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Novel modelling approaches for turbulence-chemistry interaction and particle formation in flames

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Introduction

The accurate modelling of particle formation in flames is becoming important in a wide range of applications:

- Soot formation (undesired particulate matter)
- Flame aerosol synthesis (production of tailored materials, e.g. TiO₂)

Modelling of turbulent combustion requires an accurate description of turbulence-chemistry interaction in order to obtain reliable temperature and composition profiles

In order to obtain detailed information on particle features (size, morphology, composition, etc.) it is necessary to model particle dynamics

The stochastic nature of both turbulence and some processes involved in particle dynamics suggests to statistically solve these problems in terms of the fluid probability density function (PDF) and of the particle number density function (NDF)

Turbulence-chemistry interaction

The accurate modelling of particle formation requires the accurate modelling of velocity, temperature and composition profiles in the flame: Computational Fluid Dynamics

• continuity $\frac{\partial \overline{\rho}}{\partial t} + \frac{\partial}{\partial x_i} \left(\overline{\rho} \tilde{U}_i \right) = 0$ **Turbulence modelling (Reynolds** Averaged Navier-Stokes equations) • momentum $\frac{\partial}{\partial t} \overline{\rho} \tilde{U}_i + \frac{\partial}{\partial x_-} \overline{\rho} \tilde{U}_i \tilde{U}_j + \frac{\partial}{\partial x_-} \overline{\rho} \widetilde{u}_i u_j = -\frac{\partial \overline{\rho}}{\partial x_-} + \nu \frac{\partial^2 \overline{\rho} \tilde{U}_i}{\partial x_- \partial x_-}$

• scalars $\frac{\partial}{\partial t} \overline{\rho} \tilde{\Phi}_{\alpha} + \frac{\partial}{\partial x_{i}} \overline{\rho} \tilde{\Phi}_{\alpha} \tilde{U}_{i} + \frac{\partial}{\partial x_{i}} \overline{\rho} \widetilde{\phi}_{\alpha} \tilde{u}_{i} = \Gamma_{t} \frac{\partial^{2} \overline{\rho} \tilde{\Phi}_{\alpha}}{\partial x_{i} \partial x_{i}} \left(+ \widetilde{S} \left(\mathbf{\Phi} \right) \right)$

The chemical reaction is affected by turbulent fluctuactions of both temperature and concentration. ———— The knowledge of the **probability density function** of composition and temperature allows to compute the averaged chemical source term.

Presumed PDF methods: the functional shape of the PDF is assumed

Particle formation

The accurate modelling of particle formation in flames requires the solution of the **Population Balance Equation (PBE)**, in order to describe the evolving distribution of the particle state variables of interest:

$$\frac{\partial \tilde{n}(\boldsymbol{\xi}; \mathbf{x}, t)}{\partial t} + \frac{\partial}{\partial x_i} \widetilde{U}_i \tilde{n}(\boldsymbol{\xi}; \mathbf{x}, t) - \frac{\partial}{\partial x_i} \left[(\Gamma + \Gamma_t) \frac{\partial \tilde{n}(\boldsymbol{\xi}; \mathbf{x}, t)}{\partial x_i} \right] = \widetilde{S(\boldsymbol{\xi}; \mathbf{x}, t)}$$

where $\tilde{n}(\xi; \mathbf{x}, t)$ is the **number density function** of the particle population, in terms of a number of **internal** coordinates (ξ), which are properties identifying the status of each particle (e.g., diameter, volume, surface area, velocity, composition, age...).

The solution of the PBE is not trivial. When it has to be coupled with CFD computations, the solution technique has to be simple and to have low computational cost (number of additional transport equations to be solved).

Only methods based on the moments approach are suitable to be coupled with CFD for the solution of PBEs.

$$\widetilde{m_{k}}(\mathbf{x},t) = \int_{0}^{+\infty} \widetilde{n}(\xi;\mathbf{x},t) \xi^{k} d\xi \qquad \qquad \underbrace{\frac{\partial \widetilde{m_{k}}(\mathbf{x},t)}{\partial t} + \widetilde{U_{i}} \frac{\partial \widetilde{m_{k}}(\mathbf{x},t)}{\partial x_{i}} - \frac{\partial}{\partial x_{i}} \left[\Gamma_{i} \frac{\partial \widetilde{m_{k}}(\mathbf{x},t)}{\partial x_{i}} \right] \underbrace{= \widetilde{S}(\mathbf{x},t)}$$

The source term $S(\mathbf{x},t)$ determines the evolution of moments due to **nucleation**, **aggregation**, **molecular** growth, oxidation and restructuring.

The Finite-Mode PDF model

The PDF is described by a sum of Dirac delta functions (each representing a reacting or non-reacting environment):

$$f_{\Phi}(\mathbf{\Psi};\mathbf{x},t) = \sum_{n=1}^{N_e} p_n(\mathbf{x},t) \prod_{\alpha=1}^{N_s} \delta \left[\psi_{\alpha} - \langle \phi_{\alpha} \rangle_n(\mathbf{x},t) \right]$$

(environments)

Probabilities (volume fractions) of modes $\frac{\partial p_n}{\partial t} + \tilde{U}_j \frac{\partial p_n}{\partial x_i} - (\Gamma + \Gamma_t) \frac{\partial^2 p_n}{\partial x_i \partial x_i} = G_n(\mathbf{p}) + C_n^p$

Molecular mixing Spurious terms due to the finite-mode representation

Weighted concentrations $\frac{\partial \langle s_{\alpha} \rangle_{n}}{\partial t} + \tilde{U}_{j} \frac{\partial \langle s_{\alpha} \rangle_{n}}{\partial x} - (\Gamma + \Gamma_{t}) \frac{\partial^{2} \langle s_{\alpha} \rangle_{n}}{\partial x_{j} \partial x_{j}} = M_{n,\alpha}(\mathbf{p}, \mathbf{s}) + p_{n} S(\langle \mathbf{\phi} \rangle_{n}) + c_{n,\alpha}^{s}$

 $\left|\left\langle s_{\alpha}\right\rangle _{n}=p_{n}\left\langle \phi_{\alpha}\right\rangle _{n}$

N=3

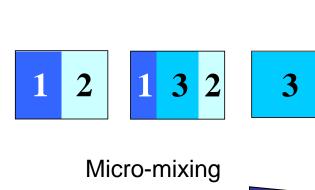
velocity

Coflow

velocity

The reaction occurs only in the mixed environment (3).

(a) The Mixing Layer



The Direct Quadrature Method of Moments (DQMOM)

Closure of the source term

Quadrature approximation

 $\tilde{n}(\xi; \mathbf{x}, t) \approx \sum_{i=1}^{N} w_{\alpha}(\mathbf{x}, t) \prod_{i=1}^{M} \delta \left[\xi_{i} - \xi_{i\alpha}(\mathbf{x}, t) \right]$

 $m_{k_1,k_2,\ldots,k_M} = \int_{-\infty}^{\infty} \xi_1^{k_1} \int_{-\infty}^{\infty} \xi_2^{k_2} \cdots \int_{-\infty}^{\infty} \xi_M^{k_M} \tilde{n}(\boldsymbol{\xi}; \mathbf{x}, t) d\xi_1 d\xi_2 \cdots d\xi_M \approx \sum_{k=1}^{N} w_{\alpha} \prod_{i=1}^{M} \xi_{i\alpha}^{k_i}$

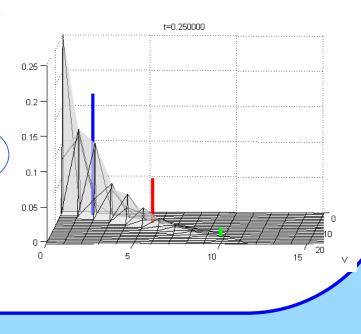
It is possible to calculate the values of **weights** and weighted **abscissas** $\zeta_{i,\alpha} = W_{\alpha} \xi_{i,\alpha}$ of the delta functions, forcing them to yield known values of the moments, directly solving the transport equations: $\frac{\partial w_{\alpha}}{\partial t} + \frac{\partial}{\partial x_{i}} \left(\tilde{U}_{j} w_{\alpha} \right) - \frac{\partial}{\partial x_{i}} \left[\left(\Gamma + \Gamma_{t} \right)^{;} \frac{\partial w_{\alpha}}{\partial x_{i}} \right] = a_{\alpha} \frac{\partial \varsigma_{i,\alpha}}{\partial t} + \frac{\partial}{\partial x_{i}} \left(\tilde{U}_{j} \varsigma_{i,\alpha} \right) - \frac{\partial}{\partial x_{i}} \left[\left(\Gamma + \Gamma_{t} \right) \frac{\partial \varsigma_{i,\alpha}}{\partial x_{i}} \right] = b_{i,\alpha}$

The source terms for weights and abscissas are calculated solving a *linear* algebraic system obtained from the population balance written as a balance equation for moments, after the application of the quadrature approximation; in the bivariate case:

representation

 $\sum_{\alpha=1}^{N} \left[\left(1 - k - l \right) \xi_{1,\alpha}^{k} \xi_{2,\alpha}^{l} a_{\alpha} + k \xi_{1,\alpha}^{k-1} \xi_{2,\alpha}^{l} b_{1,\alpha} + l \xi_{1,\alpha}^{k} \xi_{2,\alpha}^{l-1} b_{2,\alpha} \right] = \overline{C}_{k,l} + S_{k,l}^{(N)}$ Spurious terms due to the finite-mode

for moments



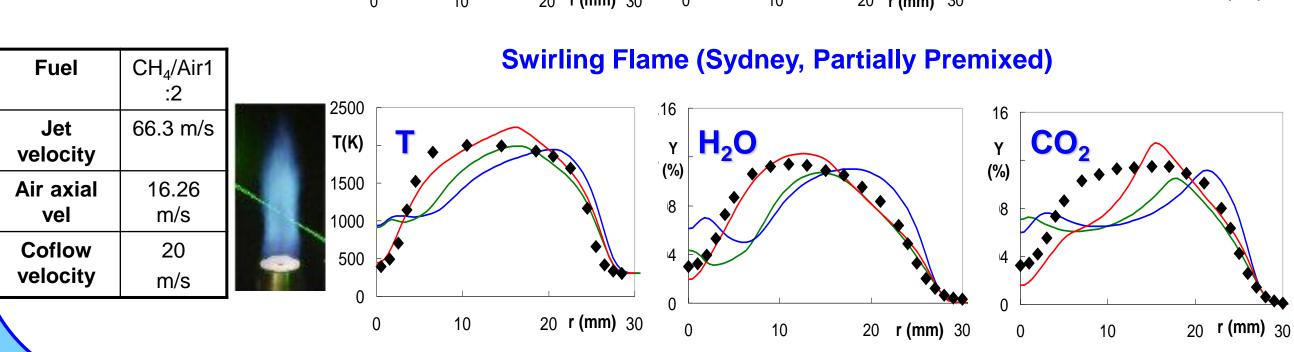
Turbulent combustion: Results

Flames studied in the framework of the International Workshop on **Turbulent Non-premixed Flames**

3E-Finite Mode PDF (4-step mechanism by Jones and Lindsted) β-PDF (chemical equilibrium) laminar flamelets (skeletal mechanism 17 species) Non Swirling Flame (Bluff body)

Fuel

Location: 30 mm above the burner



Soot formation: Results (bivariate PBE)

Case study: the non-premixed ethylene-air turbulent flame A (Kent & Honnery, 1987^(*)) **Soot volume fraction** Bivariate simulation (V and A) Monovariate simulation with 2.5 V (m³) algebraic model for fractal - - x=345 mm dimension Artelt C., Schmid H.J., Peukert W. (2003). On simulations. Journal of Aerosol Science, 34, $A (m^2) 4$ Projections of the nodes along the internal coordinates 6.29e-**Volume Surface Area** $x_{A} = 300 \text{ mm}$

A ___ B $x_{\rm R} = 590 \, {\rm mm}$ $x_{B} = 590 \text{ mm}$

(*) Kent J. H., and Honnery D. (1987). Soot and mixture fraction in turbulent diffusion flames. Combustion Science and Technology, 54, 383-397

Conclusions

In this work, two methods based on a similar description of the PDF and the NDF, represented by a finite sum of Dirac delta functions, were successfully employed to solve the problem of turbulence-chemistry interaction in turbulent flames (finite-mode PDF method), and the population balance for modelling soot formation (Direct Quadrature Method of Moments, DQMOM).

Both methods appeared to be versatile and reliable tools, particularly suitable for CFD computation, presenting a good trade-off between accuracy and computational cost.

In particular:

- The Finite-Mode PDF model is suitable for modelling turbulence-chemistry interaction in flames
- The implementation of finite rate chemistry can be crucial to obtain good results, especially in the case of partially premixed flames.
- The **DQMOM** is a valid approach for the solution of the population balance equation within a CFD code, both in the monovariate and in the bivariate case.
- Simplified kinetics for soot nucleation, growth, oxidation and aggregation lead to good results in the flame under investigation.
- In order to take into account properly the evolution of particle morphology (fractal dimension) it is important to solve the bivariate population balance, i.e. to follow the evolution of both particle volume and surface area.