

Neutronics Scoping Studies for Experimental Fusion Devices

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## NEUTRONICS SCOPING STUDIES FOR EXPERIMENTAL FUSION DEVICES

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### Abstract

A new Affordable Robust Compact (ARC) Fusion Reactor, which meets its goal in a cheaper, smaller but even more powerful, faster way to achieve Fusion Energy, with new high-field, high-temperature superconducting (HTS) magnets, has been designed in the US. SPARC will be the research tokamak aimed at the development of many ARC technologies. Ignitor is a proposed compact high-field tokamak that share with SPARC and ARC some design concepts, showing the convenience of this tokamak design development line. Neutronics and radiation damage scoping studies have been carried out for both designs. A general-purpose macroscopic model, set up by some of the authors in previous studies, has been used to estimate the radiation damage on selected machine components for the two cases. Solutions to solve the problem of radiation damage of the Toroidal and Poloidal Field Coils materials have been explored.

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3 **1. Introduction**  
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6 Progress in technological fields such as High Temperature Superconductors, additive  
7 manufacturing and innovative materials has led to new scenarios and to a second generation  
8 of Fusion Reactors designs. A new Affordable Robust Compact (ARC) Fusion Reactor, which  
9 meets its goal in a cheaper, smaller but even more powerful, faster way to achieve Fusion  
10 Energy, with new high-field, high-temperature superconducting (HTS) magnets, has been  
11 designed by MIT (Massachusetts Institute of Technology) and PSFC (Plasma Science and  
12 Fusion Center).<sup>1,2</sup> ARC too might face radiation damage problems, besides neutron-induced  
13 activation, either for the Vacuum vessel, or for the Poloidal and Toroidal Field Coils (PFC and  
14 TFC). For ARC, the selected superconducting material for the magnets is Rare Earth Barium  
15 Copper Oxide (REBCO), a high temperature superconductor that can work at temperature up  
16 to 80 K, which is higher than the one for Nb3Sn used for ITER. ARC will breed its own tritium  
17 by means of a FLiBe self-cooled blanket.<sup>1</sup>  
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38 Ignitor is a proposed compact high-magnetic field tokamak<sup>3</sup> that includes in its design many  
39 features that served, together with the ALCATOR design and experimental results, as a basis  
40 for the development of the SPARC-ARC concepts. Ignitor is aimed at studying plasma burning  
41 conditions in Deuterium-Tritium plasmas: it has a major radius of 1.3 m, minor radii of 0.47 m  
42 and 0.87 m, a peak plasma temperature of 12 keV, a peak plasma density of  $10^{21}$  ions/m<sup>3</sup>, at  
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54 <sup>1</sup> The MIT PSFC has also begun developing a conceptual design for SPARC, a compact, high-field, net fusion  
55 energy experiment. SPARC would be the size of existing mid-sized fusion devices, but with a much stronger  
56 magnetic field. Based on established physics, the device is predicted to produce 50-100 MW of fusion power,  
57 achieving fusion gain, Q, greater than 3. Such an experiment would be the first demonstration of net energy gain  
58 and would validate the promise of high-field devices built with new superconducting technology. Even if SPARC  
59 will have lower fusion power than ARC, it will have smaller dimensions, and thus activation and radiation damage  
60 aspects must be studied too.  
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1 a maximum fusion power of 90 MW. Pulses at different power levels are planned, with either  
 2 DD or DT operation, distributed over a global operation time of 10 calendar years. The peak  
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 4 neutron wall loading at maximum fusion power is about 2 MW/m<sup>2</sup>. The tokamak main  
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 6 components are: a graphite first wall, an INCONEL625 vacuum vessel, the Cu-based toroidal  
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 8 magnets, and the AISI316 machine structure (named "C-Clamp").  
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 12 A comparison of the two designs is available in Table I. In this paper, some neutronics scoping  
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 14 studies will be carried out for both tokamaks (Ignitor and ARC). A general-purpose  
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 16 macroscopic model, set up by some of the authors in previous Ignitor studies, has been  
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 18 revised and used to estimate the radiation damage on selected machine components for the  
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 20 two cases. Solutions to solve the problem of radiation damage of the toroidal and poloidal  
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 22 field coils (TFC and PFC) materials have been explored.  
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33 Table I - Ignitor and ARC Tokamaks parameters  
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PARAMETER	Ignitor	ARC
Major radius	1.32 m	3.3 m
Toroidal Magnetic Field	13 T	9 T
Plasma Volume	10 m <sup>3</sup>	141 m <sup>3</sup>
Fusion Power (MW)	90	525
Electric Power (MWe)	--	283
Q	Infinite	3
Pulse flat top	10 s	infinite
Magnets Temperature	4 K	80 K

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## 2. A model for neutronics and radiation damage scoping studies

Previous Ignitor studies<sup>4</sup> have been found relevant to set up a model for the ARC radiation damage case too.

In a simple *macroscopic* model the number of displaced atoms depends on the total available energy  $E_a$  and the energy required to displace an atom from its lattice position  $E_d$

$$\text{DPA} = \kappa \frac{E_a}{2E_d} \quad (1)$$

If the neutron flux and spectrum is known, then we have:

$$\text{DPA} = \frac{\int dV \int dE \Phi(\vec{r}, E) \sum_{i=1}^N \rho_i \sigma_{R,DPA,i}(E)}{\sum_{i=1}^N \rho_i} \quad (2)$$

summed over all N isotopes in the material mix, where  $\sigma_{R,DPA,i}$  is the DPA cross section for the isotope i, and  $\rho_i$  is the atomic density.

The most recent version of the inventory code FISPACT,<sup>5</sup> which has been extensively updated (now called FISPACT-II) is now able to compute radiation damage quantities, such as dpa (Displacement per Atom), Gas Production, KERMA (Kinetic Energy Release to Matter) factors. The code has been found a suitable tool for our neutronics scoping studies. FISPACT-II, in fact, can calculate dpa rates directly using the above formulae, with the latest cross-section nuclear data libraries, such as the TENDL-2017 library.

## 3. Neutronics and radiation damage scoping studies for Ignitor

1 Radiation damage calculations for Ignitor have been performed by means of the MCNP code.<sup>6</sup>

2 In particular, the total dose on the TFC insulator (DTFC) turned out to deserve some attention.

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4 In particular, results are as follows:

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$$DTFC = 9.01 \cdot 10^{-23} \text{ MGy}/(\text{neutron generated in the plasma}) \quad (3)$$

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9 If we now evaluate the dose on the TFC insulator based on the total neutron production  
10 foreseen for Ignitor<sup>7</sup>, namely  $9.22 \cdot 10^{22}$  neutrons in 7 years of DT operation, we have:

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$$DTFC = (9.01 \cdot 10^{-23} \cdot 9.22 \cdot 10^{22}) \text{ MGy} = 8.3 \text{ MGy} \quad (4)$$

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16 The TFC insulator is made of G10CR, a bisphenol-A epoxy resin, chlorine-free, low-N, low O,  
17 with a boron-free high-strength E glass tissue. The radiation resistance of G10CR material has  
18 to be carefully considered, since it appears to be poor, and possible substitute materials must  
19 be looked for. Alternatively, some additional shielding must be foreseen.

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22 The G10CR resin was found to have a very low radiation resistance, with a degradation of its  
23 mechanical properties as early as an irradiation of around 3 MGy was applied.<sup>8</sup> On the other  
24 hand, the similar material G11CR did not show any relevant degradation. Another early  
25 important work in the field of radiation damage of those materials (Ref. 9) stated that the G-  
26 10CR matrix is a conventional, heat-activated, amine-catalyzed, bisphenol-A, solid type epoxy  
27 resin chosen for proven performance at cryogenic temperatures, while the G-11CR matrix is  
28 an aromatic-amine-hardened, bisphenol-A, liquid-type epoxy resin expected to provide  
29 improved resistance to radiation damage.

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32 The radiation resistance limit for the epoxy used in ITER is 10 MGy (Ref. 10). That resistance  
33 does not seem enough to meet ITER requirements on a safe side, and development of novel  
34 insulators has been carried out in the recent years. Cyanate esters (CEs) offer enhanced  
35 temperature and radiation resistance as well as high mechanical strength.<sup>11</sup> No technological  
36 challenges in the coil fabrication are needed, since CE resins can be treated like epoxies and  
37 are compatible with the vacuum pressure impregnation (VPI) process, which is foreseen for  
38 the fusion coils due to their complexity. These materials are being considered also for  
39 replacement of insulators in ITER. Some recent publications<sup>10</sup> show the excellent radiation  
40 resistance properties of these materials. Several mixtures of CE and epoxy resins were  
41 investigated, and the pure CE composite, named T1, maintained about 75% of its mechanical

1 strength, compared to the unirradiated state, even at a fluence of  $5 \cdot 10^{22} \text{ m}^{-2}$ , which  
2 corresponds to a dose of 250 MGy. In conclusion, Cyanate esters could be the best candidate  
3 for Ignitor too. Recent literature shows their excellent characteristics,<sup>10</sup> and the product is  
4 available on the high-tech materials market.<sup>11</sup>  
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8 A scoping study was carried out in order to determine the best shielding material if no  
9 modification is made to the insulator. Three advanced materials were selected, based on their  
10 favourable physical properties for radiation shields, i.e., Solid lithium hydride (LiH), powdered  
11 zirconium dihydride (ZrH<sub>2</sub>), and powdered zirconium borohydride (Zr(BH<sub>4</sub>)<sub>4</sub>). The more  
12 traditional DPE (High-density Polyethylene), Borotron<sup>®</sup> HD050 and B4C have been considered  
13 too. To assess their nuclear performance, the total radiation doses to the TF coils and neutron  
14 heat deposition were obtained with coupled MCNP-FISPACT-II calculations. The three  
15 advanced shielding materials all turned out to be better than the traditional materials. In  
16 particular, ZrH<sub>2</sub>, with its high mass density, high hydrogen content, and high average atomic  
17 number, was the best performing one. Advanced neutron shield materials (Zr- and Li-  
18 hydrides) form high performance neutron/gamma shields, within possible Ignitor design  
19 modifications. In particular, a 10-cm shield of Powdered zirconium dihydride (ZrH<sub>2</sub>) can  
20 reduce the dose on the insulator by a factor 100:6 (if the dose is 100 in arbitrary units without  
21 shield, it becomes 6 with it). Higher shield thickness is not recommendable from the design  
22 viewpoint.  
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38 As far as radiation damage on vessel materials, a scoping study has been performed for  
39 several candidate structural and plasma-facing materials. Results are shown in figure 1. Due  
40 to the low foreseen fluence of Ignitor, it turns out that radiation damage for those  
41 components is not an issue, while their shielding capability is. Inconel 625 has the best  
42 shielding performance, while – as far as first wall tiles are concerned – C, due to its high  
43 moderation characteristics, has to be preferred to Mo: even if absorbing less neutrons, it  
44 enhances neutron capture in the vessel by slowing down neutrons.  
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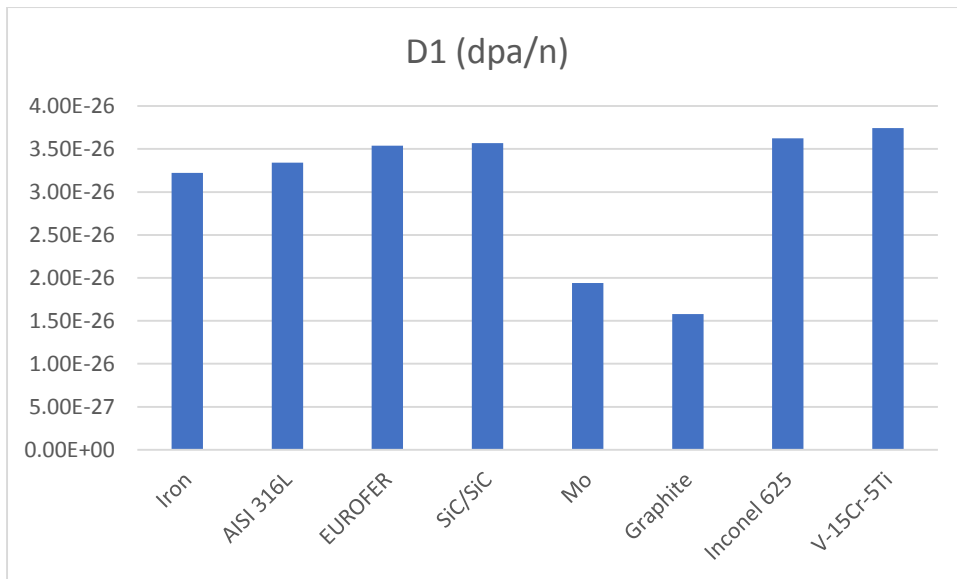


Figure 1 – Radiation damage in vessel and first wall Ignitor materials

#### 4. Detailed studies for the Affordable Robust Compact (ARC) tokamak

ARC is a tokamak designed by MIT scientists. It has been conceived for a FNSF (Fusion Nuclear Science Facility) and pilot plant for producing power,<sup>1</sup> therefore it will be used to collect data about over-energy breakeven reactors and to demonstrate the feasibility of a nuclear fusion power plant connected to an electric grid.

Magnets are the main novelty of ARC reactor: TF coils and PF coils rely on High Temperature Superconductor (HTS) technology, now available on commercial scale. HTS are alloys based on Rare Earths (more specifically Yttrium) Barium and Copper Oxide (REBCO or YBCO) and their critical temperature is as high as 80K. The adoption of the HTS technology for the magnets allows obtaining more compact and cheaper tokamaks than those using traditional technologies based on 4K superconductors. The downside of this technology is that REBCO tapes are very sensitive to neutron damage.<sup>12,13</sup> Also, since ARC's TF coils are demountable,

1 PF coils can be placed inside them in order to achieve a better plasma control.<sup>2</sup> This approach  
2 was followed by many tokamaks, such as DIII-D<sup>14</sup> and Alcator C-Mod.<sup>15</sup> However this may  
3 raise concerns about neutron damage that would be not only on TF coils, like other tokamaks,  
4 but also, and even with a higher rate, on PF coils.  
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10 ARC is Deuterium-Tritium fueled. A D-T fusion plasma is a huge source of fast neutrons and,  
11 more specifically, ARC's plasma, supposed to achieve 525 MW of fusion power, will emit  
12 about  $2.2 \times 10^{20}$  n/s (Ref. 1). Therefore, ARC is a relatively small device, with a high density of  
13 complex components near its center, and a strong neutron source at the core. This surely  
14 requires careful neutronics studies and effective shield design proposals.  
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24 The ARC shield can be split into two main components. Starting from the plasma core, the  
25 first neutron shield is the Nickel-superalloy-based vacuum vessel (VV); its first aim is to  
26 provide a vacuum and pure volume for plasma and not being an effective neutron shield,  
27 however shielding properties of VV materials will be addressed in this scoping study. The  
28 actual neutron shield of this device, however, is the blanket: in fact, the vacuum chamber is  
29 immersed in a tank full of a LiF BeF<sub>2</sub> (FLiBe) molten salt. This fluid works as a neutron  
30 multiplier, tritium breeder, and coolant, while the bulk tank is a quite effective shield for PF  
31 and TF coils.  
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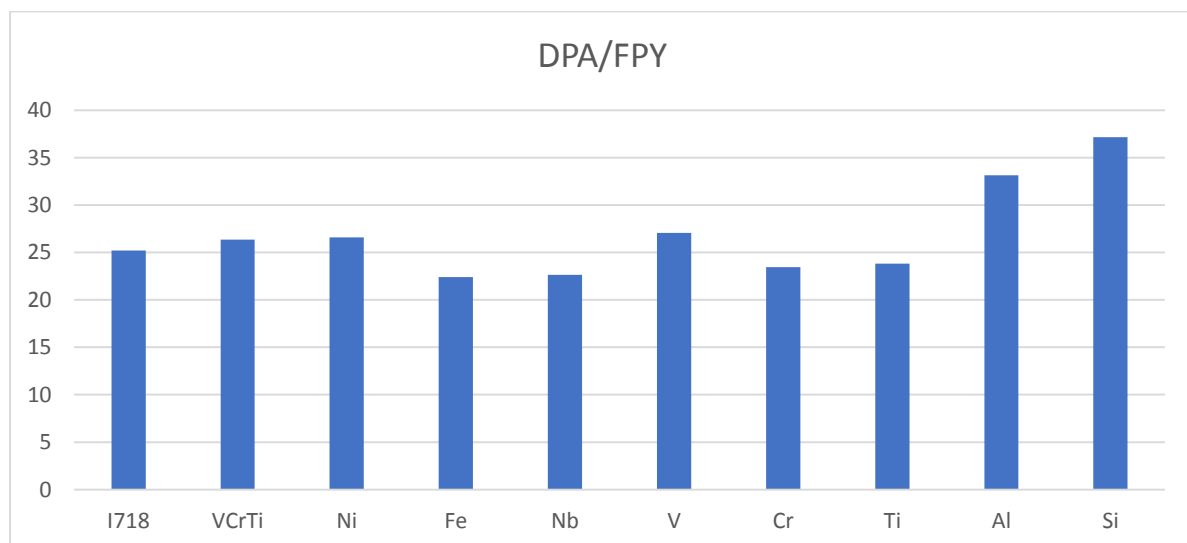
45 MCNP simulations<sup>1</sup> have shown that an additional shield was necessary in order to safeguard  
46 TF coils, and a TiH<sub>2</sub> layer has been placed all the way around the FLiBe tank. TiH<sub>2</sub> has been  
47 chosen as it confirmed – like in the case of Ignitor – its excellent moderation and absorption  
48 characteristics. Further simulations demonstrated that this configuration is actually able to  
49 guarantee a lifetime of 9 FPY (Full Power Years) to magnets.<sup>1</sup>  
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1 A second ARC design session lead to some design modifications: long leg, double null  
2 divertors, able to effectively exhaust huge heat fluxes, have been added to the machine.<sup>3</sup> The  
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4 neutron flux in the divertor area (at the outer surface of the VV at the midplane of the divertor  
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6 foot feature) is a factor of thirty lower than at the outer midplane, while the neutron spectrum  
7  
8 is significantly softened due to the moderation provided by the FLiBe.<sup>2</sup> The reduction of fast  
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10 neutron flux drastically reduces neutron damage rates, in terms of both displacements per  
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12 atom (dpa) and helium production from neutron-alpha interactions. A lower damage rate in  
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14 the divertor represents an advantage for those high heat flux components. However, the new  
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16 divertors raise the complexity of the required magnetic configuration, asking for additional  
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18 coils. Furthermore, as previously mentioned, PF coils have been moved inside the TF ones and  
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20 FLiBe tank has been reshaped.<sup>2</sup> An improved Monte Carlo model for the new configuration  
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22 highlighted the necessity of more effective shielding for the PF coils in their new location. It  
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24 has been chosen therefore to add 25 cm thick ZrH<sub>2</sub> plates directly inside the FLiBe tank, in  
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26 order to shield the magnets.<sup>2</sup> In this case, the role of the 5 cm-thick vessel gives a small but  
27  
28 relevant contribution in reducing the neutron flux on the PFC, even if most absorptions take  
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30 place in the 1 m thick FLiBe blanket: the additional shield, with its high hydrogen density,  
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32 softens the neutron spectrum and enhances neutron absorptions in the blanket. Altogether,  
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34 those structures can reduce the neutron load on PFC of roughly two orders of magnitude:  
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36 more specifically, total flux is around to  $3 \times 10^{18}$  n/cm<sup>2</sup>, with a soft energy spectrum, and that  
37  
38 guarantees to the TFC a lifetime of 10 FPY at least.<sup>3</sup>

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41 However, the mentioned previsions are supposed to be quite pessimistic. In fact,  $3 \times 10^{18}$   
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43 n/cm<sup>2</sup> is the limit set for Nb<sub>3</sub>Sn superconductors, used for ITER,<sup>16</sup> while REBCO tapes are  
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45 supposed to have less constraining limits.<sup>12</sup> Furthermore, limits were not set at the failure  
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47 point of the material, but rather at a point at which the critical current begins to degrade.<sup>2</sup> In  
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1 addition, recent literature<sup>13</sup> has shown evidence that it is possible to mitigate critical current  
2 degradation, due to fast neutrons, decreasing operating temperature (i.e. for operating  
3 temperature of 30 K and roughly  $3.2 \times 10^{18}$  n/cm<sup>2</sup>, YBCO critical current seems to be still very  
4 similar to its initial, not irradiated one). Low energy neutrons – on the other hand - have hardly  
5 any effect on the superconducting properties of YBCO tapes.<sup>13</sup> Even if ARC's magnets will be  
6 running with a significant margin to their critical current, design modifications could affect  
7 these shortcomings, like for instance the substitution of the VV material, or an optimization  
8 of the ZrH<sub>2</sub> shield thickness.  
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10 Concerning radiation damage in the vessel material, a study has been performed in order to  
11 verify the susceptibility to radiation damage of the proposed low-activation substitute of  
12 Inconel718, that is, the V-15Cr-5Ti alloy. By means of FISPACT-II, with the already mentioned  
13 new library, results available in Figure 2 have been obtained, where radiation damage in  
14 terms of dpa/FPY (Full Power Year) are shown. Dpa rate in V-15Cr-5Ti is just less than 5%  
15 higher than the same figure for Inconel718. While it is actually unknown the onset threshold  
16 for some radiation damage effects in Inconel718 or V-15Cr-5Ti, they should reach a lifetime  
17 irradiation lower than 100 dpa before being replaced for other reasons.  
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Figure 2 – Radiation damage (DpA per Full Power Year) in Inconel 718 (I718) and V-15Cr-5Ti (VCrTi), and in their main alloying elements.

The shielding capability of the vessel material can be a relevant question, given the above-mentioned necessity to shield the magnets. A good parameter to estimate the shielding performance of a material exposed to neutron flux is the KERMA rate ( $\text{kW}/\text{cm}^3$ ). Figure 3 shows results for Inconel718, V-15Cr-5Ti and their main alloying elements. It turns out that the KERMA rate for V-15Cr-5Ti is significantly (-35%) lower than for Inconel718, mainly due to the lack of Nickel. This fact will have to be taken into account if the new vessel material is adopted for ARC. Not only the shielding capability of the new material is lower, but also the effect of Inconel718 substitution on the neutron spectrum and then on the neutron absorptions in the FLiBe blanket will have to be evaluated.

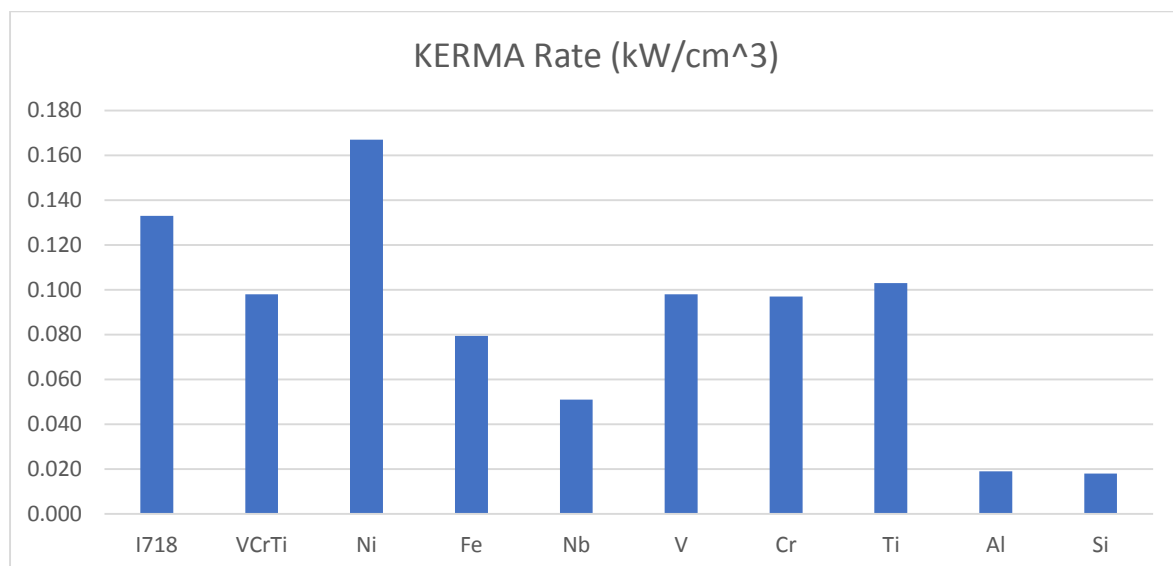


Figure 3 – KERMA Rates in Inconel 718 (I718) and V-15Cr-5Ti (VCrTi), and in their main alloying elements.

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3 **5. Conclusions**  
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6 Neutronics scoping studies have been carried out for two different compact high-magnetic  
7 field tokamaks: Ignitor and ARC. A general-purpose macroscopic model has been set up, to  
8 estimate the radiation damage on selected machine components for the two cases.  
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14 Solutions to solve the problem of radiation damage of the Poloidal and Toroidal Field Coils  
15 materials have been explored. In particular, for ARC, it has been found that ARC's magnets  
16 will be running with a significant margin to their critical current, however the effects of the  
17 substitution of Inconel 718 with V-15Cr-5Ti as vessel material will have to be taken into  
18 account.  
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