

Dissipative Solitons in Microresonators

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(Article begins on next page)

# Chapter 9

## Dissipative solitons in microresonators

**Cristina Rimoldi, Bennet Fischer, Luigi Di Lauro, Mario Chemnitz, Alessia Pasquazi, David J. Moss, and Roberto Morandotti**

**Abstract** In this Chapter we will illustrate the state-of-art in the generation of dissipative solitons in Kerr microresonator-based systems. After a brief introduction on the origin of this field of research, we will discuss the modeling of these microcavities using the generalized Lugiato-Lefever equation. Further, we will discuss the different techniques used for dispersion engineering in these systems. We will then focus on the description of the frequency combs generated by microring resonators in the Kerr soliton regime and illustrate different schemes that have been developed in this context to grant better control of the microcavity dynamics. Finally, we will review the large number of applications that these objects have originated in several fields of optics.

### 9.1 Introduction

In the past 10 years, microresonators have revolutionized the field of optics with several applications in sensing [1–3], spectroscopy [4, 5], communication [6–9], astronomy [10, 11], and quantum optics [12–20]. These devices, generally featuring a high quality (Q) factor, can be realized under many forms, such as micro-toroids [21], spheres [22, 23], disks [24], rods [25], and integrated ring resonators [26, 27]. Further, they have been studied in many different materials, such as calcium [28] and magnesium [29] fluorides ( $\text{CaF}_2$ ,  $\text{MgF}_2$ , respectively), lithium niobate ( $\text{LiNbO}_3$ )

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C.Rimoldi · B. Fischer · L. Di Lauro · M. Chemnitz · R. Morandotti (✉)

INRS-EMT, 1650 Boulevard Lionel Boulet, Varennes, Quebec J3X 1S2, Canada

A. Pasquazi

Emergent Photonics (Epic) Laboratory, Department of Physics and Astronomy, University of Sussex, Brighton BN1 9RH, United Kingdom

D. J. Moss

Centre for Microphotonics, Swinburne University of Technology, Hawthorn, Victoria VIC 3122, Australia

e-mail: morandotti@emt.inrs.ca

[30], aluminum nitride (AlN) [31], tantalum pentoxide ( $\text{Ta}_2\text{O}_5$ ) [32], silica glass [33], diamond [34], silicon [26, 35], silicon nitride ( $\text{Si}_3\text{N}_4$ ) [36], oxynitrides ( $\text{Si-O}_x\text{N}_x$ ) [37], and high-index glass [38, 39], each offering specific advantages (and disadvantages) depending on the considered application. While these devices and materials have since been thoroughly investigated for the generation of frequency combs [40–42], the first direct demonstration of dissipative solitons in microresonators only dates back to 2014 [29], building upon the first experimental observation of Kerr solitons in a fiber cavity [43]. Kerr solitons arise from the mutual interplay of, on the one hand, dispersion and nonlinearity, and on the other hand, gain and losses. The resulting broadband frequency combs exhibit a high level of coherence, which is of fundamental importance for applications in spectroscopy, communications, and quantum measurements, as illustrated later in this Chapter.

Frequency combs, generated through cascaded four-wave mixing (FWM) in the microresonator blue-detuned regime, can exhibit either an aperiodic temporal waveform, due to arbitrary and constant phases of the comb lines, or coherent sidebands with a low repetition rate and reduced bandwidth [28, 44]. In contrast, soliton frequency comb lines display synchronized phases with higher repetition rates and bandwidths, thus resulting in an extremely narrow pulsed temporal shape [29, 45, 46]. Differently from solitons generated through mode-locked laser techniques exploiting incoherent pumping schemes, Kerr soliton frequency combs present the pump frequency within their spectrum and their generation does not make use of saturable absorbers for stabilization [47, 48]. The first experimental demonstration of dissipative Kerr solitons (DKSs) in microresonators [29] was performed in an  $\text{MgF}_2$  crystal driven by a continuous wave (CW) pump laser. Here, solitons were observed when the optical system undergoes the transition between the effectively blue- and red-detuned regimes. In particular, while scanning for decreasing values of pump frequency, the system first displays primary sidebands in the frequency domain due to FWM, which are then followed by secondary lines. When the broadband radio-frequency (RF) signal transitions to a low-noise beatnote, a series of discrete steps in the transmission is observed and identified as a clear sign of the generation of Kerr solitons, which were then temporally characterized by the authors through frequency-resolved gating (i.e. FROG measurements). While for the general description of the microresonator system dynamics we refer the reader to [49], in the following we are going to discuss the details of the most used modeling approaches.

## 9.2 Modeling

The generation of dissipative Kerr solitons in microresonators can be described by means of the Lugiato-Lefever equation [50, 51] (LLE). This model was first developed for the description of pattern formation in the transverse plane (i.e., the plane

orthogonal to the propagation direction) of a Kerr medium, contained in a high-finesse cavity [50]. It is derived from Maxwell's equations considering nonlinear contributions, under paraxial, slowly varying amplitude, and mean-field approximations in the low-transmission limit [52, 53].

Years after its original formulation, the model was then adapted towards its highly successful temporal/longitudinal version [51] by Haelterman *et al.*, where the diffraction is replaced by the group velocity dispersion term and two independent temporal variables are introduced, the time  $t$  and the retarded time  $t - z/v_g$ , where  $v_g$  represents the group velocity and  $z$  is the propagation direction. Such a formulation describes a field that is uniform in the transverse plane while propagating along the cavity. A form equivalent to the temporal/longitudinal LLE, with quantities related to the parameters of a microring resonator (MRR), is the following

$$\frac{\partial E}{\partial t} = F - E - i\delta E + i|E|^2 E - i\frac{\beta}{2}\frac{\partial^2 E}{\partial \theta^2}$$

where  $E$  is the electric field and  $F$  is the optical injected field amplitude. The detuning term  $\delta$  between the cavity frequency  $\omega_0$  and the closest input frequency  $\omega_p$  is normalized to the cavity decay rate and  $\beta$  is proportional to the group velocity dispersion  $(\partial v_g/\partial \omega)_{\omega=\omega_0}$ , while the time variable  $t$  is normalized to the cavity decay time. The azimuthal angle is defined as  $\theta = z/R$ , where  $R$  is the MRR radius, and  $z$  is the propagation variable [54, 55]. Note that for any solution of the LLE in the above form with periodic boundary conditions in  $-\pi < \theta < \pi$ ,  $\theta$  will then need to be substituted by  $\theta - (v_g/R)t$  [52].

While most early descriptions of Kerr frequency comb generation have often employed coupled mode theory (CMT) for the description of FWM in the frequency domain, the LLE, which can also be derived from CMT [54, 56], was later used to give a picture of the mean field in the temporal domain [57]. Indeed, although CMT equations offer an easy control of frequency-dependent absorption and coupling terms, they do not give direct access to the information in the time domain, which is instead easily obtained through the LLE [56]. Further, the LLE, which can be easily described as a driven, detuned, and damped nonlinear Schrödinger equation, allows for the straightforward inclusion of additional terms for Raman scattering and higher-order dispersion, as we will discuss in more detail in the following sections. On the other hand, thermo-optic effects, which can represent a limitation for Kerr combs in MRRs [58], have been successfully modeled in some systems through coupled mode equations [59, 60] as well as using the LLE [29]. For the modeling of resonator dynamics through CMT, we refer the reader to [40, 61].

### 9.2.1 Higher-order dispersion

In some experimental cases, solitons with sufficiently short temporal duration exhibit a spectral bandwidth that extends towards the normal dispersion region. Such solitons cannot be properly described through the LLE in the above-mentioned form, which in fact needs to be adjusted (in its temporal version [40, 51]) through the addition of higher-order dispersion terms of the form [62]

$$D_n = i^{n+1} \frac{\beta_n}{n!} \frac{\partial^n E}{\partial \tau^n}$$

for  $n > 2$ , where  $\beta_n$  is the  $n$ -th order dispersion coefficient and  $\tau$  is a time variable, proportional to the previously mentioned retarded time. These additional terms allow for the modeling of soliton bandwidth restrictions in realistic cavities as well as dispersive wave generation [55], where the soliton repels a fraction of its energy into a radiant mode, an effect that can be interpreted as the optical analog of Cherenkov radiation. Additionally, higher-order dispersion mediates the interplay between FWM and dispersive wave formation, in turn giving rise to a spectral recoil, where the soliton spectral peak shifts from the original pump frequency [62, 63]. Finally, we would like to point out that higher-order dispersion terms are often accompanied by a self-steepening effect, as described in [64].

### 9.2.2 Raman effect

The Raman effect in microresonators has been demonstrated to be non-negligible in specific materials, such as  $\text{Si}_3\text{N}_4$  and silica [65]. This effect is usually modeled in the LLE as a fraction of the cubic nonlinearity of the form [66]

$$f_R h_R \otimes |E|^2 \approx f_R |E|^2 - f_R \tau_R \frac{\partial |E|^2}{\partial \tau}$$

often approximated to first order [65], where  $f_R$  is the Raman fraction,  $h_R$  represents the Raman response function, and  $\tau_R$  is the Raman shock time. In microresonators, the effect of Raman scattering implies the development of a self-frequency shift, where the soliton peak frequency is redshifted with respect to the CW pump laser frequency. The compensation of this shift through the spectral recoil generated by higher-order dispersion has been studied in [65]. Additionally, a new type of soliton, called Stokes soliton, has been demonstrated in the presence of Raman gain [67]. In terms of Kerr frequency comb generation, it is important to note that stimulated Raman scattering can ultimately limit the temporal and spectral width of dissipative Kerr solitons [68].

### 9.3 Dispersion engineered cavity dynamics

One of the key advantages of waveguide-integrated MRRs is the large variety of wavelength dispersion properties determining the linear propagation characteristics of the optical modes. In contrast to the unilateral geometries of whispery-gallery mode and photonic belt resonators [69, 70], the bilateral optical mode confinement in MRR opens a large variety of possibilities to adjust the dispersion properties of the circumventing modes. These include (a) adjusting the dimensions of the waveguide cross-section [71–73] or geometry (e.g. split or “race-track” waveguide) [14, 74], as well as (b) altering the composition of the waveguide core (see e.g. the recent works about Kerr combs in  $\text{LiNO}_3$  [75],  $\text{SiO}_x\text{N}_y$  [44, 76, 77],  $\text{Si}_3\text{N}_4$  [78], Diamond, Si) or the coating/cladding materials [36, 72]. While a very detailed overview of emerging materials for integrated microcavities is given in the comprehensive reviews by Kovach *et al.* [79] and Kippenberg *et al.* [47], here we aim to summarize the essentials of dispersion engineering in waveguide-based MRRs and its advantages for altering the temporal dynamics of DKSSs.

#### 9.3.1 Capabilities of dispersion engineering

The key for dispersion engineering in optical waveguides is a careful balance between material- and mode-specific waveguide dispersion. The choice of appropriate core, cladding, and cover layer materials alters the modal dispersion, while defining the guidance and dispersion constraints given by the individual material refractive indices. However, the waveguide geometry (i.e., cross-section and dimensions) may significantly change the modal confinement, increase the field overlap to the surrounding material (i.e. cladding [36] or cover layer [72]), and thus vary the dispersive properties of the mode. Moreover, the lithographic fabrication of photonic on-chip waveguides allows for the incorporation of gaps or slot layers, which add even more free parameters towards tailoring both dispersion and nonlinearity [80, 81]. In general, an appropriate choice of the waveguide materials, geometry, and dimension enables a plethora of dispersion landscapes, ranging from flat normal (i.e. without zero-dispersion) to anomalous dispersion with one, two, or even more zero-dispersion wavelengths in the vicinity of the pump field [81–83]. Commercially available numerical finite-element solvers are required to find the eigenmodes of the Maxwell’s equations in the boundary problem imposed by the rectangular waveguide cross-sections of the MRRs. However, limitations in the fabrication processes, such as material inhomogeneity, stress built-up, and lithographic mask imperfections, usually limit the range of accessible design parameters. On the positive side, recent years have seen a considerable improvement in the fabrication processes (e.g., hybrid material systems, stress release patterns, mask improvements) [47, 79] enabling ever more access to novel dispersion regimes.

### 9.3.2 Advanced control of dissipative soliton dynamics

Dispersion engineering allows waveguide-integrated optical MRR to unlock unprecedented application capabilities. Transferring operation concepts such as controlled dispersive wave emission [84–86], tailored higher-order mode coupling [87–89], and soliton molecule formation [90–93] from nonlinear fibers to MRR has enabled the observation and advanced control over the dynamics of many different cavity soliton states in recent years. In the following, we are going to highlight a few of these advances.

Beyond theoretical modeling, physical limitations in the microcavity design, such as higher-order dispersion or dispersive nonlinearity, severely impact the formation of solitons in terms of bandwidth, power, and mode order. Multiple numerical and experimental studies propose practical approaches in order to optimize Kerr comb properties. In silicon nitride systems, for example, changes as small as a few hundred nm in the waveguide dimension can lead to a significant extent of the anomalous dispersion region causing a fivefold spectral extension of the Kerr comb [94]. The same study also demonstrated the selection of a suitable pump wavelength as a practical tool to alter the Kerr comb spectral extent and power after device fabrication. If pump wavelength tuning remains inaccessible, fine detuning of the free spectral range (FSR), bandwidth, and number of DKS through controlled heating of the MRR can offer an attractive alternative [95]. Similar advantages at faster tuning rates might be offered in the near future by second-order nonlinear materials such as LiNO<sub>3</sub>-based MRRs [75]. Another promising approach on the fabrication side are multi-layer (slot) waveguides [81, 96] and non-uniform MRRs [97] that allow for the accurate adjustment of the cavity net-dispersion and nonlinearity, ultimately granting precise control over higher-order dispersion terms.

Such terms (i.e.  $\beta_n > \beta_2$ ) have been demonstrated to significantly boost the comb bandwidth through one-sided or two-sided dispersive wave generation [36, 81, 98]. Dispersive wave generation is a nonlinear optical conversion process that requires a soliton-like optical pump with a flat phase in order to fulfill the phase-matching condition [62, 99]

$$\Delta\beta = \beta - \beta_s - (\omega - \omega_s)\beta_{1,s} - \frac{1}{2}\gamma_0 P_s = 0$$

The condition compares the flat phase of a soliton  $\beta_s + \frac{1}{2}\gamma_0 P_s$  (with nonlinear parameter  $\gamma_0$  and soliton peak power  $P_s$ ) with the propagation constant of a linear wave  $\beta(\omega)$  in the moving frame of the soliton  $(\omega - \omega_s)\beta_{1,s}$  (with  $\omega$  and  $\omega_s$  angular frequencies of the linear wave and soliton respectively, and  $\beta_{1,s}$  the group dispersion of the soliton), which accounts for the group velocity mismatch. The broadband spectra generated by the interplay of dispersive wave and soliton are of fundamental

use for optical metrology [36, 100] as well as future spectroscopic applications similar to [4, 101, 102]. However, due to the nature of this radiation, the dispersive part of the spectrum does not contribute to the pulsed waveform of the Kerr soliton and thus constitutes a considerable energy loss to the soliton. Moreover, it causes the soliton to spectrally shift in order to compensate for the momentum loss (known as the soliton recoil effect). Depending on the application of the comb system, these effects might be detrimental and worth being reduced through proper dispersion design.

Finally, we like to highlight an unprecedented consequence of dispersion engineering in microcavities, which is the reduction of thermal noise in so-called quiet soliton combs [103, 104]. A comprehensive study recently revealed that operating in a cavity-specific ideal dispersion domain can reduce the thermal instabilities of soliton states up to 60 dB (with 15 dB improvement experimentally shown), thus drastically stabilizing the comb repetition rate and long-term stability [104].

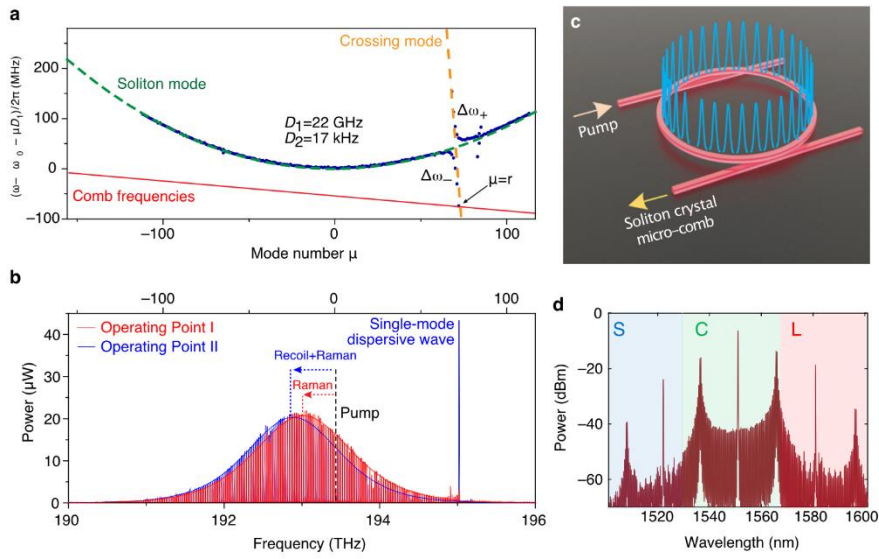
### ***9.3.3 Novel phenomena in dispersion-tailored microring resonators***

Advanced access to waveguide properties also enables the observation of a few unique effects of which no real equivalent exists in optical fiber systems. One of these effects is dispersive wave generation induced by avoided mode-crossing. Avoided mode-crossings may occur in waveguides with relatively large dimensions, which support more than one (fundamental) transversal mode per polarization (i.e., usually  $TE_{00}$  and  $TM_{00}$ ) within the bandwidth of the optical source. Here, the avoided intersections of two transversal modes cause a significant change of the individual mode dispersions (see Fig. 1a), which can be a few orders of magnitude stronger than any other waveguide-intrinsic dispersion change and perturb soliton formation. Similar effects were observed between two different polarization modes [105].

Since larger waveguide sizes are a necessity for anomalous dispersion and power scaling of DKSs [78], intermodal crossings are very likely to occur in MRRs. However, for the purpose of favorable power scaling of cavity solitons, energy leakage due to non-solitonic radiation is largely undesired. Efforts to decrease the impact of higher-order modes include the incorporation of tapered sections into the MRRs [78, 97] as well as higher-order mode isolation couplers [106].

On the contrary, it is noteworthy that mode-crossings, in turn, host the unique capability to steer dispersive-wave formation, since they provide a strong variation of the dispersion. Thus, such crossings eventually provide a set of well defined, very narrow wavelength regions of perfect phase-matching between a soliton pump (in the transversal mode 1) and a dispersive wave (in the transversal mode 2) [103,

107]. Hence, the involvement of avoided mode-crossings imposes advantages on (i) the tuneability of the overall comb bandwidth, (ii) the accurate spectral relocation of dispersive wave energy, as well as (iii) refining the temporal characteristics of the dispersive radiation. Most notably, tailored narrow-band mode-crossings were utilized for the highly efficient generation of dispersive radiation into a single resonator mode (see Fig. 1b) [103]. The study reports further on hysteresis-like interaction between this strong mode and the spectro-temporal behavior of the soliton as well as on the ability of repetition rate stabilization (so-called quiet states), which clearly hosts advantages for switching and long-term stable applications.



**Fig. 1 a).** Dispersion of a cavity soliton with avoided mode-crossing. **b)** Spectrum of soliton comb featuring a single-mode dispersive wave (blue). (a-b) adapted (labels, font size and line widths) from [103] under CC BY 4.0 license. **c)** Illustration of a soliton crystal state and **d)** respective measured spectrum. (c-d) adapted (font size) from [108] under CC BY 4.0 license.

A further specialty of MRRs is the greater ability to reach stable control over the formation of multi-soliton states. Here, mastering of cavity stability through a balance of dispersion, nonlinearity, gain and loss, allows for the formation of multiple cavity solitons. In particular, the fine control over the dispersive properties of the cavity via thermal tuning as fast as 100  $\mu$ s ultimately enables an on-demand increase of the soliton number and the controlled study of multi-soliton behavior [95]. These achievements resulted in the observation and active control of soliton crystals [33, 109]. Here, nonlinear nearest neighbor interactions allow phase-locked multi-photon states distributed over an equidistant temporal grid. The robustness of this highly ordered temporal alignment, in combination with the control over spacing and the existence of vacancies (i.e. Schottky defects) in the temporal grid, gives rise to the name *soliton crystals* in analogy to solid-state atomic crystals. The narrow spacing

of the solitons in the MRR allows for a very practical indirect read-out through their spectra. For instance, through straight-forward Fourier transform rules, the number of solitons in the crystal can be read from the FSR of the most dominant cavity modes, while the number and positions of vacancies become apparent from the underlying modulation structure of the secondary modes (see Fig. 1c,d). The manifold of crystal states and their robustness open up unique and unprecedented applications, among which we can mention background-free soliton lasers with GHz repetition rates [110], ultra-dense data transmission for telecommunications [111], as well as activation functionalities for photonic neural networks [108].

## 9.4 Soliton comb generation schemes

Although Kerr frequency combs promise a powerful alternative to fiber-based frequency comb systems, they come with certain limitations that prevent their widespread use. Indeed, the generation of Kerr combs and their reliable long-term stabilization is currently one of the major bottlenecks that prevent a successful commercialization. In particular, DKSs (a subgroup of Kerr combs) are of high interest for a variety of applications due to their inherent GHz [112] to THz [113] repetition rates, short pulse durations, as well as their high phase stability between comb lines. In order to reach stable soliton operation, several different techniques have been developed in recent years and are briefly described below. For a more thorough review of soliton comb generation schemes, see for example refs. [16, 40, 47, 114].

In general, the majority of developed schemes rely on a tunable narrow linewidth CW laser source that is swept into the microcavity to reach the red-detuned soliton operation point. In 2013, Matsko *et al.* theoretically showed how to achieve DKSs through continuous scanning of the pump frequency, from blue-detuned to red-detuned values (i.e. from a higher optical frequency to a lower optical frequency with zero detuning from the center of the resonance) [115], as was also reported in later works [29, 64, 116]. When an MRR reaches a regime that allows for the propagation of stable DKSs, the intra-cavity energy experiences a sudden drop in intensity. The understanding of this behavior led to the demonstration of DKSs in microresonators in 2014 by Herr *et al.* [29]. These were previously observed in 2013 by Saha *et al.* under the form of femtosecond stable pulses in Si<sub>3</sub>N<sub>4</sub> MRRs [117].

In 2009, Strekalov and Yu proposed a pumping scheme based on the use of a bichromatic source to produce frequency combs in MgF<sub>2</sub> MRRs, exploiting cascaded FWM rather than optical parametric generation [118, 119], leading to highly efficient DKS generation. Similarly, an electro-optic pumping scheme was exploited by Papp *et al.* [120, 121], which has experimentally shown the realization and control of extremely precise equidistant comb lines, essential for achieving ultra-stable solitons.

Additionally, techniques adapted from classical metrology such as the locking of the carrier-envelope-offset (CEO) frequency via self-referencing (i.e.  $f$ - $2f$  interferometry [122]) of the generated comb have been investigated in order to obtain fully stabilized frequency combs in a compact footprint [123, 124]. Towards long-term stabilization, several techniques such as Pound-Drever-Hall feedback control systems [103], servo feedback loops [125], or sideband modulation [126, 127] have been explored.

#### **9.4.1 Frequency scanning**

Initial schemes have utilized a simple, yet effective technique in order to overcome the issue of thermal cavity drifts [29, 115]: By shifting the CW laser source from the blue- to the red-detuned regime, an intracavity thermal equilibrium can be reached, allowing the stable generation of soliton combs. Here, the sweeping speed of the laser is crucial for the generation of the soliton combs and should match the microcavities photon and thermal lifetime, which can be difficult to achieve for some material platforms. As described earlier, the detuning of the pump starting from the blue side leads first to a primary frequency comb, formed through the intracavity power build-up, which in turn seeds FWM within the cavity. Further detuning of the pump laser results in to the generation of ‘subcombs’ and unstable combs formed by modulation instabilities (MI). The common feature of these combs in the blue-detuned regime is high noise in the RF-domain, due to multiple and broad RF beatnotes arising from MI. Once the red-detuned regime is reached, the intracavity power shows an abrupt decline in power and the so-called *soliton steps* can be observed, which show characteristic step sizes depending on the chosen material platform. Here, the generated solitons feature very narrow RF beatnotes as well as stable optical comb outputs. At the beginning of this regime, multi-soliton states are generated and, with increased detuning, they subsequently break down until a single soliton-state is reached. The goal of the frequency scanning method is, to stop the frequency detuning of the laser, once the single soliton state is obtained, which is easier achievable if the soliton step-sizes feature longer time durations ( $\sim$ ms for e.g. MgF<sub>2</sub> [29]).

#### **9.4.2 Power Kicking**

The power-kicking method [36, 128] is a widely used technique that allows for the generation of soliton combs in materials that feature a high thermo-optic coefficient. In these materials (such as Si<sub>3</sub>N<sub>4</sub>), the observed soliton steps exhibit very short time durations ( $\sim$  $\mu$ s), which prevent the effective use of the frequency scanning method (i.e. to precisely stop the laser frequency on one of the soliton steps). Instead of

using only a single tunable CW laser, two intensity modulators (acousto-optic and electro-optic modulators, AOM and EOM, respectively) are included before the microcavity. The use of the EOM is necessary to obtain the required speed, which cannot be provided by the AOM alone. Here, the AOM reduces the pump power of the source before tuning into the resonance, allowing to quickly reach the soliton steps. Subsequently, the AOM increases the pump power in order to stabilize the reached soliton step. After the AOM, an EOM helps diminishing thermal instabilities by effectively reducing the pump power right before the zero-detuning point (i.e. the resonance center), which also ensures a fast transition to the soliton steps. When the settings (and timings) for the laser frequency sweeping and both modulations are correctly chosen, this method allows for the reliable generation of soliton combs in materials featuring higher thermo-optic coefficients.

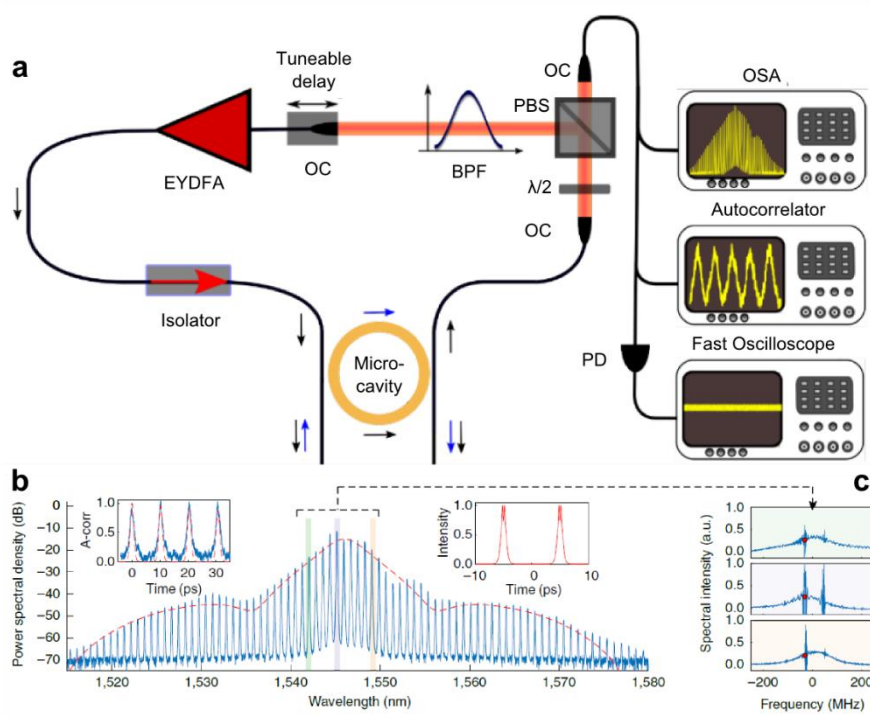
### ***9.4.3 Thermal Tuning***

A more inexpensive method can be realized with on-chip resistive heaters on top of the microcavities [95, 129]. In this scheme, the tunable CW laser is replaced by a fixed frequency CW laser diode and the cavity resonance is thermally tuned by inducing a refractive index change caused by the thermo-optic effect. This can be realized through, for example, an electrode on top of the microcavity, which is current controlled. This allows for relatively fast speeds (given the small structure and thermal mass of the electrode) as well as for the fine tuning precision (determined by the bit-depth of the used digital-to-analog converter) required to directly obtain the short ( $\sim\mu\text{s}$ ) soliton steps. Furthermore, although similar to the frequency scanning scheme, the thermal tuning technique offers advantages due to the use of single frequency lasers with lower RF noise as well as narrower linewidths (compared to tunable lasers), resulting in combs with lower noise. However, for use in more complex photonic integrated circuits (PICs), local heating of the chip might pose additional restrictions as other integrated elements would need to be shielded from any temperature gradients and effects (i.e. thermal crosstalk), thus potentially limiting the scope of this technique [130].

### ***9.4.4 Self-injection locking and laser-based configurations***

The previously reported schemes rely on the use of CW lasers for pumping, which are far from being monochromatic sources (with linewidth shifts of tens of kHz), suffer from instabilities due to noise, and require extensive optical pump power ( $\sim$  Watt level), as well as elaborate feedback control systems. Additionally, thermal instabilities can strongly affect the ability to generate and stabilize coherent states,

since solutions may experience thermal drifting, hence, leading to the destruction of the coherent soliton regimes.



**Fig. 2 Nested cavity setup for soliton generation.** **a)** The setup consists of a high-doped index silica glass (Hydex) MRR (Microcavity) nested in an external feedback fiber cavity, composed of a short-length erbium-ytterbium co-doped fiber amplifier (EYDFA), an optical isolator to ensure unidirectional propagation, a tunable optical bandpass filter (BPF), a tunable delay line, a polarizer (PBS), a waveplate ( $\lambda/2$ ) for polarization control and three optical collimators (OCs). The external propagation cavity modes sustain the microcavity pulses, which are broadened by the Kerr nonlinearity over the gain bandwidth. This setup allows to reach stable soliton states with a variable repetition rate in the order of megahertz. **b)** Soliton generation for two equidistant solitons per round-trip, with 150 mW output power from the amplifier and 30 mW output from the MRR. The experimental (blue) and theoretical (red) values of the spectrum measured with an optical spectrum analyzer (OSA) and autocorrelation trace are shown in the left and right insets, respectively. The temporal intensity output from the fiber cavity is monitored with a photodiode (PD) and a fast oscilloscope **c)** Intracavity spectrum (blue), showing the mode lasing within each microcavity resonance. Adapted (cropped with modified font size and labels) with permission from figures (3,S6) in Bao *et al.* Nature Photonics 13: 384-389 [110].

Thermo-optical nonlinearity, originating from the thermal capacitance of the microresonator material, modifies the steady-state solutions of the intra-cavity field, by creating a slow dependence of the refractive index from the temperature. This, in turn, induces an additional detuning with respect to the pump frequency, which competes with the ultra-fast Kerr red-shift, resulting in a variety of non-solitonic

nonlinear regimes, such as self-pulsing and deterministic chaos [49, 60, 85, 115, 131–134].

In order to address stabilization issues, Yi *et al.* [125] proposed an active approach by employing a feedback loop for the self-adjustment of the output power. Such a configuration allowed to achieve coherent states that are robust against thermal instabilities over long times. This in turn led to the development of even more efficient schemes that allow for the generation of stable solitons through passive driving and control of the cavity parameters, known as passive self-injection locking. This technique was proposed in an initial work by Liang *et al.*, to narrow the linewidth of a distributed feedback laser with an MRR [135].

Injection-locking schemes based on free-running diode lasers have gained increased interest for the use in simplified, small footprint turn-key soliton generators [136–139]. Here, instead of using a tunable CW laser for pumping (which needs to be optically isolated from the microcavity – a difficult task for monolithic integration), the microcavity is directly attached to a semiconductor laser diode (e.g. a distributed feedback laser, DFB), which is operated in a free-running mode. Small back-reflections inside the microcavity are being utilized to lock the free-running diode to the microcavity resonance, which subsequently allows for stable soliton generation.

In 2020, Shen *et al.* demonstrated a turn-key soliton comb generator based on a DFB laser coupled to a  $\text{Si}_3\text{N}_4$  microresonator chip packaged inside a commercially available butterfly package [138]. The authors showed reliable soliton comb generation with an FSR of 40 GHz spanning 30 nm, requiring only 30 mW of optical pump power. Remarkably, the demonstrated system not only allows for reliable turn-key operation (meaning that repeated on and off switching results in the same comb output) but it also exhibits much lower noise figures than other monolithic integrated lasers and even off-the-shelf tunable external cavity lasers.

In 2019, Bao and coauthors used a nested cavity configuration scheme for producing Kerr solitons [110, 133, 140], based on a nested configuration where an MRR is embedded in an external fiber cavity, which allows for signal reinjection into the ring.

This setup, illustrated in Fig. 2, is inspired by a passive laser mode-locking setup, first demonstrated by Pasquazi, Peccianti *et al.* in 2012 [40, 141–146], which embeds an MRR in an active laser loop. The result is a mode-locking almost insensitive to thermally-induced fluctuations. Remarkably, Bao *et al.* recently demonstrated a new class of DKSs that can be generated upon a free-CW background, with a tunable repetition rate of megahertz, sustained by the gain of the lasing medium, with a mode efficiency of 75% at average powers that are one order of magnitude lower than the energy threshold for soliton generation predicted by the LLE [110].

## 9.5 Nonlinear dynamics of DKS

Cavity solitons in MRRs can exhibit a rich variety of nonlinear dynamical regimes and intriguing nonlinear effects that have been exploited in a plethora of practical applications in spectroscopy, sensing, and telecommunications (see the following section for more details). Some examples of the available regimes are bright and dark soliton states [147], soliton Cherenkov radiation [62], Stokes solitons [67], as well as soliton crystallization [109, 111, 148], switching [149], and breather states [150, 151].

Bright and dark solitons can coexist in Kerr media that undergo third-order dispersion in the normal regime, as studied by Parra-Rivas *et al.* [152]. Indeed, Xue and coauthors have shown that dark soliton states can be observed in the normal dispersion regime [153]. Moreover, as outlined earlier, Brasch *et al.*, reported that higher-order dispersion terms in silicon nitride MRRs, while inducing a spectral broadening of the coherent states, can enable Cherenkov radiation associated to DKS propagation [36]. Stokes solitons have been also observed in MRRs, where their generation is mediated by the compensation process between Raman interaction and dispersion, which supports stable soliton propagation [47]. This is achieved through the exchange of energy with a primary DKS, formed via Kerr nonlinearity, and Stokes states, belonging to a distinct mode family.

Remarkably, in 2019, Karpov *et al.* demonstrated the generation of deterministic soliton crystal states in MRRs for a critical pump power value, corresponding to a stable defect-free lattice of optical pulses, sustained by the modulated driving field of a CW source [154]. The investigation of soliton crystals revealed the interesting dynamical features stemming from the switching of these states into transient chaos and the formation of breathers via a melting and recrystallization process.

## 9.6 Applications

Since their first introduction in 2007 [155], Kerr frequency combs (incl. soliton combs) have gained increased interest as a powerful, small-scale alternative to traditional frequency combs [122, 156], arising from their potentially low power consumption [113] as well as their cost-efficient, mass producible integration through the same CMOS-processes and infrastructure of the semiconductor industry [80]. Moreover, as outlined earlier, the generated Kerr frequency combs can eventually span, depending on the chosen material platform and dispersion engineering, the ultraviolet [157, 158], the visible [159], the mid-infrared [160], up to the THz regimes [161], offering great opportunities for many fields of application. Further, the capability of precisely adjusting the dispersion allows for the generation of combs that can intrinsically cover more than one octave (where a frequency and its double

both exist within the generated spectrum, e.g. 150 THz ( $\sim 2 \mu\text{m}$ ) and 300 THz ( $\sim 1 \mu\text{m}$ ), avoiding the need for further broadening in a preceding nonlinear device, which is important for comb stabilization [98, 124] and crucial for most of their intended applications. As a result of this versatility, Kerr soliton frequency combs have already revolutionized many applications, including classical frequency comb adaptations such as dual-comb spectroscopy [4]. Moreover, due to the small structures of microcavities, high FSRs (ranging from GHz to THz) can be achieved, which makes these platforms interesting for telecommunications applications. In fact, the FSRs of microcavities can be finely adjusted to match the WDM (wavelength division multiplexing, 100 GHz) and DWDM (dense WDM, 50 GHz) telecom grids, thus allowing for massively parallel and high-bandwidth transmission schemes obtained by exclusively using a single optical source [9, 111]. Other novel concepts and demonstrations include optical clockworks/gears, which are able to coherently link different electromagnetic domains, e.g. from hundreds of THz to MHz. This in turn allows the optical frequency of an atomic reference (e.g. Rb) to be counted by standard electronics [162–164]. Besides, promising applications including optical frequency synthesizers [165], RF processing [166], ultra-fast and multi-color optical ranging (i.e. LIDAR, light detection and ranging) [167–169], the generation of THz radiation [161], as well as astrocombs [10, 11, 170] have been all demonstrated, to only name a few.

More recently, advanced ‘hybrid’ approaches such as the combination of microcavities with piezo-electric materials [169], opto-mechanical designs [171], and integrated MRRs in electro-optic materials [75] have been investigated, offering new possibilities and functionalities for these powerful microcavity platforms. Finally, it is noteworthy that besides the aforementioned soliton applications, microcavities have attracted significant attention for utilization outside the soliton regime in applications such as biosensing [172, 173], narrow-linewidth lasers schemes [174], optical machine-learning [108, 175–178], and quantum technologies [13, 15, 17, 18, 179–184].

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