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# Analysis of plasma termination in the JET hybrid scenario

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**Abstract.** This paper analyses the final phase of hybrid scenario discharges at JET, the reduction of auxiliary heating towards finally the Ohmic phase. The here considered Ohmic phase is mostly still in the current flattop but may also be in the current ramp down. For this purpose a database is created of 54 parameters in 7 phases distributed in time of the discharge. It is found that the occurrence of a locked mode is in most cases preceded by a radiation peaking after the main heating phase either in a low power phase and/or in the Ohmic phase. To gain insight on the importance of different parameters in this process a correlation analysis to the radiation peaking in the Ohmic phase is done. The first finding is that the further away in time the analysed phases are the less the correlation is. This means in the end that a good termination scenario might also be able to terminate unhealthy plasmas safely. The second finding is that remaining impurities in the plasma after reducing the heating power in the termination phase are the most important reason for generating a locked mode which can lead to a disruption.

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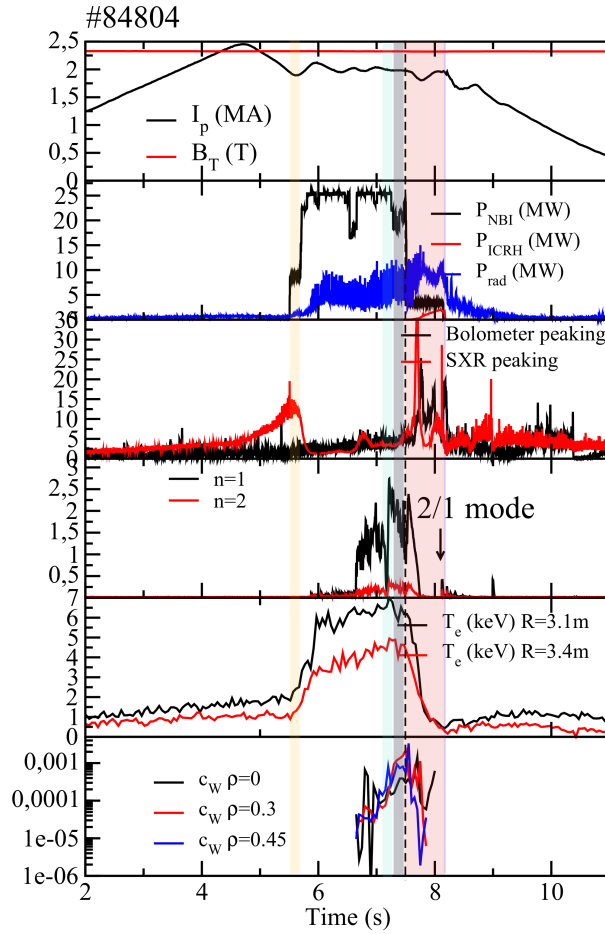
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## 1. Introduction

Within the last few years significant progress has been made on the hybrid scenario in JET[1]. The hybrid scenario [2, 3, 4, 5, 6] is one of the foreseen ITER scenarios. Compared to the standard 15MA baseline ITER scenario the plasma current is reduced and the normalised beta increased. On JET also the confinement time normalised to the  $H_{98,y2}$ -scaling is increased and the scenario is usually obtained by modifying the  $q$ -profile using a current “overshoot” [1, 7]. However most of the analysis concentrated so far on the high performance phase of the plasma. Another important aspect is to terminate such high performance plasmas safely. Future devices will have a very limited budget for disruptions before serious damage to the plasma facing components and/or the vacuum vessel and coils could occur. Especially with the introduction of the ITER like wall (ILW) in JET the plasmas often are hampered by impurity accumulation and mode activity when ramping down the power or even before [8]. Earlier a reduced data base has been analysed [9] and preliminary improvements to the termination scenario have been suggested. The paper will start with a description of a typical hybrid scenario description. In sections 3 and 4 the database and its analysis are presented. In section 5 a new termination scenario is sketched and an example of a more successful termination is discussed. Then in section 6 the paper is summarised and conclusions are drawn.

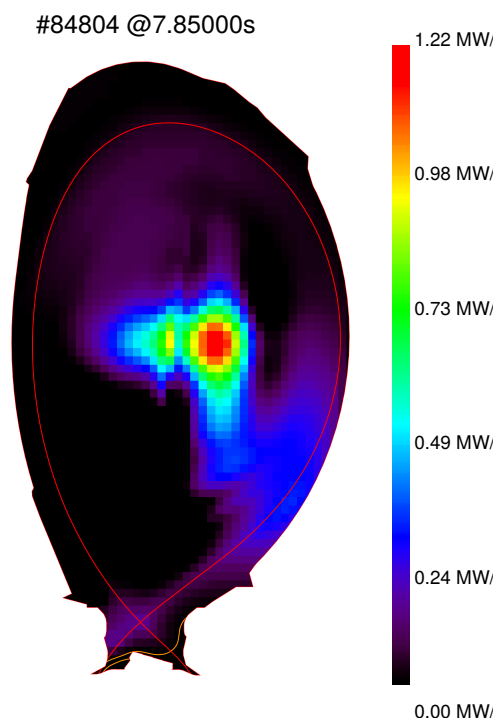
## 2. Description of an ILW hybrid scenario termination

In figure 1 time traces of a representative plasma termination are shown. The figure is organised as follows: the top graph contains the plasma current and the magnetic field. The next graph down contains the NBI and ICRH heating power and the total radiated power. In the next graph the radiation peaking is represented as ratios between horizontal central and about half radius line integrated measurements from the Bolometer (Channels 15+18 for further reference) and the Soft X-Ray (SXR, channels 10+12) diagnostic. In the next row down the amplitude of selected differences of magnetic pick up coils is plotted being proportional of  $n=1/n=2$  MHD perturbations in the plasma. In the next graph a central and an off-axis electron temperature from the High Resolution Thompson Scattering (HRTS) diagnostic is shown. In the bottom row an estimated W concentration from a simple deconvolution of the SXR radiation and atomic data as input [10] is plotted for different radii. The plasma does not accumulate heavy Z impurities (mainly W) in the main heating phase and has only a moderate W concentration of  $10^{-4}$  opposite to the cases discussed in [11, 9]. At the time when the NBI power reduces at  $t = 7.5s$  the W concentration off-axis increases to almost  $10^{-3}$  but the radiation profile is not peaked yet and the total radiation is significantly larger



**Figure 1.** Overview of a typical hybrid pulse termination including the marking of the considered discharge phases as vertical bars.

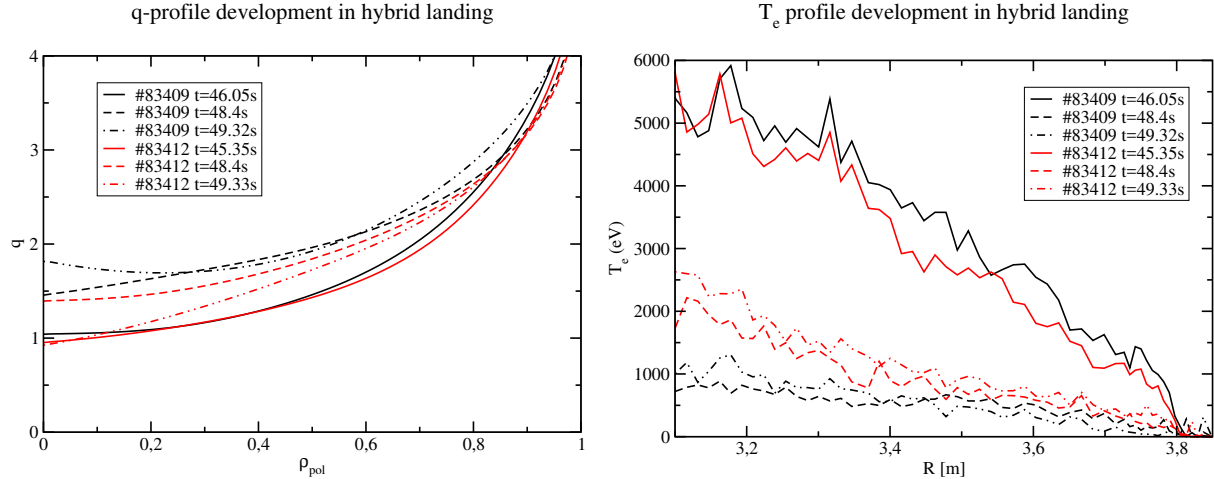
than the heating power. 100ms later the peaking of the SXR diagnostic increases strongly, which is typical for high Z impurity accumulation. The electron temperature drops within 500ms and the profile flattens. The impurity peaking between  $t=7.7s$  and  $t=8.2s$  is mainly seen on the bolometer and is increasing again. In figure 2 a tomographic reconstruction of the radiation measured by the bolometer at  $t=7.85s$  is shown. Even though there are some vertical and horizontal artifacts the reconstruction shows the strong peaking at about 100ms before the onset of the  $n=1$  mode. The estimate of the W concentration in this phase fails because the plasma temperature becomes too low to detect the SXR radiation through up to  $250\ \mu m$  thick Be filters. The increase of the SXR peaking after 8s is caused by a drop of the off-axis channel and is not representative for the core radiation. The peaking factors of the SXR and the bolometer diagnostics are very different in the main heating phase due to a strong  $T_e$  dependence in the SXR radiation which is much weaker on the total radiation. The change in  $T_e$  profile leads then to the excitement of a  $n=1$  mode which locks shortly afterwards (as reported in [8]). As a consequence the control system stops the pulse by initiating a fast current ramp. In the statistics described later this pulse counts as a locked mode in the low



**Figure 2.** Radiation peaking in a tomographic reconstruction shortly before the MHD mode is excited.

power phase.

The excitement of the  $n=1$  mode is connected to a change in  $q$ -profile (as reported in [8]). In figure 3 on the left hand side the  $q$ -profile development for a pulse with locked mode (black) and without locked mode (red) is shown. A different pair of pulses is shown here because the MSE measurement in the landing phase is often not available because the measurement beam is in most pulses switched off. On the right hand side the electron temperatures are plotted. With the switch off of the main heating the temperature drops in both cases strongly. In the case without locked mode some temperature peaking remains whereas in the other case very flat temperature profiles are found. In this phase, external current drive is negligible and the current profile is dominated by the Ohmic contribution. Since the temperatures are low the  $q$ -profile is changing on a fast time scale reflecting the changes in the electron temperature profile. The  $q$ -profile in the pulse without locked mode somewhat recovers and stays monotonic, in the pulse with locked mode a high  $q_{\min}$  can be seen and also shear reversal is found in the central region. To assess the tearing mode stability the toroidal plasma current density gradient and the resistivity at the  $q = 2$  surface for both plasmas have been computed. In the case where a mode occurs the resistivity is larger and an increase in current density gradient is observed before the mode is triggered. In the case without mode locking the resistivity is generally lower and no sustained current density gradient increase is observed. Qualitatively this supports that the plasma which develops a locked mode was more tearing unstable before than the plasma without. In addition the rotation is usually low as well and

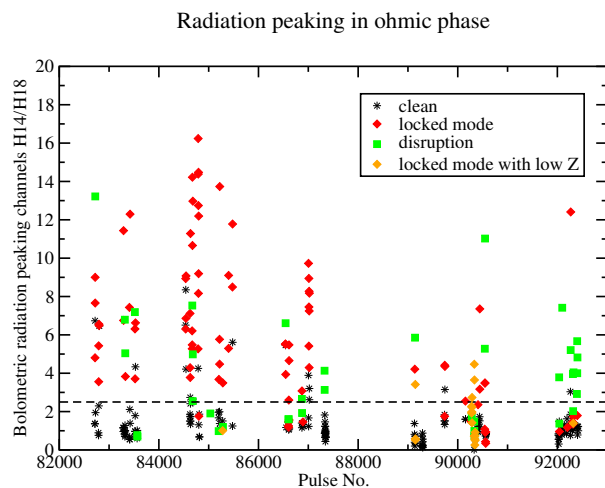


**Figure 3.**  $q$ -profile and  $T_e$ -profile development with (black) and without (red) locked mode

a locking is likely. In the pulse discussed earlier (figure 1) the electron temperature recovers after the mode locking and the radiation peaking reduces before a disruption could occur. In about 53% of the hybrid pulses a ramp down succeeds after a locked mode without disruption (and of course many plasmas terminate without locked mode or disruption). Most probably this is due to the higher  $q_{95}$  compared to baseline plasmas.

### 3. Database

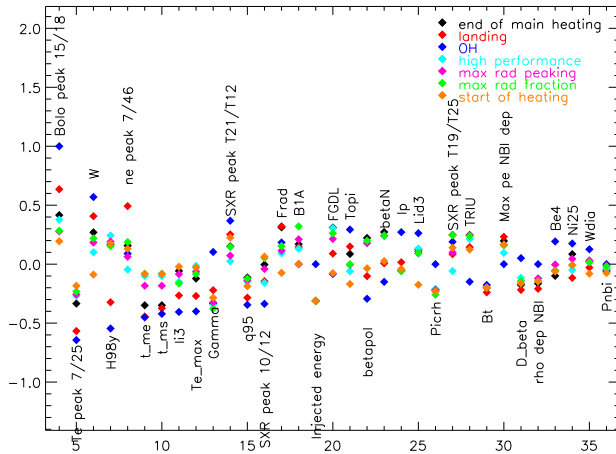
For this paper a database is developed in order to reveal the intricate relationship between various plasma parameters at different times in the discharge affecting the landing of the plasma. The database consists of 480 pulses (all hybrid pulses in the ILW which reached the main heating phase) of which 215 pulses had a locked mode and 101 of them disrupted (5 in the main heating phase due to a stop of vertical position control and 2 in the main heating phase due to excessive radiation and 76 in the Ohmic phase after the heating has stopped, the Ohmic phase before the heating starts is not considered here). In the 40 pulses with  $q_{95} < 3.6$  (3.8 is the nominal value for a JET hybrid pulse) 33 had a locked mode and 18 disrupted. In the reduced database (pulses with ILW until 2014 [9]) 63% of the pulses had a locked mode whereas the extended database (all pulses with ILW until now) has now 45% locked modes which indicates a learning effect taken place in the years in between. On the other hand the disruptivity in the 2014 database was 13% and in the extended database it has increased to 21%. The increase in disruption rate is mainly because of the higher currents used in the more recent experiments. Above a plasma current of 2MA a triggering of the disruption mitigation valve (DMV) is mandatory if a disruption is predicted, e.g. if the locked mode signal is exceeding a certain value. This protection has been used also at smaller currents than 2MA in order to prepare the scenario. Out of the 49 disruptions 30 disruptions were actually caused by the firing of the DMV. Whether the plasma would have disrupted without DMV or not cannot be determined. Since before 2015 the operation was different and the DMV in these cases was triggered only during an already ongoing disruption the statistics is misleading. An interesting subset of the pulses have been seeded by Neon, either to reduce the power load in the divertor



**Figure 4.** Bolometric radiation peaking in Ohmic phase - definition of threshold

or to improve the ion temperature measurement. Of the 29 pulses with Neon, 28 pulses have a locked mode and 8 of those disrupt. The only plasma which terminates cleanly is the one with the lowest Neon gas puff. The main difference in the parameters during the landing is that pulses with Neon in the main heating phase tend to maintain a higher density during the low power and Ohmic phase which then during the current ramp down causes either a density limit disruption as often observed during operation in a carbon machine or results in a locked mode but without disruption. From now on only the extended database is considered. To understand the importance of the different phases of the pulse a set of 54 parameters has been collected in 7 phases of the pulse. The phases are defined as 200ms windows at the end of the main heating phase, the maximum performance (maximum stored energy), the maximum SXR radiation peaking within the main heating, the maximum radiation fraction within the main heating phase and at the beginning of the main heating. In addition the low power phase following the main heating and a time window of 0.7s at the start of the following Ohmic phase are taken, both cut short in case of a locked mode or disruption. The phases are also indicated in figure 1 as colored bars.

In order to make use of the collected data a common reference point has to be found. In figure 4 the bolometric peaking factor is shown, the pulses with locked modes have red symbols and clean plasmas black ones. Above a peaking of 2.5 we find 75.3% of the pulses which have a locked mode not taking into account pulses with Neon injection and 62% of the pulses which disrupted but only 9.6% of the pulses without problems. This shows that in most pulses the radiation peaking in the Ohmic phase is a critical parameter. Doing the exercise with the other parameters in the database does not yield an as good discrimination criteria and therefore the radiation peaking in the Ohmic phase has been used as a reference for a correlation analysis with other parameters to get an indication of their importance. As can be seen in 6 the radiation peaking in different phases remains an important parameter in this analysis. Together with the physics picture given in the introduction this is all consistent and is indicating that the statistics not only gives correlations but shows causality in this case.



**Figure 5.** Correlation coefficient of bolometric radiation peaking during the Ohmic phase plotted against reduced set of database parameters. X-axis sorted according to highest correlation coefficients ignoring the different phases.

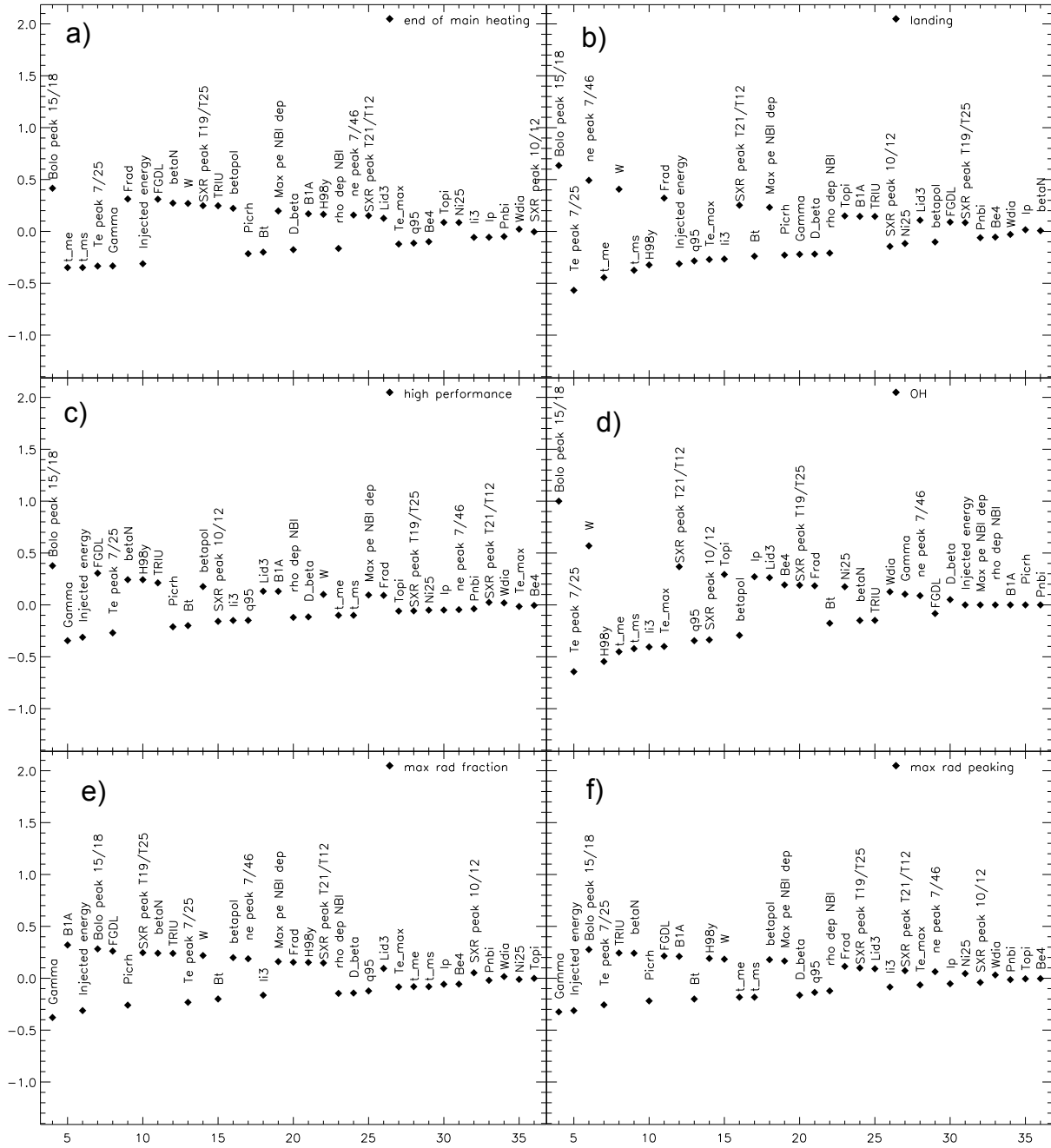
#### 4. Analysis of the database using correlations

In the following a correlation analysis between different parameters within the database is presented. The correlation coefficient e.g. between the heating power in the main heating phase and the radiation peaking in the Ohmic phase is calculated. The idea behind this analysis is that first the most important parameters are identified and second some information on the temporal evolution is obtained. To make an example, if bad terminations would be caused predominantly by large impurity events in the main heating phase then a large correlation coefficient between the maximum radiation and/or maximum radiation fraction in the high radiation fraction time window and the radiation peaking in the Ohmic phase should be visible - which is not the case. The correlation coefficient of a reduced set of parameters is shown in figure 5. The colours symbolise the different phases (also indicated in figure 1) and the x-axis is sorted from higher correlations on the left to lower on the right using the absolute values and not the phase specific ones.

The signals are described in table 1. In this table there are a few outstanding parameters like 3 bolometric plus 2 SXR (Soft X-Ray) peaking factors. The fact that W has a complicated spatial and temporal evolution (see [11]) makes a 0-D analysis complicated as well. First after an influx W is usually not accumulating in the core immediately but larger W concentrations are observed off-axis at about half radius with relatively large poloidal asymmetries due to the large toroidal rotation speed. In this case a horizontal channel in the mid-plane will observe an increase in radiation but a vertical channel from a top view not. So the peaking of the horizontal channels detects an increase in the W concentration but not necessarily a central peaking. On the other hand the signal of the vertical camera channels will see just the central peaking of the impurities but only if the Shafranov shift is right. Therefore several different ratios of vertical channels are necessary to detect the peaking for different Shafranov shifts e.g. during the main heating phase and during the low power phase during the termination.

**Table 1.** Summary table of most important correlations in all seven phases.

Label	Description
Bolo peak 15/18	ratio of two horizontal bolometer channels, one through the centre and the other cutting at about half radius
Te peak 7/25	electron temperature ratio from the HRTS diagnostic using a channel at 3.1m (central) and at 3.4m (off-axis)
W	W source signal (WII) in the divertor measured by a VUV spectrometer
H98y	H-mode scaling factor describing the confinement relative to the IPB $H^{98y2}$ scaling
ne peak 7/25	electron density channel ratio (as for $T_e$ ) from the HRTS diagnostic
t_me/t_ms	ending/starting time of the window where the data have been taken
li3	internal inductance of the plasma
Te_max	highest electron temperature measured in the plasma by HRTS
Gamma	total gas flux from the fuelling system
SXR peak T21/T12	ratio of 2 vertical lines of sight, one through the center and one going off-axis
SXR peak T19/T25	similar as SXR peak T21/T12 slightly different positions
SXR 10/12	ratio of horizontal channels with thicker Be-filters
q95	$q_{95}$ from the equilibrium reconstruction
Frad	radiated power measured by bolometer divided by the total heating power
B1A	amplitude of the strongest n=1 mode in the plasma
injected energy	time integral of the heating power
FGDL	electron density divided by the Greenwald scaling density
Topi	totally radiated power from the bolometer
betapol	poloidal beta calculated by the equilibrium reconstruction Def.: $\beta_{\text{pol}} = 2\mu_0 \frac{\langle p \rangle_A}{\langle B_{\text{pol}} \rangle^2}$ , where $\langle p \rangle_A$ is the poloidal cross-section averaged plasma pressure and $\langle B_{\text{pol}} \rangle$ the average poloidal magnetic field on the plasma boundary
betaN	normalised beta, $\beta_N = \beta_{\text{tor}} / \frac{I_p}{aB_T}$ with $B_T$ toroidal magnetic field
Lid3	line integrated density through the centre from the interferometer diagnostic
Picrh	injected power from the ICRH heating
TRIU	upper triangularity of the plasma configuration calculated by the equilibrium reconstruction
Max pe NBI dep	maximum power density deposited in the electrons by the NBI heating calculated by the inter-shot PENCIL
rho dep NBI	radius of the maximum power deposition from PENCIL
Be4	calibrated line intensity from a VUV spectrometer proportional to the Be source
NI25	proportional to the Nickel concentration measured as well by a VUV spectrometer
Wdia	total stored energy from diamagnetic loop
Pnbi	total injected power from the neutral beam heating system



**Figure 6.** Correlation coefficient as in figure 5. X-axis sorted according to importance in the labelled phase of the pulse.

The different sensitivity for high Z impurities in the SXR diagnostic compared to the total radiation makes it useful to look to it separately. The geometrical properties are as discussed before. In addition the SXR diagnostic is strongly temperature dependent but very sensitive to high Z impurities. Therefore the diagnostic is ideal to diagnose a W accumulation in the main heating phase but almost without use in an Ohmic phase due to the lower temperatures. Additionally the horizontal SXR camera has thicker Be-filters ( $350 \mu\text{m}$  compared to  $250 \mu\text{m}$  in the vertical camera) and measures generally only at higher temperatures (this explains the

**Table 2.** Summary table of most important correlations to the radiation peaking in the Ohmic phase for all seven phases.

	Max pos	2nd	3rd	Max neg	2nd	3rd
All	Rad peak (0.64) low pow.	W influx (0.57) OH	$n_e$ peak. (0.49) low power	$T_e$ peaking (-0.65) OH	$H_{y,2}^{98}$ (-0.54) OH	$l_i(3)$ (-0.4) OH
End of heating	Rad. peak (0.42)	$f_{\text{rad}}$ (0.31)	$f^{\text{GW}}$ (0.31)	$T_e$ peaking (-0.33)	$\Gamma$ (-0.33)	Injected En. (-0.33)
Low power	Rad. peak (0.64)	$n_e$ peaking (0.49)	W influx (0.41)	$T_e$ peaking (-0.57)	$H_{y,2}^{98}$ (-0.32)	Injected En. (-0.31)
OH	W influx (0.57)	SXR peak. (0.37)	$P_{\text{rad}}$ (0.29)	$T_e$ peaking (-0.59)	$H_{y,2}^{98}$ (-0.54)	$l_i(3)$ (-0.4)
Max. perf.	Rad. peak (0.38)	$f^{\text{GW}}$ (0.31)	$\beta_N$ (0.24)	$\Gamma$ (-0.34)	Injected En. (-0.31)	$T_e$ peaking (-0.27)
Max. rad. peaking	Rad. peak (0.28)	$\delta^U$ (0.24)	$\beta_N$ (0.24)	$\Gamma$ (-0.32)	Injected En. (-0.31)	$T_e$ peaking (-0.27)
Max. rad. fraction	B1A (0.32)	Rad. peak (0.28)	$f^{\text{GW}}$ (0.26)	$\Gamma$ (-0.38)	Injected En. (-0.31)	$P_{\text{ICRH}}$ (-0.26)
H-mode entrance	SXR peak. (0.22)	Rad. peak (0.19)	$H_{y,2}^{98}$ (0.18)	Injected En. (-0.31)	$\Gamma$ (-0.29)	$P_{\text{ICRH}}$ (-0.23)

anti correlation in the Ohmic phase).

The magnetic fluctuation signals are from magnetic probes. B1A is the amplitude of the strongest  $n=1$  mode in the plasma which is usually produced by either sawteeth or fishbones,  $2/1$  modes are extremely rare in the JET hybrid mode plasmas. Unfortunately the  $n=2$  and  $n=3$  signals were so scarcely available for the database that they had to be omitted.

The database contains 18 more signals which have been omitted in the figures either because they are redundant (4 bolometer peakings, 2  $T_e$  peaking factors, 5 SXR peaking factors, the thermal confinement time, line integrated density off-axis, density peaking factor from the interferometer channels, total radiated power from the bolometer using a different integration method) or because they are not well populated as the  $n=2$  and  $n=3$  MHD amplitudes.

The highest correlations are seen within the Ohmic phase itself. The leading parameters related to  $T_e$  as e.g.  $\tau_E$ ,  $H_{98y2}$ ,  $\rho_{\text{dep}}^{\text{NBI}}$ ,  $P_{\text{ICRH}}$  are not useful in this phase of the pulse.  $t_{\text{ms}}$  and  $t_{\text{me}}$  are the time of the start and ending of the phase and also probably not of much use.

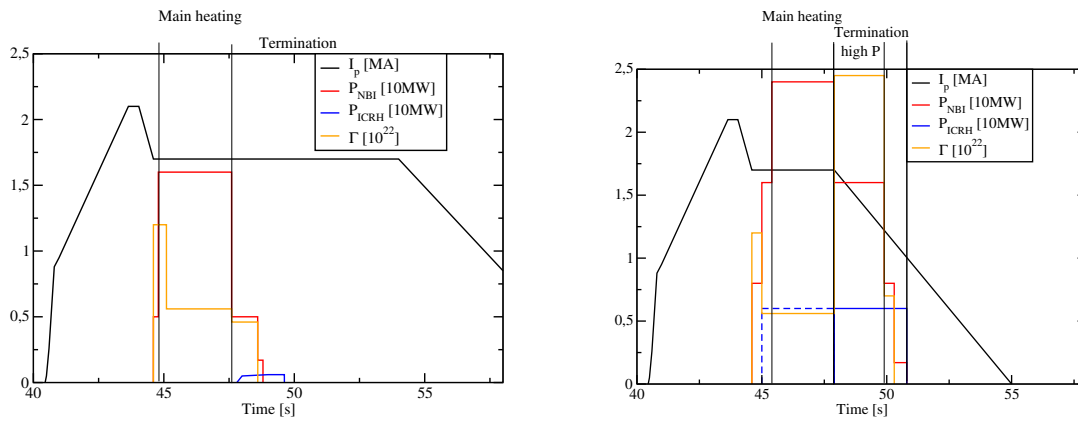
In figure 6 a-f the same data but reduced to the appropriate phase and sorted just on the data shown are plotted. In general there are two different sets of important data depending on the phase. In case of a low power tail or Ohmic the most important parameters are connected to the electron temperature, radiation, ICRH power and W source as can be seen in figure 6-b. During any of the high power phases the magnetic field, the energy confinement, the NBI power deposition to the electrons and the gas flux are main players but also a tendency can be

seen that radiation peaking remains important. In general the further away from the Ohmic phase the data are taken the lower the correlation to the Ohmic phase is. This sounds trivial but in the end it means that the plasma does not have a long memory for events and the quality of the termination is mainly determined by the design of the termination phase.

In table 2 the three most positive and three most negative correlations for all 7 phases are summarised. The data have been selected to reduce the number of strongly related parameters.

## 5. Proposed new termination scenario

The data gathered in this database indicates that events which happen closer to the termination of the plasma are more important than events earlier - or in other words by choosing the right termination we might be able to repair damage which has occurred earlier, e.g. by impurity



**Figure 7.** “Traditional” landing scheme on the left (before 2014) and suggested new landing scheme on the right (partially tried in 2015/16)

events, MHD or generally impurity accumulation. On the other hand there are some examples in the database where the plasma during the main heating phase is quite healthy but still develops a locked mode later due to a wrong termination. Based on this assumption a revised termination scenario has been proposed and partially explored. As a first step the heating power is reduced compared to the main heating phase while keeping or increasing the ICRH power because the remaining power has to provide enough absorbed power in the centre to compensate the radiation losses. The power reduction can probably not be strong enough on JET to go out of H-mode. At the same time the gas fuelling is increased and the strike points are moved onto the vertical target. The vertical target is chosen to avoid overheating of the divertor target used and the high gas fuelling reduces the temperature and increases the ELM frequency which has been identified as critical parameter in baseline discharges [12]. The high central power density prevents a flattening of the temperature profile. In addition the lowered input power and increased gas flux will reduce the energy confinement time. The second step would reduce the NBI heating power and the gas fuelling drastically and keeps the ICRH power on. In this phase the density and the W source should reduce while the central heating is supposed to control the impurity peaking. As a last step the Ohmic phase will be at

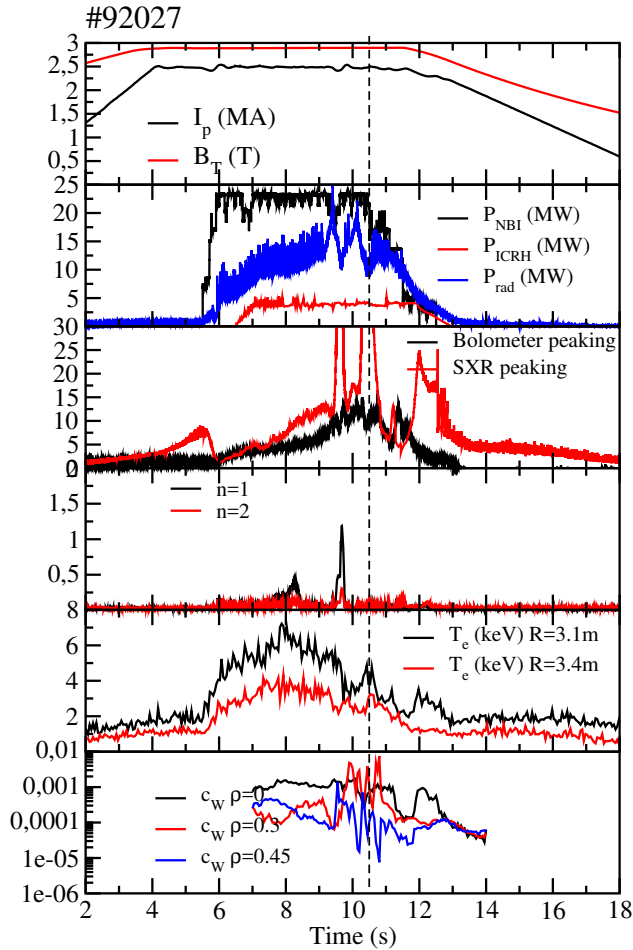


Figure 8. Overview of a new hybrid termination

zero feed forward gas fuelling but density feedback control set to a low density to avoid error field locked modes and density limit disruptions. The plasma current would be ramped down during all termination phases to reduce the chance of an existing locked mode to trigger a disruption and generally to reduce the energy in the plasma and the possible disruption forces.

The new landing scheme was partially tried in the campaigns 2015/2016. But it was not always possible to stick to the described scheme for technical reasons. Therefore the free parameters like the length of termination phase, the remaining heating power or the right gas level could not be optimised. Nevertheless the locked mode ratio has been reduced from 63% to 45%. Even though higher current and higher heating power plasmas were run. It was felt more difficult to terminate the higher current plasmas cleanly even though this difficulty is not visible in the statistics. An example of a new termination is shown in figure 8. The figure is organised as figure 1. The example chosen here is at the highest current of  $I_p = 2.5\text{MA}$  which has been used so far in the hybrid development at the nominal  $q_{95}$ . The radiation fraction is already much higher in the main heating phase compared to the example discussed earlier. The SXR peaking factor is above 10 already at  $t = 8\text{s}$  and has a strong first peaking at about  $t = 9.5\text{s}$  caused by an impurity influx (can be seen on the radiation power) and a loss of regular ELMs at  $t = 9\text{s}$ . At about  $t = 10\text{s}$  another impurity influx with a subsequent strong

peaking phase is visible. As can be seen in row 6 on the W concentration a strong ( few times  $10^{-3}$ ) off-axis enrichment at about half radius follows shortly afterwards. The NBI power is partially lost at  $t = 10.5$ s which is very similar to the proposed termination scenario but the current ramp and the strike point position change happen only at about  $t = 12$ s. Differently to the example discussed in the introduction here the radiation stays mostly below the applied heating power and the bolometric radiation peaking decays towards the low power phase. The ICRH heating is kept at high power levels until  $t = 12$ s. The gas injection is controlled in a real time feedback on the ELM frequency and increases at  $t = 10.3$ s by 100%. In this case the radiation peaking reduces before the heating power is switched off and the electron temperature profile remains peaked. No  $n=1$  mode is excited and therefore no locking is observed. The increase of the electron temperature at  $t = 12$ s leads also to an increase in SXR signal. At the same time the plotted SXR peaking and the W concentrations are increasing without an obvious reason. This indicates that the measurement between  $t = 11$ s and  $t = 12$ s is probably not trustworthy and the SXR peaking and the W concentrations are still large in this time interval.

## 6. Summary and conclusion

A novel way of analysing the termination of JET hybrid plasmas is presented. The first finding is that the occurrence of locked modes and with about 50% chance a disruption is connected to an increased radiation fraction after reducing the heating power. After switching off the heating power completely a radiation peaking in the Ohmic phase leads to a flattening or reversing of the temperature profile which in turn leads to an increase in central  $q$  and to shear reversal. Next a 2/1 MHD mode is triggered and most often locks shortly afterwards. In the created database a threshold value for the radiation peaking in the Ohmic phase can be given above which the probability of generating a locked mode is larger than 75%. The radiation peaking in the Ohmic phase is the best parameter in this database linked to the occurrence of locked modes. It is therefore used as a reference for a correlation analysis with 54 parameters in 7 phases of the discharge. The correlation analysis highlights parameters as most important which are consistent with the picture of a radiation driven  $q$ -profile change as the dominating effect to generate locked modes. It shows as well that the parameters closer in time to the start of the termination are having higher correlation coefficients and therefore are more important. This indicates that a good landing procedure might be able to terminate pulses safely even if they are not healthy during the main heating phase. A new termination procedure has been proposed and partially implemented. As a measure of success the locked mode probability has reduced from 63% to 45% afterwards. Not understood in this context is that the disruption probability has increased from 13% to 21%. The termination procedure is not yet optimised and further improvements are possible.

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## **References**

- [1] Hobirk J *et al.* 2012 *PPCF* **54** 095001
- [2] Gruber O *et al.* 1999 *Phys. Rev. Lett.* **83** 1787
- [3] Wolf R C *et al.* 1999 *Plasma Phys. Control. Fusion* **41** B93
- [4] Staebler A *et al.* 2005 *Nucl. Fusion* **45** 617
- [5] Luce T C *et al.* 2001 *Nucl. Fusion* **41** 1585
- [6] Luce T C *et al.* 2004 *Physics of Plasmas* **11** 2627
- [7] Joffrin E *et al.* 2008 *Proceedings of the 22nd IAEA Fusion Energy Conference* (Geneva, Switzerland)
- [8] de Vries P C *et al.* 2014 *PoP* **21** 056101
- [9] Hobirk J *et al.* 2014 *Europhysics Conference Abstracts, Proc. 41st EPS Conference* Vol. 38F P1.003 (Berlin)
- [10] Pütterich T *et al.* 2013 *PPCF* **55** 12
- [11] Angioni A *et al.* 2014 *NF* **54** 12
- [12] Köchl F *et al.* 2016 *Proceedings of the 26th IAEA Fusion Energy Conference Ex/P6-16* (Kyoto, Japan)
- [13] Wade M R *et al.* 2005 *Nucl. Fusion* **45** 407
- [14] Sips A C C *et al.* 2007 *Nucl. Fusion* **47** 1485