

Efficiency and Mechanisms of Biochar Aerogel-Assisted Biodegradation of Taste and Odor Compounds in a One-Step Membrane Bioreactor for Rural Drinking Water Production

Original

Efficiency and Mechanisms of Biochar Aerogel-Assisted Biodegradation of Taste and Odor Compounds in a One-Step Membrane Bioreactor for Rural Drinking Water Production / Shu, Jingyu; Wu, Qidong; Ren, Xiaoyu; Tang, Peng; Chen, Guijing; Cheng, Xin; Chen, Chen; Tiraferri, Alberto; Liu, Baicang. - In: ACS ES&T ENGINEERING. - ISSN 2690-0645. - 4:2(2024), pp. 300-309. [10.1021/acsestengg.3c00233]

Availability:

This version is available at: 11583/2986690 since: 2024-03-10T10:56:46Z

Publisher:

AMER CHEMICAL SOC

Published

DOI:10.1021/acsestengg.3c00233

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1 In preparation for *ACS ES&T Engineering*

2 Date: *September 4, 2023*

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4 Efficiency and mechanisms of biochar
5 aerogels-assisted biodegradation of taste &
6 odor compounds in a one-step membrane
7 bioreactor for rural drinking water production

8 Jingyu Shu ^{a, b}, Qidong Wu ^{a, b}, Xiaoyu Ren ^{a, b}, Peng Tang ^{a, b}, Guijing Chen ^{a, b}, Xin
9 Cheng ^{a, b}, Chen Chen ^c, Alberto Tiraferri ^d, Baicang Liu ^{a, b, *}

10 ^a College of Architecture and Environment, Institute of New Energy and Low-Carbon
11 Technology, Sichuan University, Chengdu, Sichuan 610207, PR China

12 ^b Yibin Institute of Industrial Technology, Sichuan University Yibin Park, Section 2,
13 Lingang Ave., Cuiping District, Yibin, Sichuan 644000, PR China

14 ^c Litree Purifying Technology Co., Ltd., Haikou, Hainan 571126, PR China

* Corresponding author.

Tel.: +86-28-85995998; fax: +86-28-62138325; e-mail: bcliu@scu.edu.cn;

baicangliu@gmail.com (B. Liu).

15 ^d Department of Environment, Land and Infrastructure Engineering, Politecnico di

16 Torino, Corso Duca degli Abruzzi 24, 10129 Turin, Italy

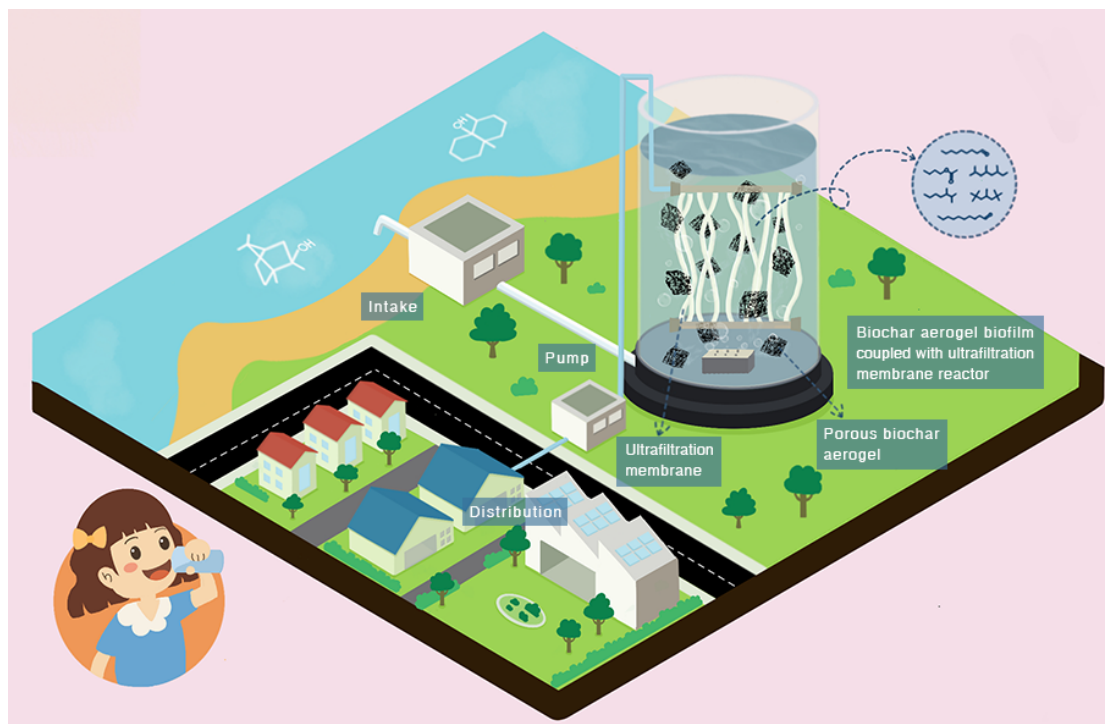
17

18 **Abstract:** In many rural areas, lakes and reservoirs represent common sources for
19 drinking water, but these water bodies are more likely affected by taste & odor problems
20 that cause discomfort to consumers. Taste & odor compounds, especially 2-
21 methylisobornol (2-MIB) and geosmin (GSM), are not easily removed using
22 conventional water treatment processes, and this problem is exacerbated in rural areas
23 where treatment systems are often sparser, modest, and dated compared to typical urban
24 water sources. Herein, a combined process deploying biochar aerogels-supported
25 biofilms and performed in an ultrafiltration reactor (BAB-UF) was evaluated and
26 investigated to treat rural water polluted with 2-MIB and GSM. During a 40-day
27 experiment, the system performance was analyzed at different values of the empty bed
28 contact time, while the microbial communities in different BAB-UF reactors were
29 examined extensively. The process proved to be effective in removing 2-MIB and
30 GSM, predominantly through biodegradation. Specifically, using biochar aerogels as
31 suspended fillers in the reactor and an EBCT of roughly 1 h, the removal rate of 2-
32 MIB/GSM was higher than 95%, and the effluent satisfied the requirements for
33 domestic drinking water. Microorganisms with specific functions were enriched in
34 different BAB-UF reactors and governed the transformation process, highlighting the
35 importance of system tuning for achieving the desired biological function, hence
36 product water quality.

37 **Keywords:** Biochar aerogel; Geosmin (GSM); 2-methylisobornol (2-MIB); Microbial
38 community; Rural drinking water treatment.

39 **Synopsis:** This study proposes and analyzes a combined process of biotransformation
40 and selective filtration to produce safe drinking water from rural reservoir water
41 polluted with taste & odor compounds.

42 **TOC/Abstract Art:**



43

44

45 1. Introduction

46 Drinking water quality in rural areas is a global concern. Currently, approximately 2.2
47 billion people, particularly those living in remote rural areas, e.g., mountainous,
48 pastoral, and forest areas, do not have access to safely managed or high-quality
49 drinking water.^{1,2} For example, according to a national Chinese survey, about 80% of
50 water bodies in China have taste & odor issues, particularly, lakes and reservoirs that
51 serve as main water sources in rural areas.³ Human life depends on access to clean,
52 safe drinking water, and consumers instinctively avoid water that tastes or smells
53 unpleasant because this characteristic may be an indicator of a harmful supply.⁴⁻⁶ The
54 terpenes, 2-methylisobornyl (2-MIB, C₁₁H₂₀O) and geosmin (GSM, *trans*-1,10-
55 dimethyl-*trans*-9 decanol-C₁₂H₂₂O), originate from the metabolism and
56 biodegradation activity of certain types of cyanobacteria^{7,8} and they have been
57 identified in water supplies as key odorants of the musty/earthy group.⁹ The
58 concentrations of 2-MIB and GSM in water can be perceived by the human nose at
59 concentrations as low as 6 ng/L⁴ and 4 ng/L¹⁰, respectively.

60 Studies have shown that 2-MIB/GSM are not removed to concentration values
61 below their odor threshold concentrations by conventional drinking water treatment
62 processes consisting of coagulation-flocculation, sedimentation, and filtration.^{8, 11, 12}
63 Treatment methods that have been successfully employed by centralized water
64 treatment plants to remove 2-MIB/GSM include granular activated carbon (GAC)
65 adsorption and advanced oxidation processes (AOP)¹³. Several researchers have

66 demonstrated the use of oxidants, such as ozone and hydrogen peroxide, and the use of
67 ultraviolet light (UV) for the removal of 2-MIB/GSM¹⁴⁻¹⁶. However, these methods
68 have limitations for rural water treatment. For instance, activated carbon has a limited
69 adsorption capacity and needs to be replaced frequently for capacity regeneration. In
70 addition, adsorption is strongly influenced by the presence of natural organic material
71 (NOM) in natural water.¹⁷ NOM is generally present in much higher concentrations
72 (mg/L) compared to T&O compounds (ng/L). The various fractions of NOM occupy
73 some adsorption sites and cause inhibition of adsorption of target odor substances. Also,
74 large NOM molecules may block the diffusion pathway of odorants and thwart
75 transport toward the adsorption sites¹³. As a result, high doses of activated carbon are
76 required for successful removal of the T&O compounds. Most rural drinking water
77 supply systems have lower capacity than urban systems, are managed by operators with
78 typically less professional experience compared to those operating in urban areas,¹ and
79 the addition of costly chemicals or complicated operating procedures associated with
80 adsorption and advanced oxidation processes would require sustained management and
81 maintenance that are not compatible with such rural systems. A simpler approach,
82 characterized by less complexity and requiring minimum skilled oversight, would
83 benefit water supply in rural areas.

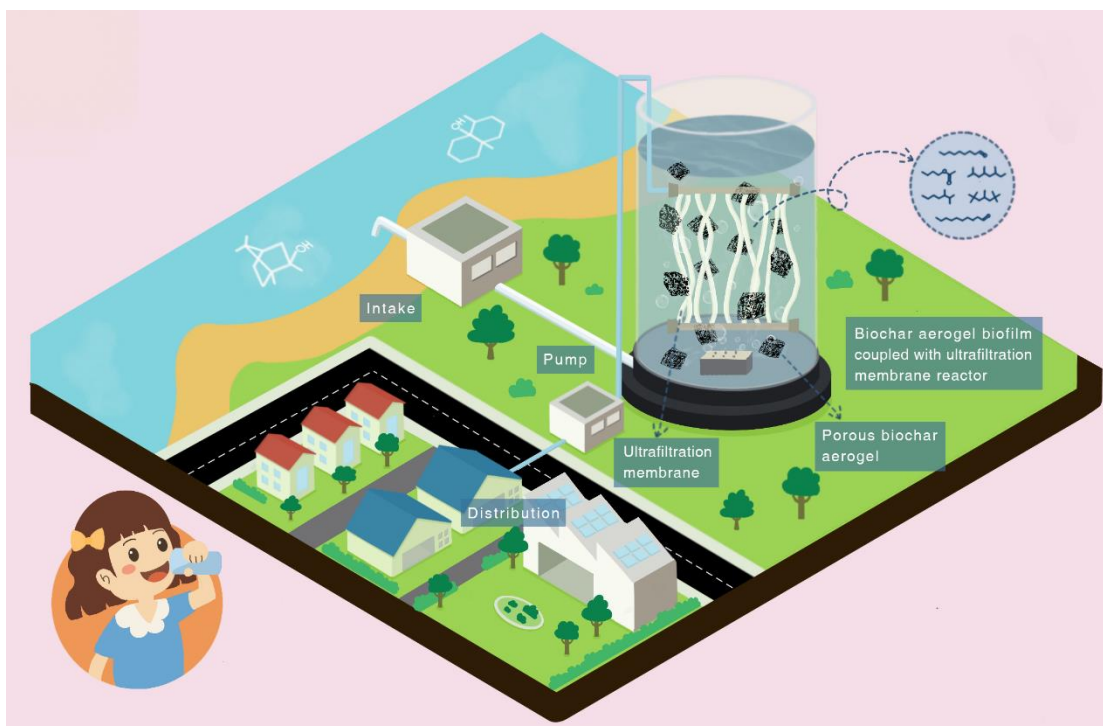
84 Biological processes play an important role in the future of drinking water
85 treatment, especially for developing countries, due to their environmental friendliness.
86 Biological drinking water treatment relies on the activity of non-pathogenic bacteria for

87 biochemical degradation, and to the ability of these microbes to produce a biologically
88 stable water that prevents the growth of other pathogenic microorganisms in the water
89 distribution system.¹⁸ These processes remove pollutants with minimal technological
90 complexity, require the addition of little or no chemicals, and limit the creation of by-
91 products that may be toxic or harmful for humans or the environment. Common
92 biological technologies include slow and rapid sand biofiltration (SSF/RSF), biological
93 activated carbon (BAC), and biological aerated filter (BAF).^{7, 19} For example, BAC
94 consists of microbes attaching and growing on the GAC surface to form a biofilm,
95 which removes contaminants as water filters through the media, thus exploiting
96 adsorption and biodegradation simultaneously, and extending the GAC service life.^{20,}
97 ²¹ Biosand and BAC depth filtration, as well as their aerated counterpart (BAF), are
98 effective methods for removing low molecular weight organic compounds and are
99 becoming widespread processes for advanced water treatment in large urban water
100 supply systems also in developed countries (such as Japan, the Netherlands, the United
101 States).^{22, 23}

102 A possible biological treatment alternative consists of a combined process
103 whereby biological activated carbon is used within a membrane bioreactor. In such a
104 configuration, the biologically-active media are suspended as fillers in the aerated raw
105 water and the product water is extracted through membrane filtration. It has been
106 suggested that such system would improve the quality of treated water and also help
107 alleviating membrane fouling.^{24, 25} Since membrane filtration can intercept most of the

108 suspended solids, microorganisms, and macromolecules in water,^{26, 27} and since it can
109 be applied in rugged mountain areas to meet drinking water treatment needs of remote
110 areas,²⁸ the hypothesis of this study is that the combination of biological treatment and
111 ultrafiltration should provide a **simple and easy-to-operate** way to solve odor problems
112 associated with 2-MIB and GSM in rural drinking water systems. To date, little or no
113 research has been conducted on these processes, resulting in a substantial lack of
114 knowledge related both to the engineering and to the underlying mechanisms
115 characterizing the related systems.

116 This study investigates the use of activated carbon-assisted biological degradation
117 combined with an ultrafiltration bioreactor to address T&O issues in rural drinking
118 water. To reduce the adsorption of NOM on the support carbon material, biochar
119 aerogels were used as suspended biological fillers to form an aerogel-supported biofilm
120 (BAB). **A schematic diagram of the combined one-step process (BAB-UF reactor) is**
121 **shown in Figure 1.** Specifically, this study examines: (1) the treatment performance of
122 rural reservoir water containing 2-MIB and GSM via four different BAB-UF reactors;
123 (2) the biodegradation rates of 2-MIB and GSM; (3) the possible pathways of
124 biodegradation of 2-MIB and GSM; (4) the efficiency and potential of the system for
125 drinking water treatment; (5) the microbial communities developing in the reactor and
126 their role on treatment performance.



127

128 **Figure 1.** The schematic diagram of the combined one-step process (BAB-UF reactor)

129

130 2. Material and Methods

131 2.1. Materials.

132 Water from a reservoir in Zhong county (Chongqing, China) was used as
 133 experimental water. Wahaha brand bottled water was used for the establishment of 2-
 134 MIB/GSM standard curves and for blank control experiments. A standard mixture of 2-
 135 MIB (trace CERT[®]) and GSM (trace CERT[®]) was purchased from Sigma-Aldrich ¹³.
 136 Sodium chloride (NaCl, 98% purity), potassium hydroxide (KOH, 90%), acetic acid
 137 (CH₃COOH, 99.5% purity), and sodium azide (NaN₃, 99%) were provided by Agilent
 138 Technologies (China) Co., Ltd. Chitosan was purchased from Jinan Haidebe Marine
 139 Biological Engineering Co., Ltd. (China), and glucose was purchased from Chengdu
 140 Kelong Chemical Reagent Factory (China). The ultrafiltration hollow fiber membranes

141 used in this study were provided by Litree Purifying Technology Co., Ltd (Hainan,
142 China). Peristaltic pumps (BT-300-2 J, Longer Pump, China) were used to feed water
143 from the tanks to the BAB-UF reactors, as well as to extract effluents from the
144 ultrafiltration hollow fiber membrane modules.

145 **2.2. Methods**

146 **2.2.1. BAB-UF reactors set-up.**

147 The shallow sediment of the reservoir was collected for microbial enrichment, and
148 a 28-day acclimation process was required to allow microbial aggregation and biofilm
149 formation on the suspended fillers. **Specific details regarding the acclimation process**
150 **and associated data can be found in the Supporting Information (SI, Text S1 and Figure**
151 **S1-2).** Following the 28-day acclimation period, degradation experiments were initiated.
152 **Actual water from the reservoir mixed with 2-MIB and GSM at a concentration of 100**
153 **ng/L was used as the raw water (RW), which was supplied to all reactors simultaneously.**
154 Because odor problems are seasonal²⁹, with outbreaks typically lasting about 1 to 2
155 months during the warm weather season, the study was conducted in the laboratory for
156 40 days. Basic information of the different BAB-UF reactors is shown in **Table 1.**⁴
157 Concentrations of 2-MIB and GSM were measured every three days for 33 days in the
158 influent and effluent streams from the BAB-UF reactors. After the systems achieved
159 stability, the concentration of odorant was gradually increased from 100 ng/L to 200
160 ng/L.

161 **Table 1.** Operating parameters of the BAB-UF reactors in this work.

Operators ID	Suspended Fillers	Flow rate (ml/min)	EBCT (min)	Gas-water ratio	Running Time (d)
UF	-	0.524	-	3:1	40
BAB-20-UF	BA	0.524	18	3:1	40
BAB-40-UF	BA	0.524	36	3:1	40
BAB-60-UF	BA	0.524	54	3:1	40

162 Note: The running time of the reactors only includes the degradation experiments period.

163

164 2.2.2. Experimental setup comprising biodegradation, adsorption and aeration in

165 BAB-UF

166 The following three control experiments were conducted on the 40th day of the
167 experiment when the influent 2-MIB/GSM concentration was 200 ng/L. In one control
168 experiment, only aeration was applied while the fillers and ultrafiltration membranes
169 were not present, to understand the rate of volatilization. In a second control experiment,
170 Wahaha purified water containing 300 mg/L sodium azide was used to soak the filler in
171 the BAB-UF device for 2 h, which inhibited the biological activity of the biofilm
172 without affecting other functions (e.g., adsorption).²⁰ A third control test was conducted
173 in which the membrane reactors operated simultaneously under the same conditions but
174 without aeration and without the presence of the ultrafiltration membrane. The four full
175 BAB-UF reactors were instead run at different empty bed contact time (EBCT) of 18,
176 36, 54 min and contained 20%, 40%, and 60% fillers, respectively. In all cases, we
177 measured the influent 2-MIB/GSM concentrations and the effluent concentrations three

178 times, and for each setup we calculated the average effluent concentration as a
179 percentage of the influent concentration to obtain the removal rate of 2-MIB and GSM.
180 The biodegradation contribution in the full BAB-UF reactors was obtained by
181 subtracting the aeration and adsorption rates from the total BAB-UF removal rate.

182

183 **2.2.3. Preparation of biochar aerogel fillers for biofilm support**

184 The biochar adsorbent powder was prepared using the sol-gel method;³⁰⁻³² refer to
185 the SI (**Text S2**) for a detailed description of the method. The method of BAB aerogel
186 production was adapted from previous research³³ and comprised with the following
187 steps: chitosan powder with a mass concentration of 4.0 wt% was dissolved in 1.0 wt%
188 aqueous glacial acetic acid solution by stirring, resulting in a yellow transparent
189 homogeneous solution. The previously prepared 0.1 wt% biochar adsorbent powder was
190 added to the chitosan solution and stirred for 30 min to ensure even dispersion. The
191 mixture was then injected quickly **with a syringe into a cylindrical mold about 7 mm**
192 **height and about 5 mm in diameter**, and then rapidly frozen at -20°C before being
193 freeze-dried for 24 h. The resulting dried granular aerogel was removed from the mold
194 and placed in a 4 wt% aqueous NaOH solution, where it was shaken for 2 h at room
195 temperature to fully react and neutralize the acid in the aerogel. Finally, the pellet
196 aerogels were washed with pure water until neutral pH to obtain the final BAB supports.

197 **2.3. Analytical methods**

198 **2.3.1. 2-MIB and GSM analysis**

199 The concentrations of 2-MIB and GSM were analyzed using a gas
200 chromatography-mass spectrometry (GC-MS) system, which was coupled with a solid
201 phase micro-extraction (SPME) fiber holder and SPME fiber assembly-
202 divinylbenzene/carboxen/polydimethylsiloxane (DVB/CAR/PDMS). An Agilent 8890
203 Series gas chromatograph equipped with an HP-5 MS capillary column (30 m × 0.25
204 mm × 0.25 mm film thickness) interfaced to an Agilent 7010B mass selective detector
205 was used. To quantify the 2-MIB/GSM, 35 mL of water sample and 3.5 g of NaCl baked
206 at 300 °C in a muffle for 2 h were mixed evenly into a 40 mL brown headspace bottle.
207 The bottle was placed into a 65 °C water bath for preheating, and extraction was carried
208 out for 15 min. The extraction head was then inserted into a GC injection port for 5 min
209 for quantitative analysis of 2-MIB/GSM. The carrier gas was high purity He (99.999%,
210 Rising Corp., China) at a column flow rate of 1 mL/min. The injection port operated in
211 a separation mode with split ratio of 20:1 while the temperature maintained at 250 °C.
212 The column oven initial temperature was set at 60 °C for 2.5 min, increased to 250 °C
213 at a rate of 10 °C/min, and then maintained for 5 min. The MS ion source temperature,
214 the four-stage rod temperature, and the auxiliary heating zone temperature were
215 maintained at 230 °C, 150 °C, and 280 °C respectively. The solvent delay was set to 7.5
216 min. The MS ionization energy was set to 70 eV, and the scanning mode was set at
217 multiple reaction monitoring (MRM). The quantitative ion pair parameters are 95/67

218 for 2-MIB,112/97 for GSM. Standard chromatograms and 1-200 ng/L 2-MIB/GSM
219 standard curves are presented in the SI (**Figure S4**).

220

221 **2.3.2. Effluent quality analysis**

222 A portable multifunctional Ultrameter II 6PFC (Myron L Company, Carlsbad,
223 USA) was utilized to determine the total dissolved solids (TDS). COD_{Mn} was
224 determined based on the permanganate index (GB 11892-89). DOC and UV₂₅₄ values
225 were obtained, respectively, with a TOC analyzer (TOC-L CPH, Shimadzu, Japan) and
226 with a UV-vis spectrophotometer (Orion AquaMate 8000, Thermo Fisher, USA). The
227 pH was measured using a pH meter (PB-10, Sartorius Scientific Instruments Co, Ltd.,
228 Gottingen, Germany), while turbidity was measured using a turbidimeter (2100Q, Hach
229 Company, Loveland, USA). A three-dimensional excitation-emission matrix (3D EEM)
230 fluorescence spectrum (F-7000, Hitachi, Japan) was used to characterize the DOM
231 components in the effluent and on the membrane contaminated layers. For detailed
232 information on the related methods, please refer to our previous studies.^{34,35}

233 **2.3.3. 16S-rRNA analysis**

234 The microbial diversity of the biofilm formed on the suspended fillers in the
235 continuous mode BAB-UF reactor at different times was sequenced using 16S-rRNA
236 to analyze changes in microbial communities and dominant functional microorganisms
237 over time. In the four BAB-UF reactors, a total of six BAB filler samples and two
238 sections of ultrafiltration membrane samples were collected on days 10 and 40. For

239 each BAB filler sample, 2 g of packing material from approximately the middle depth
240 of the reactor was taken and placed into a sterilized 10 mL polyethylene bottle. The
241 sample was then transported to the analytical laboratory on ice packs, while an equal
242 volume of packing was backfilled immediately after removal. The detailed operation
243 method of 16S-rRNA can be found in the SI (**Text S4**).

244 **2.3.4. Membrane fouling analysis**

245 The membrane fouling layer morphology was examined with scanning electron
246 microscopy (SEM, Regulus 8230, Hitachi, Japan) on membrane samples after their use
247 in the reactor. Before SEM analysis, the dried sample surfaces were coated with Au by
248 a model MS-2S gold coating instrument (IXRF Systems Inc., USA), reaching a
249 thickness of approximately 2 nm.

250

251 **3. Results and Discussion**

252 **3.1. Biodegradation is the dominant removal mechanism of 2-MIB and GSM**

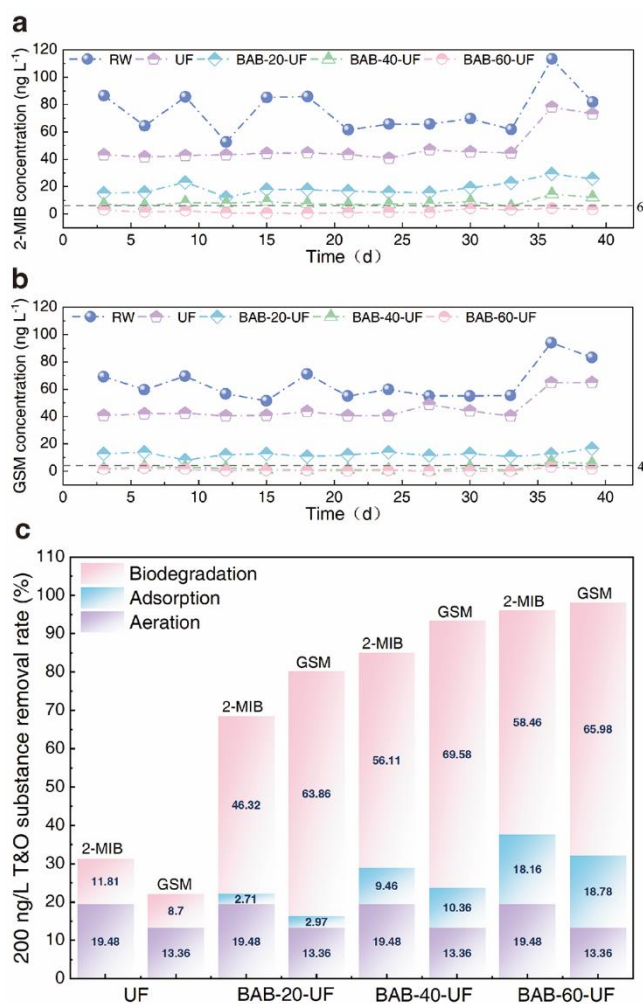
253 In this study, a fraction of 2-MIB/GSM was lost due to natural volatilization since
254 the experimental device could not be kept sealed (due to continuous aeration, the
255 pressure in the reactor would increase if it was completely sealed, resulting in increased
256 water flow resistance and reduced water flow velocity). The results of the control
257 experiments suggested that the fractions of volatilized 2-MIB and GSM were 32.4%
258 and 42.3%, respectively, at a starting concentration of 100 ng/L, while 56.25% and

259 61.01%, were lost at a starting concentration of 200 ng/L. These losses were accounted
260 for when computing raw water concentrations and in the following calculations.

261 By observing the influent and effluent concentrations 2-MIB/GSM from the four
262 BAB-UF reactors throughout 40 day of testing, it is clear that the removal efficiency
263 increased with EBCT; see **Fig. 2a, b**. For example, the effluent 2-MIB/GSM
264 concentrations were 6 and 4 ng/L, respectively, from BAB-40-UF and BAB-60-UF,
265 hence lower than the human nose perception threshold and attaining values that respect
266 the local standards for drinking water quality (GB 5749-2022). Note that the removal
267 rate obtained in the control experiments comprising the UF membrane only was around
268 or lower than 30%, due to the small molecular size of the two T&O compounds that
269 cannot be excluded from entering and moving across the membrane pores. **Such**
270 **removal rates recorded in the control experiment are attributed to the presence and**
271 **activity of bacteria on the ultrafiltration membrane. These bacteria were remnants from**
272 **the initial acclimation phase conducted prior to the commencement of the control**
273 **experiment.**

274 The contribution of aeration, adsorption, biodegradation to the overall 2-
275 MIB/GSM removal rate is presented in **Fig. 2c**. Aeration was responsible for 19.5%
276 and 13.4% of the total removal of the two substances. The adsorption removal rates
277 were instead 2.7%, 9.5%, and 18.2% for 2-MIB and, quite similarly, 3.0%, 10.4%, and
278 18.8% for GSM, from the three reactors characterized by EBCT 18, 36, 54,
279 respectively. Indeed, the contribution of biodegradation was dominant and estimated as

280 follows: UF only (11.8%, 8.7%), BAB-20-UF (46.3%, 63.9%), BAB-40-UF (56.1%,
 281 69.6%), BAB-60-UF (58.5%, 66.0%). The findings indicate that the process of
 282 adsorption did not provide substantial removal, possibly due to the chemical nature and
 283 to the low concentrations of 2-MIB and GSM. On the other hand, biodegradation
 284 contributed to around 60% of the overall removal rate, which aligns with the
 285 conclusions drawn by earlier research⁷, and represented the dominant removal
 286 mechanism in the examined system.



287
 288 **Figure 2.** Removal rates of T&O compounds: (a) 2-MIB concentrations and
 289 corresponding removal rates in different reactors: the grey line indicates the 2-MIB

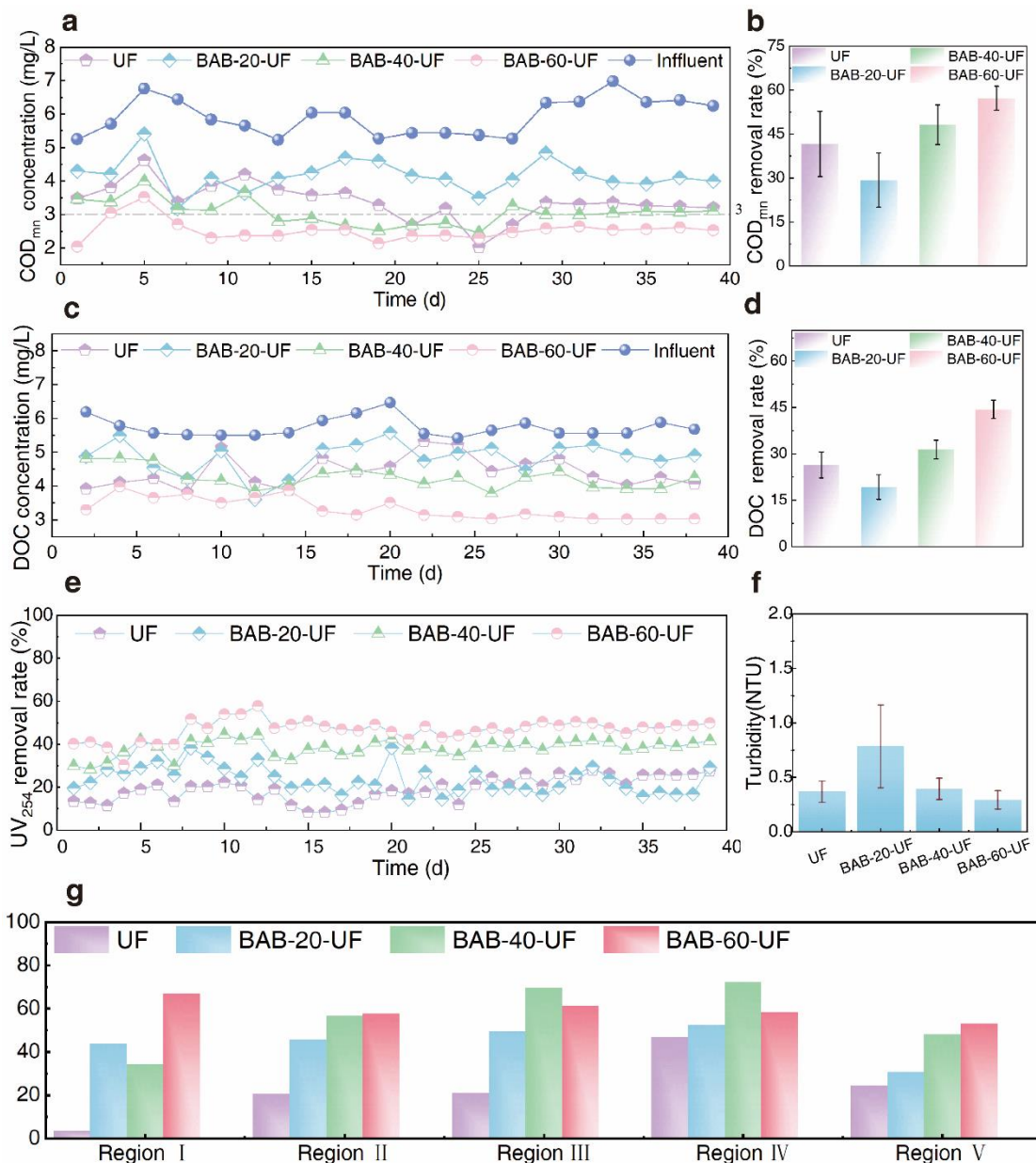
290 odor threshold in water at 6 ng/L; (b) GSM concentrations and corresponding removal
291 rates in different reactors: the grey line indicates the GSM odor threshold in water at 4
292 ng/L; (c) contributions to removal rates from different mechanisms. RW refers to the
293 reservoir water containing 2-MIB/GSM.

294

295 3.2. The effluent from the BAB-UF systems met local drinking water standards

296 The water quality parameters of influent and effluent streams from different BAB-
297 UF reactors are displayed in **Fig. 3**. The COD_{Mn} of effluents from BAB-60-UF and
298 BAB-40-UF were below 3 mg/L, thus meeting local drinking water standards
299 (GB5749-2022); see **Fig. 3a, b**. Specifically, the COD_{Mn} removal efficiency was higher
300 than that of the UF device alone, suggesting that BAB adsorbed and/or biodegraded
301 part of organic compounds. Considering DOC, the average removal rate increased by
302 roughly 12% with each doubling of EBCT, achieving approximately 44% in BAB-60-
303 UF (**Fig. 3c, d**). Other than removal rate itself, the stability of removal was apparently
304 higher for reactors characterized by longer EBCT. A similar trend was also observed
305 for the UV_{254} parameter, which can be used to quantify the amount of dissolved
306 organic pollutants with unsaturated bonds in the raw water. As shown in **Fig. 3e**, the
307 removal of UV_{254} was between approximately 19.0 (BAB-20-UF) and 46% (BAB-60-
308 UF). The fact that the removal rate of UV_{254} was higher than that of DOC indicates that
309 the BAB-UF reactor more efficiently degraded unsaturated organic and aromatic
310 compounds.

311 Turbidity and TDS were used as additional indicators related to the quality of
 312 drinking water. As shown in **Fig. 3f** and consistent with the removal behavior of
 313 organics, the removal rates generally increased with EBCT and the average turbidity of
 314 the effluent of BAB-UF reactors was lower than 0.5 NTU, indicating higher than 90%
 315 removal rate of turbidity in all cases. Finally, the TDS did not change considerably,
 316 converting from 120-140 ppm in the RW to 100-130 ppm in the treated effluents, the
 317 minimal removal likely due to uptake by microorganisms for growth.



318

319 **Figure 3.** Water quality parameters of influent and effluent streams from different
320 BAB-UF reactors during 40-days. (a) COD_{Mn} concentrations; (b) corresponding
321 average removal rates of COD_{Mn} : here, the grey dotted line marks the local drinking
322 water standard limits for COD_{Mn} in the GB5749-2022 legislation; (c) DOC
323 concentrations; (d) corresponding average removal rates of DOC; (e) UV_{254} removal
324 rates; (f) average turbidity concentrations in the effluents. (g) Removal rates of
325 Fluorescence EEM spectra computed for different BAB-UF reactors.

326

327 Beside overall removal rates, the changes in the composition of DOC were
328 examined with fluorescence EEM spectroscopy. The EEM spectrum may be classified
329 into five regions: Region I : (Ex/Em = 220-250/280-330 nm, tyrosine protein-like
330 substances), region II : (Ex/Em=220-250/330-380 nm, tryptophan protein-like
331 substances), region III: (Ex/Em = 220-250/380-480 nm, fulvic acid-like matters),
332 region IV: (Ex/Em = 250-440/280-380 nm, soluble microbial by-product-like matters),
333 and region V: (Ex/Em = 250-400/380-540 nm, humic acid-like components).^{34, 36} As
334 shown in **Fig. S5e**, fulvic acid-like matters (region III), soluble microbial by-product-
335 like matters (region IV), and humic acid-like components (region V) were the main
336 organic constituents in the raw water, far more than tyrosine protein-like substances
337 (regions I and II). This observation is attributed to the fact that, similar to previous
338 studies, fulvic acid-like matters (region III) and humic acid-like components (region V)
339 are the major components of NOM in surface waters.³⁷ The removal efficiency of BAB-

340 UF for regions III and IV were the highest and most consistent for the different systems,
341 with removal rates higher than 50% observed for the two higher EBCT values for
342 regions II, III, IV, and V, consistent with the removal efficiency of COD_{Mn} and UV₂₅₄;
343 see **Fig. 3g**. This result implies that the BAB-UF reactors are especially apt to the
344 purification of hydrophilic low and medium molecular weight organic components,
345 which actually represent the largest fraction of organics in rural surface water sources,
346 such as lakes and reservoirs.

347

348 **3.3. Adaptation of the microbial community in BAB-UF systems**

349 All analyzed samples had coverage values greater than 0.99 (see **Text S4.2**) ,
350 indicating that the sequencing depth was sufficient to cover most microorganisms, even
351 some rare species.^{35, 38} The flattening of the rarefaction curve in **Fig. 4a** also indicates
352 sufficient sequencing depth. The combined result imply that the community richness
353 and diversity of the 40th day samples was higher than that of the 10th day samples.

354 **Fig. 4b** and **c** show the microbial community composition at the genus level
355 (relative abundance > 0.05% in all samples) and at the phylum level (relative abundance
356 > 0.1% in all samples), respectively. Similar to previous studies using BAF or other
357 methods for drinking water treatment,^{28,39} *Proteobacteria* were the most abundant and
358 broad in all samples (in this study, 40%-88% of the samples on the 10th day, and 51%-
359 93% of the samples on the 40th day). Another dominant phylum was *Bacteroidetes*,
360 which are well-known degraders of organic matter.⁴⁰ The above two phyla, together

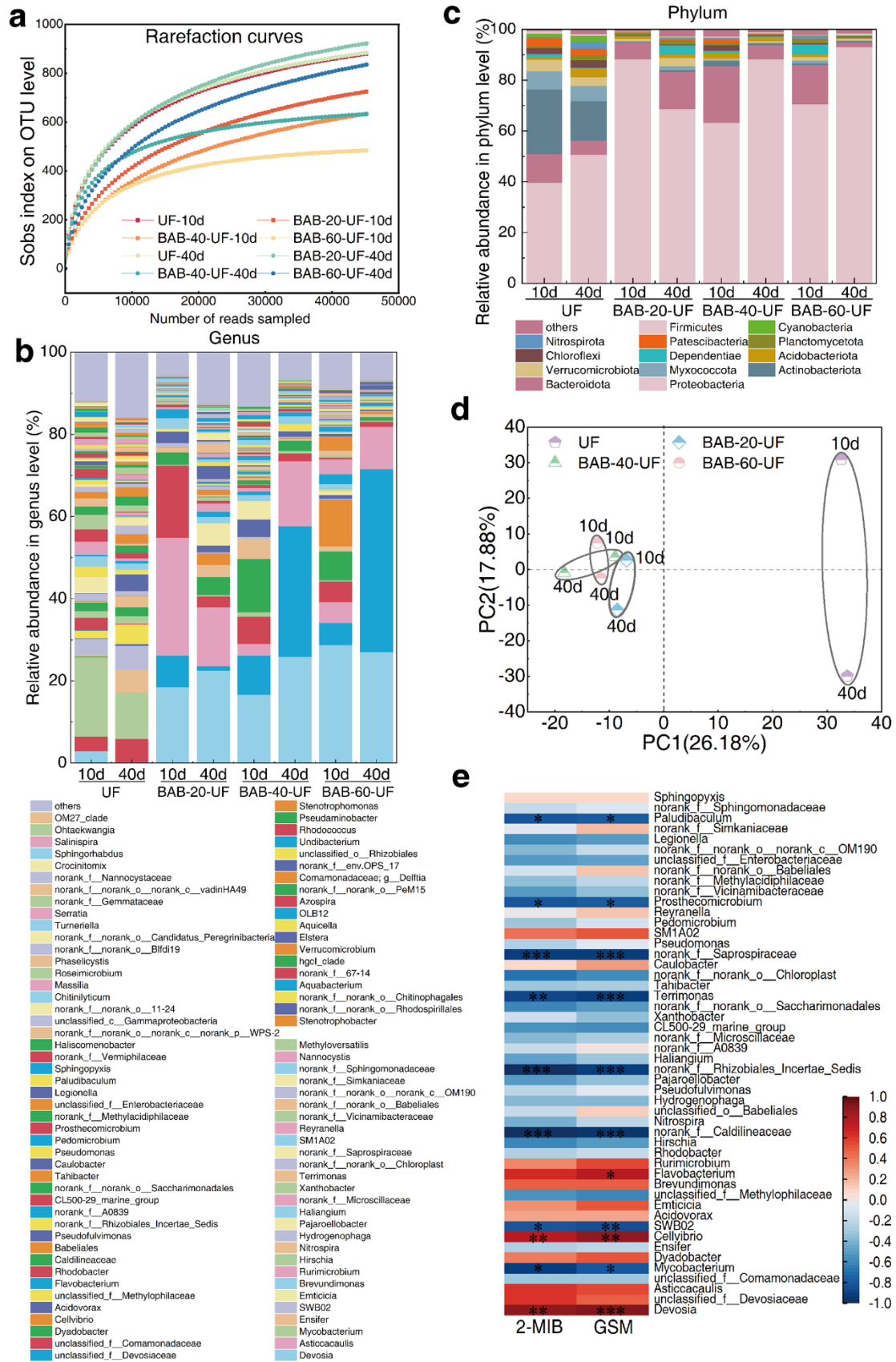
361 with *Actinobacteriota*, *Myxococcota* and *Verrucomicrobiota*, accounted for more than
362 81% of the community.

363 Principal component analysis (PCA) of OTUs levels of microbial communities in
364 different BAB-UF reactors (**Fig. 4d**) provides information on the similarity of the
365 bacterial community structure between the four reactor samples and the effect of
366 different operating times on the bacterial community structure. The bacterial
367 community structures of BAB-20-UF, BAB-40-UF, and BAB-60-UF were similar,
368 whereas the bacterial community structures of the reactors using ultrafiltration alone
369 showed substantial differences. This result may be mainly attributed to the fact that the
370 ultrafiltration membrane is not suitable for microbial attachment and growth compared
371 to fillers and that it has a relatively poor ability to absorb substances from the influent
372 water. The results also imply that materials with strong bioattachment capabilities may
373 play an important role in acclimating stable microbial communities. While there were
374 some differences in the bacterial community structure across the three BAB-UF
375 reactors, the essential microorganisms were comparable. According to the data plotted
376 in Fig. 4c, these core microbes were *Devosia*, *unclassified_f_Devosiaceae*,
377 *Asticcacaulis*, *Unclassified_f_Comamonadaceae*, *Dyadobacter*, *Ensifer* and *Cellvibrio*,
378 all belonging to *Proteobacteria* and *Bacteroidetes*, indicating that a large number of
379 microorganisms potentially capable of degrading organic matter were adapted and
380 retained in the biofilm-rich systems.

381 To further investigate microorganisms activity for 2-MIB/GSM removal,
382 correlation analysis (**Fig. 4f**) was performed between the 2-MIB/GSM removal rate
383 and the genus-level microbial community (top 50 genus in abundance). The results
384 suggest that *Devosia* with abundance of 0.2% to 26% was positively correlated with
385 substance removal ($p < 0.01$ and $p < 0.001$ for 2-MIB and GSM, respectively). It has been
386 reported that *Devosia* isolated from enriched bacterial cultures showed effective
387 degradation of alcohols, e.g., deoxynivalenol, whose molecular structure is similar to
388 that of GSM.⁴¹ Degradation enzymes in *Devosia* may belong to the aldo-keto reductase
389 (AKR) family.⁴² *Cellvibrio* (0.9%-13%) were also positively correlated with the
390 removal rates of 2-MIB and GSM ($p < 0.05$ and $p < 0.01$, respectively), but its
391 mechanistic contributions requires additional research. Finally, *Flavobacterium* (0.2%-
392 2.4%) had a significant correlation with the GSM removal rate ($p < 0.05$). Yuan *et al.*
393 reported that the ability of *Flavobacterium* to remove 2-MIB with an initial
394 concentration of 515 ng/L reached 96.3%.^{7, 19} According to the correlation analysis
395 results of this study, *Flavobacterium* may also contribute to the degradation of GSM,
396 but further studies are needed to prove this hypothesis. It is worth noting that
397 *Pseudomonas*, *Sphingomonas sp.* were found in the four groups of BAB-UF reactors,
398 and it has been pointed out that these two bacteria are likely to participate in the
399 biodegradation of 2-MIB and GSM.^{7, 19} Indeed, the abundance of *Pseudomonas* and
400 *Sphingomonas* in the BAB-UF reactors at 40 days was an order of magnitude higher
401 than that measured at 10 days, and also it increased with BAB filler amount,

402 corroborating previous reports. Note that the correlation analysis discussed above is
403 hypothetical and based on data obtained from the 16s rRNA assay. Additional
404 investigations will be conducted in future studies to test this hypothesis and the
405 relationships with other water elements will also be taken into consideration. Specific
406 microbiological tests will be conducted for each distinct bacterium in the water at the
407 appropriate 2-MIB and GSM concentrations.

408 In conclusion, after the completion of the acclimation phase, the microbial
409 communities in the different BAB-UF reactors were adapted to the raw water. After
410 long-term operation, *Proteobacteria* was dominant in all communities. It appears that
411 suspended fillers with robust biological affinity were able to acclimate stable microbial
412 communities, which in turn effectively broke down contaminants in water. In addition,
413 several microorganisms were found have a strong correlation with 2-MIB/GSM
414 removal, including *Devosia*, *Cellvibrio*, *Flavobacterium*, *Pseudomonas*, as well as
415 *Sphingomonas*. These correlations shall be further evaluated and quantified by future
416 studies.



417

418 **Figure 4.** Microbial community analysis in four BAB-UF reactors: a) OTUs-level

419 rarefaction curves at different operation times. Bacterial community compositions of
420 (b) genus (> 0.05%), (c) the phylum (> 0.1%) and (d) principal component analysis. (e)
421 are the correlation analysis of the above genus-level (top 50) microbial community and
422 2-MIB/GSM removal rate variables (“*” represents a value of $p < 0.05$, “**”
423 represents a value of $p < 0.01$ and “***” represents a value of $p < 0.001$).

424

425 **3.4 Biochar aerogel fillers slightly improved the membrane fouling behavior**

426 The morphology of the fouling layer on the membrane surface in various BAB-
427 UF reactors was analyzed with SEM; see representative micrographs and results in **Fig.**
428 **S8**. Surfaces were covered with a thick fouling layer. Interestingly, the fouling layer of
429 BAB-60-UF membranes was the thinnest among the aerogel-assisted reactors,
430 suggesting that EBCT ought to be no less than roughly 54 min to control fouling in the
431 investigated system. Therefore, the impact of aerogel was minor but not negligible, and
432 may deserve further study to understand how the presence of fillers might change the
433 interaction of microorganisms and organic matter with the membrane.

434

435 **ASSOCIATED CONTENT**

436 **Supporting Information**

437 Additional experimental materials, methods, and procedures for data processing;
438 discussion on DTPs and comparative analysis; and a number of other supporting
439 materials are provided in Texts S1–S5, Tables S1–S4, and Figures S1–S8.

440 **AUTHOR INFORMATION**

441 **Corresponding Author**

442 *E-mail: bcliu@scu.edu.cn; baicangliu@gmail.com. Tel: +86-28-85995998; Fax:
443 +86-28-62138325

444 Baicang Liu – College of Architecture and Environment, Institute of New
445 Energy and Low-Carbon Technology, Sichuan University, Chengdu 610207, P.R.
446 China

447 Notes: The authors declare no competing financial interest.

448 **ACKNOWLEDGMENTS**

449 This work was supported by the National Natural Science Foundation of China
450 (52270075, 52070134), Litree Purifying Technology Co., Ltd. (2021H012), Sichuan
451 University and Yibin City People's Government Strategic Cooperation Project
452 (2020CDYB-2), and Sichuan University from 0 to 1 innovation research of
453 transformative technology project (2022SCUH0042). A.T. acknowledges the support
454 of Politecnico di Torino. The views and ideas expressed herein are solely those of the
455 authors and do not represent the ideas of the funding agencies in any form.
456

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