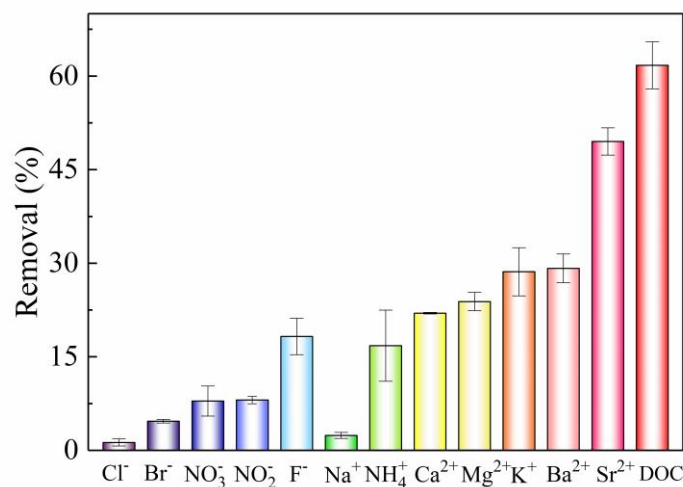
448

449 **Fig. 6.** Contents of different contaminants, specifically, (A) DOC; (B) UV<sub>254</sub>; (C) TDS; and (D)

450 turbidity obtained at different stages of the treatment systems and for effluents that were pre-  
451 treated by different processes. The label “No Pre” indicates raw water without any pre-treatment.

### 452 **3.5 Ion removal during activated carbon adsorption**

453 Although coagulation, adsorption, and UF did not remove TDS at a significant rate, it is of  
454 further interest to evaluate the ability of pre-treatments to remove some specific ions from FPW.  
455 The effect of coagulation and UF on specific ion removal was previously studied (Chang et al.,  
456 2019b; Guo et al., 2018). Here, we focus on the removal rates of different ions from the  
457 coagulated FPW by adsorption, presented in Figure 7. The results indicate a competition effect  
458 for the adsorption of cations, whereby the removal rate may be ranked in the following ascending  
459 order:  $\text{Na}^+$  (2.4%) <  $\text{NH}_4^+$  (16.8%) <  $\text{Ca}^{2+}$  (22.0%) <  $\text{Mg}^{2+}$  (23.9%) <  $\text{K}^+$  (28.6%) <  $\text{Ba}^{2+}$   
460 (29.2%) <  $\text{Sr}^{2+}$  (49.5%) < DOC (61.7%). The removal rate of anions may be instead arranged in  
461 the order:  $\text{Cl}^-$  (1.3%) <  $\text{Br}^-$  (4.7%) <  $\text{NO}_3^-$  (7.9%) <  $\text{NO}_2^-$  (8.1%) <  $\text{F}^-$  (18.3%) < DOC  
462 (61.7%). Clearly, the removal of divalent ions was greater than that of monovalent ions, as the  
463 adsorption of negatively charged DOC promotes the concurrent removal of cations associated  
464 with the organic molecules electrostatically or by complexation (Foo and Hameed, 2010; Gao et  
465 al., 2018). Interestingly, the removal of  $\text{K}^+$  was higher than for other divalent cations known to  
466 interact favorably with organic matter, such as calcium. This result may be partially rationalized  
467 with the overall larger size of  $\text{K}^+$ , which are thus associated with a more favorable energy of  
468 adsorption (Neugebauer and Scheffler, 1992). Finally, the kinetics of removal of the various ions  
469 by adsorption are presented in Fig. S6.



470

471 **Fig 7.** Removal rates of DOC, anions, and cations during the adsorption step with WP260  
 472 powdered activated carbon at the dose of 300 mg/L. **The adsorbate was coagulated FPW.**

473 **4. Conclusions**

474 Shale gas flowback and produced water, as a complex mixture of fracturing fluid and formation  
 475 water, may be effectively reused if appropriately treated. **This study provides a new FPW**  
 476 **treatment train consisting of coagulation, adsorption followed by UF and RO desalination.** In  
 477 particular, this work focused on the mechanism of adsorption and on the effects of pre-treatment  
 478 on effluent quality and membrane fouling control. The following main conclusions can be drawn  
 479 from the results:

- 480 1. The overall system performed a reliable treatment of the specific FPW to obtain a high-  
 481 quality product water with characteristics compatible with its reuse. Therefore, this study  
 482 provides a potential reference for a centralized shale gas FPW treatment plant in the Sichuan  
 483 Basin of China.

484 2. Coagulation and adsorption are valid pre-treatment for membrane processes. Interesting  
485 patterns were observed: when PAC was directly applied to adsorb contaminants from the raw  
486 FPW, the UF membrane fouling decreased with increasing PAC dosage. However, when  
487 coagulation was added before adsorption, UF membrane fouling increased with increasing PAC  
488 dosage. However, in this latter case, membrane fouling was much smaller than when UF was  
489 applied to an effluent pre-treated only by adsorption. Therefore, adsorption should be preceded  
490 by coagulation for improved performance of the system.

491 3. There was an optimal activated carbon dosage of 300 mg/L for the adsorption treatment.  
492 This dose resulted in the greatest gain in terms of fouling reduction in both UF and RO and in  
493 terms of quality of the final product water.

494 4. During the adsorption process, ions were removed at different rates, also due to co-sorption  
495 of cations with the organic matter. The mechanism of the adsorption of ions by PAC in FPW  
496 needs further research.

497

## 498 **Appendix A. Supplementary material**

499 The supporting information is available free of charge.

500 The size distributions of three adsorbents; linear plots of pseudo first order and pseudo second  
501 order adsorption kinetics of DOC on WP260; summary of adsorption kinetic parameters; EDS  
502 analyses of the new UF and RO membranes surface.

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511

512

513 **References**

- 514 Alzahrani S, Mohammad AW. Challenges and trends in membrane technology implementation  
515 for produced water treatment: A review. *Journal of Water Process Engineering* 2014; 4:  
516 107-133.
- 517 Amin Reyhania KS, Seyed Mahdi Seyed Shahabadi, Fatemeh Rekabdar, Ali Gheshlaghi.  
518 Optimization of operating conditions in ultrafiltration process for produced water  
519 treatment via Taguchi methodology. *Desalination and Water Treatment* 2015; 54: 2669-  
520 2680.
- 521 Angin D. Utilization of activated carbon produced from fruit juice industry solid waste for the  
522 adsorption of Yellow 18 from aqueous solutions. *Bioresource technology* 2014; 168: 259-  
523 266.
- 524 Annevelink MP, Meesters JA, Hendriks AJ. Environmental contamination due to shale gas  
525 development. *Science of the Total Environment* 2016; 550: 431-438.
- 526 Barbot E, Vidic NS, Gregory KB, Vidic RD. Spatial and temporal correlation of water quality  
527 parameters of produced waters from Devonian-Age shale following hydraulic fracturing.  
528 *Environmental Science & Technology* 2013; 47: 2562-2569.
- 529 Bellona C, Drewes JE, Xu P, Amy G. Factors affecting the rejection of organic solutes during  
530 NF/RO treatment--a literature review. *Water research* 2004; 38: 2795-2809.
- 531 Butkovskiy A, Bruning H, Kools SAE, Rijnaarts HHM, Van Wezel AP. Organic Pollutants in  
532 Shale Gas Flowback and Produced Waters: Identification, Potential Ecological Impact,  
533 and Implications for Treatment Strategies. *Environmental Science & Technology* 2017;  
534 51: 4740-4754.
- 535 Chang H, Li T, Liu B, Vidic RD, Elimelech M, Crittenden JC. Potential and implemented  
536 membrane-based technologies for the treatment and reuse of flowback and produced  
537 water from shale gas and oil plays: A review. *Desalination* 2019a; 455: 34-57.
- 538 Chang H, Liang H, Qu F, Shao S, Yu H, Liu B, et al. Role of backwash water composition in  
539 alleviating ultrafiltration membrane fouling by sodium alginate and the effectiveness of  
540 salt backwashing. *Journal of Membrane Science* 2016; 499: 429-441.
- 541 Chang H, Liu B, Yang B, Yang X, Guo C, He Q, et al. An integrated coagulation-ultrafiltration-  
542 nanofiltration process for internal reuse of shale gas flowback and produced water.  
543 *Separation and Purification Technology* 2019b; 211: 310-321.
- 544 Chang H, Liu T, He Q, Li D, Crittenden J, Liu B. Removal of calcium and magnesium ions from  
545 shale gas flowback water by chemically activated zeolite. *Water Science & Technology*  
546 2017; 76: 575-583.
- 547 Chang H, Qu F, Liu B, Yu H, Li K, Shao S, et al. Hydraulic irreversibility of ultrafiltration  
548 membrane fouling by humic acid: Effects of membrane properties and backwash water  
549 composition. *Journal of Membrane Science* 2015; 493: 723-733.
- 550 Chen G, Wang Z, Nghiem LD, Li X-M, Xie M, Zhao B, et al. Treatment of shale gas drilling  
551 flowback fluids (SGDFs) by forward osmosis: Membrane fouling and mitigation.  
552 *Desalination* 2015; 366: 113-120.
- 553 Cheng-Fang Lin Y-JH, Oliver J Hao Ultrafiltration processes for removing humic substances:  
554 effect of molecular weight fractions and PAC treatment. *Water Research* 1999; 33: 1252-  
555 1264.
- 556 Cheng W, Ding C, Sun Y, Wang X. Fabrication of fungus/attapulgite composites and their



557 removal of U(VI) from aqueous solution. *Chemical Engineering Journal* 2015; 269: 1-8.  
558 Crittenden JC, Trussell RR, Hand DW. *MWH's water treatment: principles and design* ( third  
559 edition ), 2012.  
560 Elimelech M, Phillip WA. The future of seawater desalination: energy, technology, and the  
561 environment. *Science* 2011; 333: 712-717.  
562 Estrada JM, Bhamidimarri R. A review of the issues and treatment options for wastewater from  
563 shale gas extraction by hydraulic fracturing. *Fuel* 2016; 182: 292-303.  
564 Foo KY, Hameed BH. Insights into the modeling of adsorption isotherm systems. *Chemical*  
565 *Engineering Journal* 2010; 156: 2-10.  
566 Gao H, Cao R, Xu X, Xue J, Zhang S, Hayat T, et al. Surface Area- and Structure-Dependent  
567 Effects of LDH for Highly Efficient Dye Removal. *ACS Sustainable Chemistry &*  
568 *Engineering* 2018; 7: 905-915.  
569 Guo C, Chang H, Liu B, He Q, Xiong B, Kumar M, et al. A combined ultrafiltration–reverse  
570 osmosis process for external reuse of Weiyuan shale gas flowback and produced water.  
571 *Environmental Science: Water Research & Technology* 2018; 4: 942-955.  
572 Harkness JS, Dwyer GS, Warner NR, Parker KM, Mitch WA, Vengosh A. Iodide, bromide, and  
573 ammonium in hydraulic fracturing and oil and gas wastewaters: environmental  
574 implications. *Environmental Science & Technology* 2015; 49: 1955-1963.  
575 Howarth RW, Ingraffea A, Engelder T. Natural gas: Should fracking stop? *Nature* 2011; 477:  
576 271-275.  
577 Huang L, Fan H, Xie H, Huang Z. Experimental study of treatment processes for shale gas  
578 fracturing flowback fluid in the eastern Sichuan Basin. *Desalination and Water Treatment*  
579 2016; 57: 24299-24312.  
580 Jarzyńska M, Pietruszka M. The application of the Kedem–Katchalsky equations to membrane  
581 transport of ethyl alcohol and glucose. *Desalination* 2011; 280: 14-19.  
582 Kondash A, Vengosh A. Water footprint of hydraulic fracturing. *Environmental Science &*  
583 *Technology Letters* 2015; 2: 276-280.  
584 Kong F-x, Chen J-f, Wang H-m, Liu X-n, Wang X-m, Wen X, et al. Application of coagulation-  
585 UF hybrid process for shale gas fracturing flowback water recycling: Performance and  
586 fouling analysis. *Journal of Membrane Science* 2017; 524: 460-469.  
587 Liu Q-S, Wang P, Zhao S-S, Zhang W. Treatment of an industrial chemical waste-water using a  
588 granular activated carbon adsorption-microwave regeneration process. *Journal of*  
589 *Chemical Technology & Biotechnology* 2012; 87: 1004-1009.  
590 Luek JL, Gonsior M. Organic compounds in hydraulic fracturing fluids and wastewaters: A  
591 review. *Water Research* 2017; 123: 536-548.  
592 Manz KE, Haerr G, Lucchesi J, Carter KE. Adsorption of hydraulic fracturing fluid components  
593 2-butoxyethanol and furfural onto granular activated carbon and shale rock.  
594 *Chemosphere* 2016; 164: 585-592.  
595 Neugebauer J, Scheffler M. Adsorbate-substrate and adsorbate-adsorbate interactions of Na and  
596 K adlayers on Al(111). *Physical Review B* 1992; 46: 16067-16080.  
597 Nguyen AH, Tobiasson JE, Howe KJ. Fouling indices for low pressure hollow fiber membrane  
598 performance assessment. *Water Research* 2011; 45: 2627-2637.  
599 Quay AN, Tong T, Hashmi SM, Zhou Y, Zhao S, Elimelech M. Combined Organic Fouling and  
600 Inorganic Scaling in Reverse Osmosis: Role of Protein-Silica Interactions. *Environmental*  
601 *Science & Technology* 2018; 52: 9145-9153.  
602 Remize PJ, Guigui C, Cabassud C. Evaluation of backwash efficiency, definition of remaining

603 fouling and characterisation of its contribution in irreversible fouling: Case of drinking  
604 water production by air-assisted ultra-filtration. *Journal of Membrane Science* 2010; 355:  
605 104-111.

606 Rosenblum JS, Sitterley KA, Thurman EM, Ferrer I, Linden KG. Hydraulic fracturing  
607 wastewater treatment by coagulation-adsorption for removal of organic compounds and  
608 turbidity. *Journal of Environmental Chemical Engineering* 2016; 4: 1978-1984.

609 Shaffer DL, Arias Chavez LH, Ben-Sasson M, Romero-Vargas Castrillon S, Yip NY, Elimelech  
610 M. Desalination and reuse of high-salinity shale gas produced water: drivers,  
611 technologies, and future directions. *Environmental Science & Technology* 2013; 47:  
612 9569-9583.

613 Shao S, Cai L, Li K, Li J, Du X, Li G, et al. Deposition of powdered activated carbon (PAC) on  
614 ultrafiltration (UF) membrane surface: influencing factors and mechanisms. *Journal of*  
615 *Membrane Science* 2017; 530: 104-111.

616 Sontheimer H, Crittenden JC, Summers RS. Activated carbon for water treatment. Vol 2.  
617 American Water Works Association 1988.

618 Stoll ZA, Forrestal C, Ren ZJ, Xu P. Shale gas produced water treatment using innovative  
619 microbial capacitive desalination cell. *Journal of Hazardous Materials* 2015; 283: 847-  
620 855.

621 Vengosh A, Jackson RB, Warner N, Darrah TH, Kondash A. A critical review of the risks to  
622 water resources from unconventional shale gas development and hydraulic fracturing in  
623 the United States. *Environmental Science & Technology* 2014; 48: 8334-8348.

624 Vidic RD, Brantley SL, Vandenbossche JM, Yoxheimer D, Abad JD. Impact of shale gas  
625 development on regional water quality. *Science* 2013; 340: 1235009.

626 Wang H, Qu F, Ding A, Liang H, Jia R, Li K, et al. Combined effects of PAC adsorption and in  
627 situ chlorination on membrane fouling in a pilot-scale coagulation and ultrafiltration  
628 process. *Chemical Engineering Journal* 2016; 283: 1374-1383.

629 Xiong B, Zydney AL, Kumar M. Fouling of microfiltration membranes by flowback and  
630 produced waters from the Marcellus shale gas play. *Water Research* 2016; 99: 162-170.

631 Zhang MM, Li C, Benjamin MM, Chang YJ. Fouling and natural organic matter removal in  
632 adsorben/membrane systems for drinking water treatment. *Environmental Science &*  
633 *Technology* 2003 37: 1663-1669.

634 Zhang Z, Zhuang Y, Li J, Zhou Z, Chen S. Feasibility evaluation of the treatment and recycling  
635 of shale gas produced water: a case study of the first shale gas field in the Eastern  
636 Sichuan Basin, China. *Environmental Science: Water Research & Technology* 2019; 5:  
637 358-369.

638 Zou C, Ni Y, Li J, Kondash A, Coyte R, Lauer N, et al. The water footprint of hydraulic  
639 fracturing in Sichuan Basin, China. *Science of the Total Environment* 2018; 630: 349-356.  
640