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Highlights

- Sand dune aerodynamics investigated within a computational study
- Simulation of different experimental setup
- Comparison between computational results and experimental measurements
- Emerging 3D coherent, mushroom-like flow structures in a nominally 2D setup
- Some good practices in dune aerodynamics are recommended

Sand transverse dune aerodynamics: 3D Coherent Flow Structures from a computational study

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Abstract

The engineering interest about dune fields is dictated by the their interaction with a number of human infrastructures in arid environments. Sand dunes dynamics is dictated by wind and its ability to induce sand erosion, transport and deposition. A deep understanding of dune aerodynamics serves then to ground effective strategies for the protection of human infrastructures from sand, the so-called sand mitigation. Because of their simple geometry and their frequent occurrence in desert area, transverse sand dunes are usually adopted in literature as a benchmark to investigate dune aerodynamics by means of both computational or experimental approaches, usually in nominally 2D setups. The present study aims at evaluating 3D flow features in the wake of a idealised transverse dune, if any, under different nominally 2D setup conditions by means of computational simulations and to compare the obtained results with experimental measurements available in literature.

Keywords: dune aerodynamics, Computational Wind Engineering, 3D flow, mushroom-like coherent flow structures

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1. Introduction

The engineering interest about dune fields is dictated by their interaction with a number of human infrastructures in arid environments, such as roads and railways, pipelines, industrial facilities, farms, buildings (e.g. [Alghamdi and Al-Kahtani, 2005](#)). Some of such undesired effects are shown in Figure 1. The

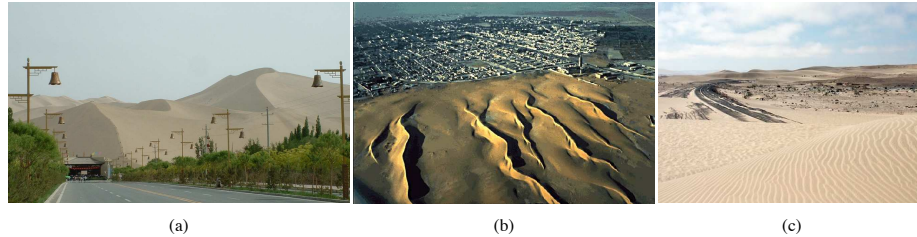


Figure 1: Windblown sand interaction with anthropic activities: megadunes surrounding a road and farmlands in Dunhuang, Gansu Province, PRC. Photo: I.A. Inman, 2007 (a), linear dunes encroaching Nouakchott, capital of Mauritania. Landsat 1565-10032-6, 1974 (b), loose sand covering the Aus to Lüderitz railway line, Namibia. Photo: K. Dierks, 2003 (c)

development, shape and migration of dunes depend fundamentally on availability of mobile sediment, on the incoming wind directionality, and on the flow structures of local disturbed wind ("topographically forced wind" in Geomorphology literature), that is on the wind ability to induce sand erosion, transport and deposition. In particular, coherent flow structures embedded within fluid flow fields are considered to govern the magnitude, form and scaling of sediment transport events ([Bauer et al., 2013](#)), and the dune shape in turn. Hence, a wind-focused perspective has been adopted in aeolian dune geomorphology in order to investigate the former to explain the latter. In wind engineering, a deep understanding of dune aerodynamics serves to ground effective strategies for the protection of human infrastructures from sand, the so-called sand mitigation. In areas of constant wind direction and under high sand availability, the transverse dune - which has nearly fixed profile in the direction perpendicular to the wind - is the prevailing dune type ([Livingstone and Warren, 1996](#)). Furthermore, ideal sharp-crested transverse dune, i.e. without crest-brink separation ([Bauer](#)

et al., 2013), are usually adopted in fundamental aerodynamic studies for their geometric simplicity. Previous studies (e.g. Lancaster, 1995) have revealed that transverse dunes generally have upwind (windward, stoss) slope angles ranging between $2^\circ \leq \alpha_u \leq 20^\circ$ and downwind (leeward) slope angles ranging between $28^\circ \leq \alpha_d \leq 34^\circ$, i.e. around the sand friction static angle. For sake of clarity, a simplified 2D scheme of the transverse dune geometry and of the flow around it is given in Figure 2. The aerodynamic behaviour of sand dunes in atmospheric

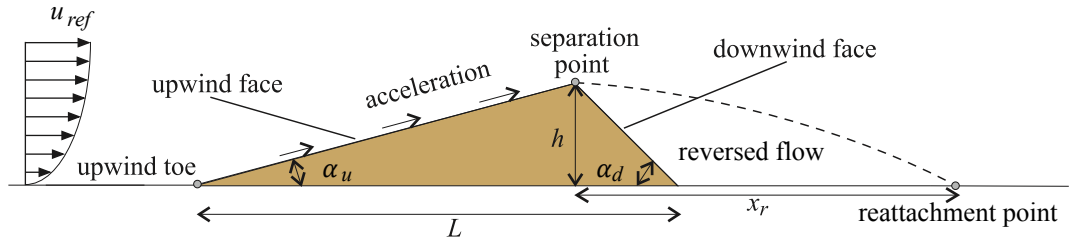


Figure 2: Ideal sharp crest, transverse dune aerodynamics scheme

boundary layer belongs to the very general class of bluff bodies and to the general one of hills (for a review, see e.g. Bitsuamlak et al., 2004). The incoming wind flow is first fairly decelerated at the upwind toe, then strongly accelerated along the dune upwind face straight up to crest. The separation of the boundary layer then occurs at the crest itself. The naturally inclined downwind face is surrounded by a reversed flow region, whose extent is one of the key parameters describing the flow. Reattachment of the boundary layer occurs far downstream the dune crest, being x_r the so-called reattachment length. The latter quantity is experienced in sharp-edge bluff body aerodynamics to be highly sensitive to a number of setup parameters (e.g. Reynolds number, surface roughness, incoming turbulence). Much more detailed 2D topological mapping of the wake region for isolated transverse dunes under crest-normal flow can be recovered in literature (e.g. Walker and Nickling, 2002, 2003; Delgado-Fernandez et al., 2011).

While the 2D flow structures above have been extensively scrutinized and re-

viewed in [Livingstone et al. \(2007\)](#), very little is known about three-dimensional coherent flow structures in the wake (for an updated review, see [Bauer et al., 2013](#)). On one hand, in the Geomorphology community, such 3D coherent flow structures past nominally 2D dunes are usually ascribed to: i. oblique incoming wind, i.e. where a yaw angle $\alpha_C > 45^\circ$ gives rise to helical vortices in the wake ([Allen, 1970](#); [Walker and Nickling, 2002](#)), and/or ii. small crest irregularities, inducing spanwise flow in the wake, spanwise swirling of the reversed flow, and secondary recirculation zones (see the recent CFD simulations and field measurements in [Jackson et al., 2011, 2013](#); [Delgado-Fernandez et al., 2013](#), , respectively). It is worth pointing out that from an aerodynamic point of view both occurrences involve a 3D setup. On the other hand, to the writers best knowledge, 3D coherent structures in the wake of genuine 2D setups (i.e. ideal transverse dune under normal wind) remain elusive and scarcely studied in literature, if any. Difficulties in both wind tunnel facilities and measurement techniques, and in 3D computational simulations are conjectured by the writers and other authors (e.g. [Walker and Nickling, 2003](#)) to be the cause of such lack of knowledge.

On one side, Wind Tunnel (WT) tests in the aeolian field adopt scaled dune models spanning across the whole test section width (i.e. $S = w$), and with rather low values of the dune aspect ratio (span/chord ratio S/L), e.g. $S/L = 1.28$ in [Walker \(2000\)](#) and [Walker and Nickling \(2003\)](#), $1.92 \leq S/L \leq 10.32$ in [Dong et al. \(2007\)](#); [Qian et al. \(2009\)](#), $S/L = 5.4$ in [Liu et al. \(2011\)](#)). Such values of the aspect ratios:

- are by far lower than the ones adopted in other bluff body aerodynamics problems characterised by separation, reversed flow and reattachment, especially when 3D flow features are expected (see for instance [Bruno et al., 2014](#));
- are suspected to significantly affect the 3D features of the flow in the wake, because of the tips effects due to interaction between the boundary layers surrounding the dune and the WT side walls. For instance, in [Walker and](#)

Nickling (2003, Figure 5a, page 1119) the normalised shear stress profile along the WT midline (i.e. .46 m far from the WT side wall) does not reach nil value in the conjectured reattachment area nor elsewhere in the dune wake.

More generally, difficulties in WT studies are recognised in the proper scaling of different setup lengths, i.e. the ones related to the dune geometry, the surface roughness, the turbulent length scale of the turbulent incoming flow (Walker and Nickling, 2003).

On the other side, the fundamental computational (CFD) studies on the flow field over the transverse dune (e.g. Parsons et al., 2004a,b; Schatz and Herrmann, 2006; Araújo et al., 2013) usually consider simplified 2D condition (see Livingstone et al., 2007, for a review). Only recently, Liu et al. (2011) have compared the simulated flow around a transverse dune obtained in 2D and "2.5D" conditions between them and with WT measurements. The "2.5D" heading indicates that despite the computational domain is 3D, its height and width are equal to half the WT working section dimensions where reference experimental test are performed. In other terms, both left-to-right and bottom-to-top symmetry of the flow are conjectured to reduce the domain size and related computational costs. Under such an assumption, interesting preliminary results are obtained. In particular, 3D flow features of the flow in the near wake of the 2D dune are qualitatively observed (Liu et al., 2011, Figure 8a, page 884). According to the writers, some questions immediately follow. Which aerodynamic phenomena underly and/or trigger the 3D flow features observed in the cited experiments and computational simulations? In particular, do the WT side wall effects play any role in generating such 3D structures? That is, would similar structures having corresponding characteristic lengths obtain if the same dune had, in the limit, an infinitely long span (i.e., an infinite aspect ratio)?

The present study aims at shedding some light on such issues. The sensitivity of the 3D features of the wake to the setup geometrical scaling is studied. In particular, the domain size and the related inlet and side boundary conditions

are the retained parameters of the study. In such a perspective, the present study takes the baton relay from the stimulating study of (Liu et al., 2011) conceived in the Geomorphology community, and develops it according to the knowledge background of Bluff Body Aerodynamics. The adopted computational approach is expected to efficiently complement the wind tunnel studies in exploring a huge number of setup conditions, where a single parameter is varied at the time and border, or even unphysical, conditions can be scrutinized. The experimental setup of Liu et al. (2011) is adopted as the reference one. The obtained computational results are compared with the experimental ones available in literature. Finally, a deeper insight in the 3D emerging coherent flow structures in the wake is provided.

2. Wind flow modelling and computational approach

The incompressible, turbulent, separated, unsteady flow around the dune profile is modeled by the classical Time-dependent Reynolds Averaged Navier-Stokes (T-RANS) equations, which, in Cartesian coordinates, read:

$$\frac{\partial \bar{u}_i}{\partial x_i} = 0 \quad (1)$$

$$\frac{\partial \bar{u}_i}{\partial t} + \bar{u}_j \frac{\partial \bar{u}_i}{\partial x_j} = -\frac{1}{\rho} \frac{\partial \bar{p}}{\partial x_i} + \frac{\partial}{\partial x_j} \left[\nu \left(\frac{\partial \bar{u}_i}{\partial x_j} + \frac{\partial \bar{u}_j}{\partial x_i} \right) \right] - \frac{\partial}{\partial x_j} (\overline{u'_i u'_j}), \quad (2)$$

where \bar{u}_i is the averaged velocity, u' the velocity fluctuating component, \bar{p} the averaged pressure, ρ the air density and ν the air kinematic viscosity. The SST $k - \omega$ turbulence model first proposed by Menter (1994) and further modified in Menter et al. (2003) is used to close the T-RANS equations:

$$\frac{\partial k}{\partial t} + \bar{u}_i \frac{\partial k}{\partial x_i} = \frac{\partial}{\partial x_i} \left[\left(\sigma_k \nu_t + \nu \right) \frac{\partial k}{\partial x_i} \right] + \tilde{P}_k - \beta^* k \omega \quad (3)$$

$$\frac{\partial \omega}{\partial t} + \bar{u}_i \frac{\partial \omega}{\partial x_i} = \frac{\partial}{\partial x_i} \left[\left(\sigma_\omega \nu_t + \nu \right) \frac{\partial \omega}{\partial x_i} \right] + \alpha \frac{\omega}{k} P_k - \beta \omega^2 + (1 - F_1) \frac{2\sigma_\omega}{\omega} \frac{\partial k}{\partial x_i} \frac{\partial \omega}{\partial x_i}, \quad (4)$$

where k is the turbulent kinetic energy, ω its specific dissipation rate and ν_t the so-called turbulent kinematic viscosity. The kinetic energy production term

126 \tilde{P}_k is modeled by introducing a production limiter to prevent the build-up of
 127 turbulence in stagnation regions:

$$\tilde{P}_k = \min(P_k, 10\beta^*k\omega) \quad \text{being} \quad P_k \approx 2\nu_t D_{ij} \frac{\partial \bar{u}_i}{\partial x_j}.$$

128 For sake of conciseness, the definition of the blending function F_1 and the values
 129 of the model constants are omitted herein. Interested readers can find them in
 130 [Menter et al. \(2003\)](#). The SST $k - \omega$ turbulence model is selected for the
 131 current application because of its proven accuracy in bluff body aerodynamics
 132 in general ([Menter et al., 2003](#)) and in dune aerodynamics in particular ([Liu](#)
 133 [et al., 2011](#)).

134 At the ground and dune surfaces the so-called sand-grain roughness wall func-
 135 tions are selected for the current application because of their wide use in environ-
 136 mental CWE in general (e.g. [Blocken et al., 2007a](#)) and the proofs of adequacy
 137 obtained in previous 3D simulations of sand dune aerodynamics by [Liu et al.](#)
 138 [\(2011\)](#); [Jackson et al. \(2011, 2013\)](#). In particular, standard wall functions ([Launder](#)
 139 [and Spalding, 1974](#)) with roughness modification ([Cebeci and Bradshaw,](#)
 140 [1977](#)) are applied. The equivalent sand grain roughness height is determined
 141 as $K_s = 9.793z_0/C_s$, where $C_s = 0.5$ is the roughness constant and z_0 is the
 142 aerodynamic roughness. All the application setups involve $z_0 = 0.1$ mm and
 143 shear velocity $u^* = 0.512$ m/s, both estimated in wind tunnel tests. It follows
 144 $K_s = 1.96$ mm, and non-dimensional roughness height $K_s^+ = K_s u^* / \nu \approx 70$, in
 145 the so-called transitional regime [Blocken et al. \(2007a\)](#).

146 The adopted computational domains and the conditions imposed at their
 147 boundaries are the object of a parametrical study. They are detailed in the
 148 next Section.

149 The OpenFoam©Finite Volume open source code is used in the following to
 150 numerically evaluate the flow-field. The cell-centre values of the variables are
 151 interpolated at face locations using the second-order Central Difference Scheme
 152 for the diffusive terms. The convection terms are discretised by means of the
 153 so-called Limited Linear scheme, a 2nd order accurate bounded Total Varia-
 154 tional Diminishing (TVD) scheme resulting from the application of the Sweby

155 limiter (Sweby, 1984) to the central differencing in order to enforce a mono-
 156 tonicity criterion. The pressure-velocity coupling is achieved by means of the
 157 pressure-implicit PISO algorithm, using a predictor-corrector approach for the
 158 time discretisation of the momentum equation, whilst enforcing the continuity
 159 equation. The space discretization is accomplished by a predominantly struc-
 160 tured grid of hexahedral control volumes. Unstructured patterns locally occur
 161 at the intersection between the surface-fitted grid boundary layer and the carte-
 162 sian grid in the higher part of the domain. The denser grid is located close
 163 to the wind tunnel floor and side walls, and to the dune surface. The grid in
 164 the whole domain and its detail around the dune surface are shown in Figure
 3(a) and (b), respectively. The height of the control volume adjacent to the

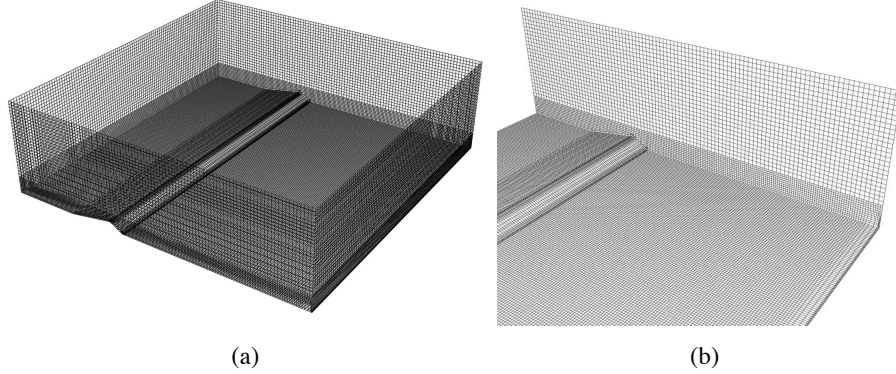


Figure 3: Computational grid in the whole domain (a) and close to the dune (b)

165
 166 wall $n_w = 2n_p$ is driven by the sand-grain roughness wall function requirements
 167 (Blocken et al., 2007b). In particular, n_w should i. provide a sufficiently high
 168 mesh resolution in the normal direction n to the surface, ii. comply with the
 169 standard requirement on dimensionless wall unit $30 < n^+ = n_p u^* / \nu < 100$, and
 170 iii. be longer than twice the sand grain roughness height, $K_s = 1.96$ mm in
 171 the considered setup. The third requirement obeys to the need of avoiding grid
 172 cells with centre points within the physical roughness height. Both the second
 173 and third requirements limit the grid density at wall. In the following, n_w is

174 set equal to $n_w = 0.2h = 5$ mm in order to satisfy at best the above criteria.
 175 The n^+ value along the flat surface far upwind and downwind from the dune
 176 is $n^+ = 80$, while its values along the dune surface vary from $n^+ = 70$ and
 177 $n^+ = 35$ at the dune upwind and downwind toes, respectively, to $n^+ = 110$ at
 178 the dune crest. The ratio $n_p/K_S = 1.28$ is larger but close to unit: hence no
 179 significant further grid refinement at wall can be done within the adopted wall
 180 treatment. The advancement in time is accomplished by the implicit two-step
 181 second order Backward Differentiation Formulae (BDF) method. The adopted
 182 time step is equal to $\Delta t = 0.00025$ [s], i.e. $\Delta t u_{ref}/h = 0.1$ dimensionless time
 183 unit.

184 **3. Application setup**

185 Three setups are adopted and the resulting flow are compared. All of them
 186 adopt a sharp-crested transverse dune, and generally refer to the experimen-
 187 tal setup described by [Liu et al. \(2011\)](#). Besides such main reference, critical
 188 comparison is also made to other measurements provided in [Dong et al. \(2007\)](#);
 189 [Qian et al. \(2009\)](#); [Walker and Nickling \(2003\)](#), the former two being obtained
 190 for several incoming speeds, the latter in slightly different experimental condi-
 191 tions. Table 1 summarizes the main features of the cited experimental setups,
 192 where z_0 is the dune and floor aerodynamic roughness and u_{ref} is the incom-
 193 ing reference speed. It follows that the reference Reynolds number is equal to
 194 $Re_h = u_{ref}h/\nu = 1.7e + 4$.

195 The setups differ in both the size of the analytical domain in space and in the
 196 corresponding applied boundary conditions (b.c.). The domain size and the
 197 kind of b.c. adopted in the setups are depicted in Figure 4, while the profiles of
 198 the incoming wind (mean velocity u_x , turbulence intensity It and length scale
 199 Lt) are plotted in Figure 5. The setups are briefly commented in the following:

- 200 **s1** only 1/4 of the wind tunnel working section volume is retained. Symmetry
 201 conditions are imposed on the vertical plane because of the conjectured
 202 symmetry of the flow. Free stream b.c.s are set on the upper horizontal

Table 1: Experimental setups

Authors	h [mm]	α_u [deg]	α_d [deg]	L/h [-]	S/L [-]	u_{ref} [m/s]	z_0 [mm]
Liu et al. (2011)						10	
Dong et al. (2007)	25	10	30	7.4	5.40	8,10,12,14	0.1
Qian et al. (2009)						8,10,12,14	
Walker and Nickling (2003)	80	8	30	9.0	1.28	8,13,18	n.a.

plane to disregard the influence of the WT upper wall. The incoming mean wind velocity and turbulence intensity profiles are fitted on the WT measurements ([Liu et al., 2011](#), estimated shear velocity $u^* = 0.512$ m/s), while turbulence length scale is conjectured constant and equal to $Lt = 5$ mm because of the lack of experimental data (Figure 5). The spatial grid involves about $4.e + 5$ control volumes. This setup is often retained in CFD practice to reduce the number of grid volumes and related computational costs when the WT conditions are to be emulated (e.g. in [Liu et al., 2011](#)). The setup is intended to discuss the accuracy of such an approach;

s2 the setup exactly reproduces the size of the WT working section in [Dong et al. \(2007\)](#); [Qian et al. \(2009\)](#); [Liu et al. \(2011\)](#). No-slip b.c.s are set at the four alongwind boundary planes to model the WT walls. A complementary simulation (s2-a, Figure 4) is preliminary performed along an empty channel to replicate the WT approaching section described in [Liu et al. \(2011\)](#). Periodic conditions at the inlet and outlet of s2-a are set to obtain a fully self-developed, horizontally homogeneous incoming boundary layer flow ([Blocken et al., 2007b](#)). The resulting u_x , It and Lt profiles are then imposed at the inlet of the main domain (Figure 5). The spatial grid in s2-b involves about $1.5e + 6$ control volumes. The setup aims

at removing the ansatz introduced in s1 in order to suggest best practice guidelines in CFD simulations of WT tests;

s3 The side walls of the WT working section are replaced by spanwise periodic conditions. Two domain spanwise lengths are considered: $w_{3a} = w_2$ is set in setup s3a, and $w_{3a} = 4w_2$ in setup s3b. The height of the domain is set equal to $12h$, i.e. larger than the range suggested in [Franke et al. \(2007\)](#) $4h < h_{WT} < 10h$ for external flows in Wind Engineering. The spatial grid in s3b involves about $2.7e + 6$ control volumes. The setup aims at comparing the results to the ones obtained in the s2 setup and at evaluating 3D flow features, if any, under 2D, "external" incoming flow conditions. The profiles of the incoming turbulent length scale and turbulence intensity are set in accordance to [Richards and Norris \(2011\)](#) to replicate an external flow.

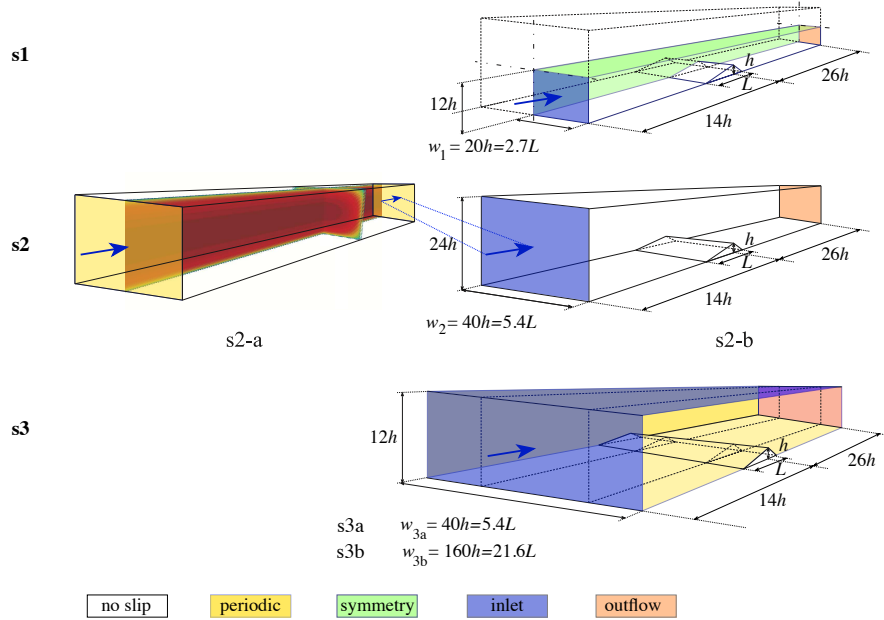


Figure 4: Scheme of the adopted setup conditions (not in scale) including b.c. (wind from left to right)

236 In all setups, Neumann conditions ("outflow" in Figure 4) involving the velocity
 237 field and the pressure (null normal component of the stress tensor) as well as k
 238 and ω are imposed at the outlet boundary. No-slip conditions are imposed at the
 floor surface and at the WT walls, if any. Uniform initial conditions are imposed

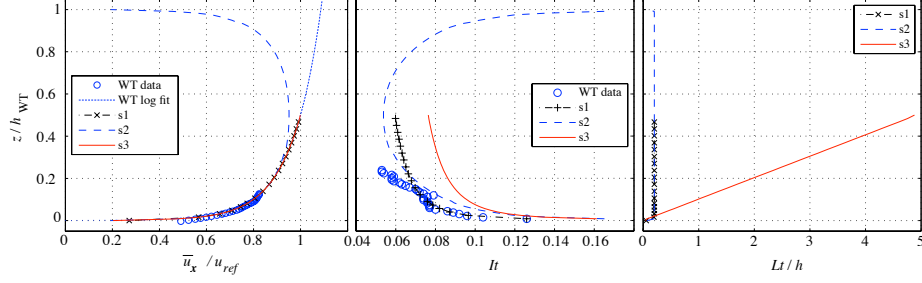


Figure 5: Vertical profiles of the inlet boundary conditions

239
 240 at the beginning of the time-dependent simulations. The simulated time for each
 241 setup is equal to about $Tu_{ref}/h = 4000$ dimensionless time units, long enough
 242 to guarantee the convergence of the first and second statistical moments in time
 243 for all the flow variable, following the convergence check proposed by Bruno
 244 et al. (2010). The simulations have been performed thanks to the Optiflow
 245 pc cluster (32 nodes with 4 cores each, 4 Gb RAM per node, Intel Nehalem
 246 2.8 GHz clock, 1.4 Tflops). An overall cpu time of about 25 hours on 63 cores
 247 results for the complete parametrical study.

248 4. Results

249 4.1. Setup effects on the overall flow regime

250 In this section, the time dependent behavior of the simulated flow in the
 251 three setups is discussed with reference to both bulk and local quantities. The
 252 former is defined as the aerodynamic coefficient $C_D(t)$ of drag force per span-
 253 wise unit length that results from integration of the stress field on the dune
 254 downwind face, Figure 6(a). The Power Spectral Density of the drag coefficient
 255 is plotted versus the dimensionless frequency $f^* = fh/u_{ref}$ in Figure 6(b).

The PSDs in both s1 and s2 setups clearly show a well defined peak at about

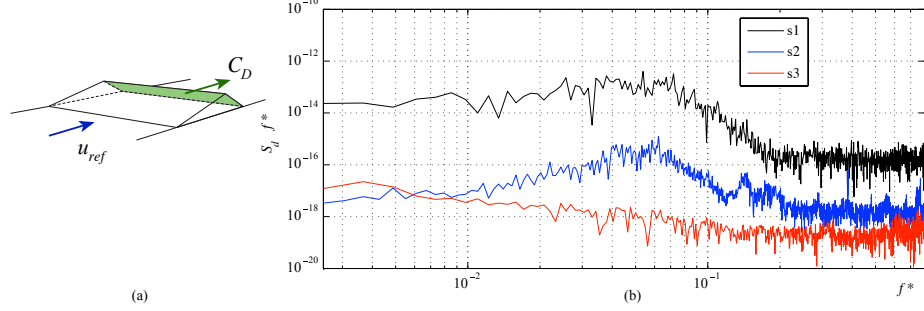


Figure 6: Time dependent flow: PSD of the drag coefficient

256

257 $f^* \approx 0.05 = St$, that conversely disappears in s3a and s3b setups (both notated
 258 "s3" in the following, if not specified otherwise, for the sake of simplicity). At
 259 such Strouhal number St the power density in setup s1 is one order of magni-
 260 tude higher than the one in s2, that is in turn by far greater than in s3. The
 261 high frequency fluctuations ($f^* > 3e - 1$) are due to spurious numerical oscil-
 262 lations of the solution. In summary, the drag force resulting from s3 is almost
 263 steady ($std(C_D) \approx 5.6e - 7$), while very weak to moderate time fluctuations in
 264 the remaining setups ($std(C_D) \approx 7.3e - 5$ and $std(C_D) \approx 1.e - 3$ in s2 and
 s1, respectively) suggest a localized unsteadiness of the flow. To prove such

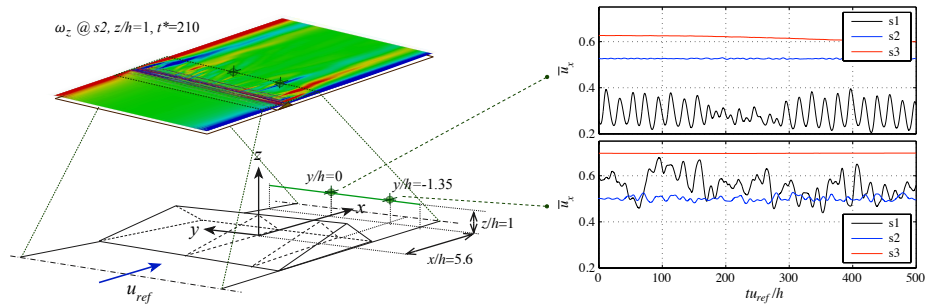


Figure 7: Time dependent flow: spanwise position of the time dependent phenomena

265

266 conjecture, the time history of the longitudinal component of the velocity u_x

is plotted for the three setups and at two probes in the wake (Figure 7). In s1 and s2, the closer the probe to the WT side wall, the larger the velocity fluctuations, while in s3 the flow in the wake is almost steady everywhere. An instantaneous field of the z -vorticity on the plane $z/h = 1$ for s2 is provided in the same Figure to shed some light on the underlying fluid flow phenomenon. In fact, the interaction between the separated boundary layer at the dune crest and the attached one along the WT sidewall induces a 3D flapping along the latter.

As previously introduced, the reattachment length x_r is one of the most relevant quantities in transverse dune aerodynamics. In the adopted computational approach, the reattachment point is evaluated as the one in which the longitudinal component τ_x of the shear stress change sign downwind the dune downwind toe. Heaving in mind the weak variability in time of the overall flow, the time averaged reattachment point ($t - avg(x_r)$) is evaluated, while its spanwise trend is described by the reattachment line, i.e. $t - avg(x_r(y))$. The latter ones obtained in the three setups are plotted in Figure 8.

The following remarks follow:

- very significant WT wall effects take place close to the dune tips in both s1 and s2 setups. In particular:
 - in s1 such effects propagate along all the dune span, so that a meaningful estimate of the reattachment length can be obtained by spanwise averaging nor by adopting a point wise value, e.g. at the mid plane;
 - in s2 the spanwise variability due to the WT side wall is limited to a distance from the wall of about $d \approx 1.5L$, clearly related to the unsteady plumes pointed out in Figure 7. A central segment with nearly constant x_r can be recognized: at the vertical mid plan ($y = 0$) $x_r \approx 6.35h$, pretty close to the value measured by [Dong et al. \(2007\)](#) ($x_r \approx 6h$) in the same setup conditions;
- unexpectedly, a quasi-periodic, "festoon-shaped" spanwise reattachment

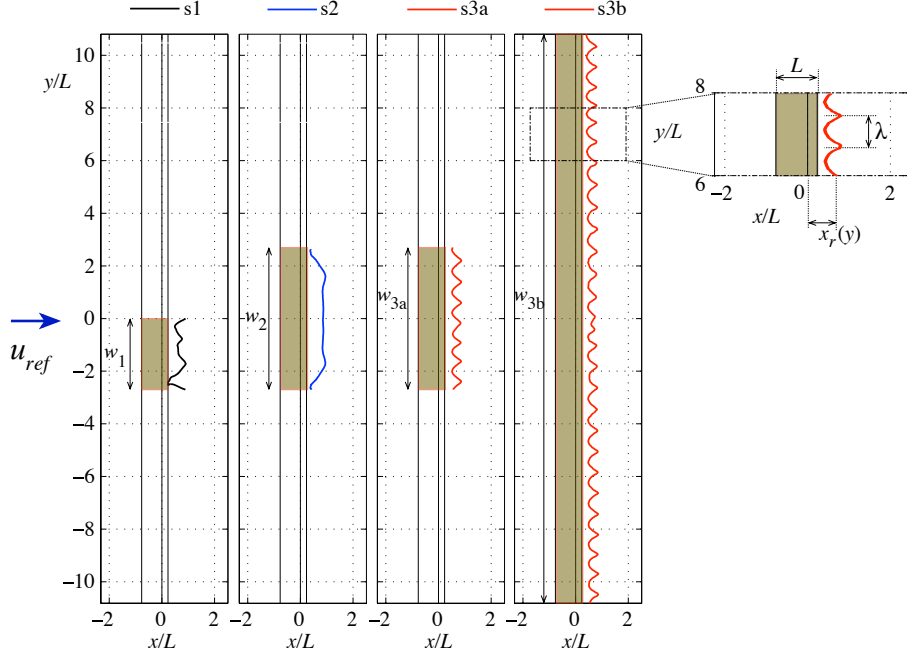


Figure 8: Spanwise dependent flow: variation of the reattachment line

line emerges from both simulations s3a and s3b. Such a trend allows to estimate some spanwise statistics.

- The first two statistical moments of the reattachment length, i.e. its mean value $y - avg(t - avg(x_r))$ and standard deviation $y - std(t - avg(x_r))$, are:

s3a $y - avg(t - avg(x_r)) = 5.04h$, $y - std(t - avg(x_r)) = 0.82h$;

s3b $y - avg(t - avg(x_r)) = 4.64h$, $y - std(t - avg(x_r)) = 0.88h$.

It is worth pointing out that in both simulations the mean value $y - avg(t - avg(x_r))$ is significantly lower than the one obtained at the mid-plan in s2.

- Let us define a characteristic spanwise length (or wavelength) λ of the reattachment line (see closeup view in Figure 8). Its spanwise statistics are:

s3a $y - avg(t - avg(\lambda)) = 5.61h$, $y - std(t - avg(\lambda)) = 0.43h$;

s3b $y - avg(t - avg(\lambda)) = 5.75h$, $y - std(t - avg(\lambda)) = 0.36h$.

The value of the standard deviation $y - std(t - avg(\lambda))$ is small in both simulations, that is the festoon shape is quite stable spanwise.

- Finally it is worth pointing out that the spanwise dimension w_{3a} in setup s3a accommodates 7 wavelengths (including the two halves at the domain side), while the one $w_{s3b} = 4w_{s3a}$ in setup s3b accommodates 27 waves plus an oscillation at midspan, i.e. at the far section from the lateral periodic b.c.s.

In summary, the findings obtained in the Section prove significant effects of the WT side walls (s1 and s2) on the overall flow regime, and suggest that they inhibit the triggering of an almost periodic spanwise variability of the flow in the wake, as observed in external flow conditions (s3).

4.2. Comparison between WT measurements and CWE results

In this Section, comparisons between time-averaged WT measurements at the dune midspan ($y/L = 0$) and the present computational results obtained in the different setups are provided. Bearing in mind the quasi-periodic spanwise reattachment line in s3 (Fig. 8), also spanwise statistics are evaluated for such setup. The z -wise profiles of the longitudinal component of the velocity u_x have been measured in WT tests by Liu et al. (2011) using PIV at different positions in the the vertical mid plan ($y = 0$) of the WT working section. These profiles are compared to the computational ones in Figure 9. The scatter with the WT data around the upwind face (Figure 9, lines a-b) are probably due, according to Liu et al. (2011), to the limitation of the PIV system, which cannot fully resolve the high-speed gradient in the near-surface zone and leads to nonzero wind speed at the surface. The agreement in the reversed flow region (Figure 9, lines e-f) is excellent for setup s2, that replicates the WT conditions. The computational results from setup s1 strongly overestimate the speed deficit in the near wake, while the $y - avg(t - avg(\bar{u}_x))$ in s3 is quite different form the

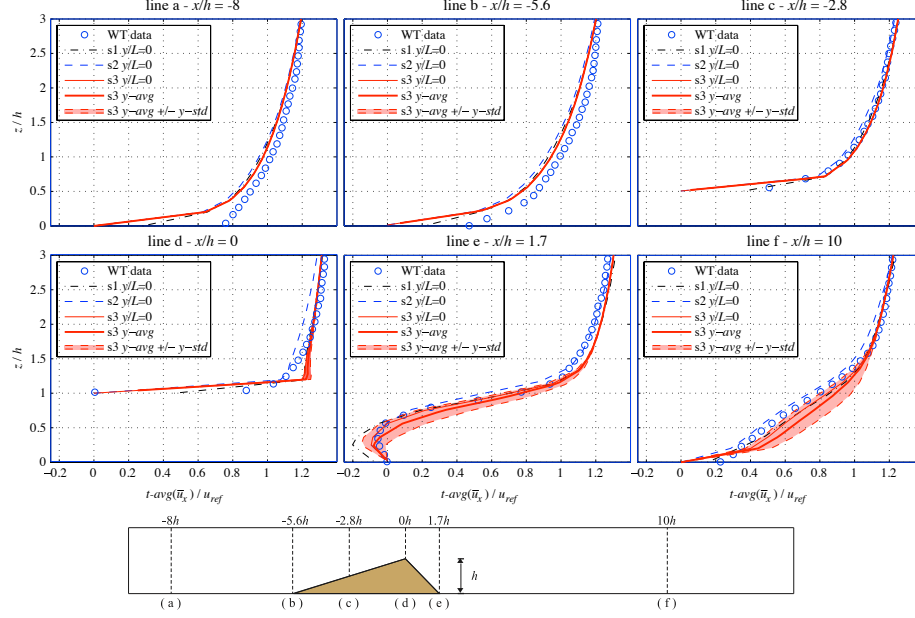


Figure 9: Horizontal velocity profiles: WT measurements (Liu et al., 2011) and present CWE results

centre plane one and from WT data. In the same setup, a significant spanwise deviation occurs in the wake (Figure 9, lines e-f).

The measured x -wise profiles of the vertical component of the velocity u_y at the level $z \approx h$ are reported in Qian et al. (2009). PIV technique has been adopted on the WT vertical mid plan ($y = 0$, i.e. at a distance from the side wall $d/L = 2.7$) at different reference velocities of the incoming wind. The u_y profiles obtained in the three computational setups are compared among them in Figure 10(a), while the profiles measured at midspan are compared in Figure 10(b) to the computational ones at different distance from the side wall in setup s2. Considerable differences between s1 and s2 can be observed in the far wake only, while a dramatic change in the vertical component of the velocity occurs in s3 especially in the near wake. At the dune downwind face ($0 < x/h < 1.7h$), u_y changes its sign from positive (upward flow, s1 and s2) to negative (downward flow, s3). In other terms, the 2D clockwise recirculating region which character-

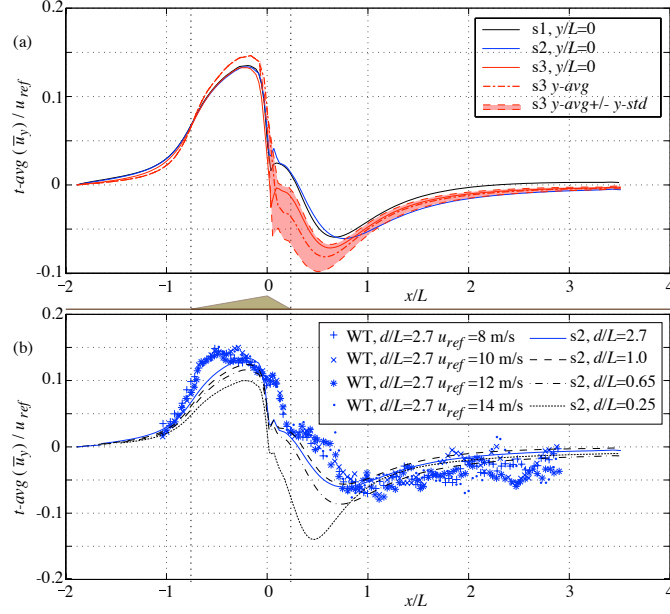


Figure 10: Vertical velocity profiles: WT measurements (Qian et al., 2009) and present CWE results

izes the near wake topology in s2 at mid line no longer holds and it is suspected to change in a 3D local flow (see the large spanwise standard deviation of u_y). A satisfactory agreement is observed between WT and computational approaches, if the same setup and distance from the side wall is adopted (blue points and continuous line in Fig. 10-b). Conversely, the closer the vertical plan to the side wall, the smaller the upward speed at the upwind face and the higher the downward speed at the downwind surface.

An analogous post processing is proposed for the x -wise profiles of the shear stress magnitude $|\tau|$ at the floor in Figure 11. The shear stress is a quantity of particular interest in windblown sand dynamics because above a given threshold value τ_t it induces the sand grain saltation, i.e. the sand bed erosion. Conversely, at $|\tau| < \tau_t$ sedimentation of the flying grains occurs (Bagnold, 1941). For such reason, the $|\tau|/\tau_t$ obtained by computations in the three setups is plotted in Figure 11(a). s1 fails in predicting the sedimentation just downwind the crest

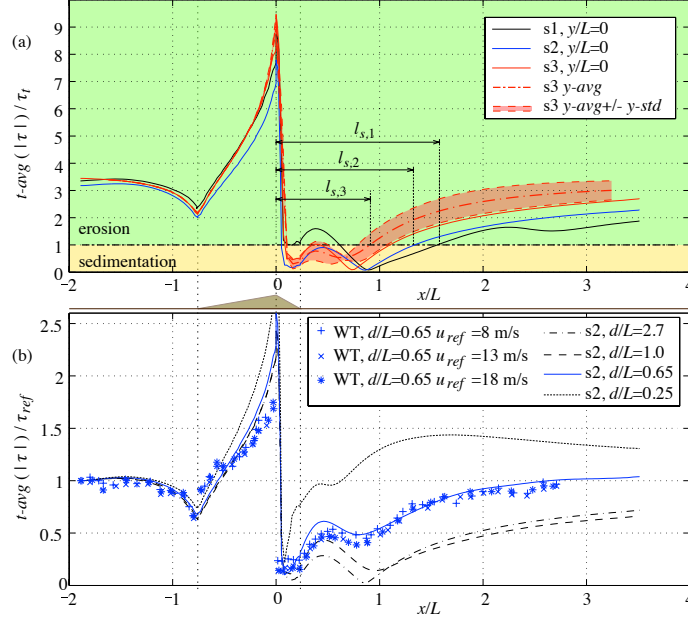


Figure 11: Shear stress profiles: Wind Tunnel measurements (Walker and Nickling, 2003) and present CWE results

and the downwind toe. The lower the blockage ratio, the shorter the sedimentation length l_s , i.e. the closer to the dune the point from which erosion takes place again. Once more, the spanwise variability of the profile along the wake is significant in s3, and the sedimentation length varies from about $0.75L$ to $1.1L$. Figure 11(b) compares the shear stress magnitude profiles obtained in s2 with the one measured by Walker and Nickling (2003) in their WT test by using Irwin-type differential pressure sensors. It is worth pointing out that in this case the experimental setup differs from the computational one in the dune cross section, in the dune aspect ratio, and in the Reynolds number (see Table 1). On one hand, the smaller angle of the upwind face α_u in WT test induces the lower shear stress magnitude along it. On the other hand, the $|\tau|$ profile downwind the crest is mainly affected by the dune aspect ratio, i.e. by the distance d of the measurement alignment from the WT side wall. In fact, a very good agreement is obtained when the measurements at the WT mid plan

381 (i.e. $d = 0.5S/L \approx 0.65$) are compared to the computational profile at the same
382 distance from the side wall. The closer the alignment to the side wall, the higher
383 $|\tau|$ along the wake. In other terms, in this case study the WT wall side effects
384 are by far larger than the ones induced by L/h and/or u_{ref} , even if much more
385 emphasis is traditionally given to the latter than to the former.

386 4.3. 3D Coherent Flow Structures

387 This final Section aims at providing a sound phenomenological reading of the
388 spanwise variability in simulated in external flow conditions (setup s3). A deeper
389 insight in the flow characteristics is then performed, thanks to the amount of in-
390 formation available from computational simulations. Advanced post-processing
391 and flow visualization techniques are employed to this aim. In particular, the
392 velocity and shear stress vector fields are visualized on selected planes by us-
393 ing the so-called Line Integral Convolution (LIC, Cabral and Leedom, 1993;
394 Stalling and Hege, 1995; Laramée et al., 2003). Some information are provided
395 herein, being a technique scarcely used in the Wind Engineering field.

396 LIC is based upon locally filtering an input texture along a curved stream line
397 segment in a vector field and it is able to depict directional information at high
398 spatial resolutions. The directional structure of a vector field can be graphically
399 depicted by its stream lines, i.e. paths whose tangent vectors coincide with
400 the vector field. Given a pixel \mathbf{x}_0 of the desired resulting image and numeri-
401 cally computed a streamline σ , passing by $\mathbf{x}_0 = \sigma(s_0)$, line integral convolution
402 consists in calculating the intensity for that pixel as

$$I(\mathbf{x}_0) = \int_{s_0-L}^{s_0+L} k(s-s_0)T(\sigma(s))ds, \quad (5)$$

403 where s is the arc-length coordinate, T is an input texture, $2L$ is the filter length
404 and k is a filter kernel normalized to unity. In LIC visualizations of fluid flows,
405 a white noise or similar random image is chosen as input texture T . The con-
406 volution causes pixel intensities to be highly correlated along individual stream
407 lines, but independent in directions perpendicular to them. In the resulting
408 images the directional structure of the vector field is clearly visible.

Figure 12(a) and (b) show the LIC visualization of the time-averaged velocity field on an ideal inclined plane ($\beta = 12^\circ$) crossing the near wake from the dune crest, and the LIC visualization of the time-averaged shear stress field on the dune downwind face and wake floor, respectively. In both figures, the direction of the field is highlighted by superimposed arrowed lines. The most striking

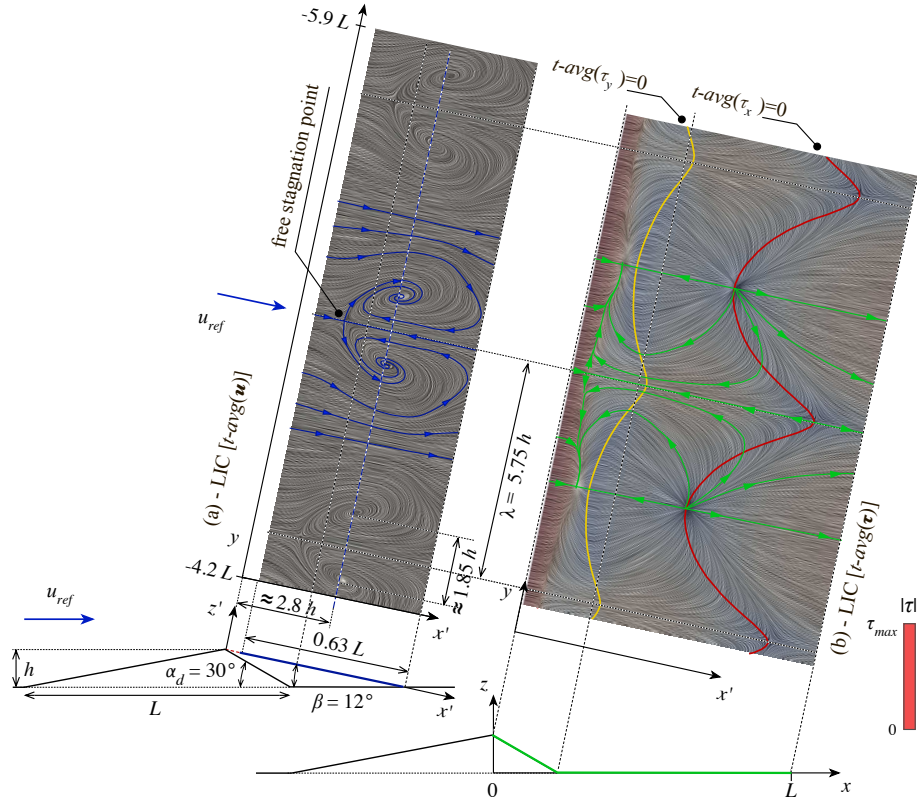


Figure 12: Spanwise 3D coherent structures in the dune wake: time averaged velocity field (a), time averaged shear stress field colored by the its modulus (b)

result is that in Figure 12(a), where the LIC of the time-averaged velocity field highlights quasi-steady, "mushroom"-like coherent flow structures having a pair of owl eyes each. These structures consists of two counterrotating foci with a free stagnation point downwind the crest and between the foci. The main dimensions of such structures are given in the figure. The corresponding LIC of

419 time-averaged shear stress field (Fig. 12-b) is even more complicated and char-
 420 acterized by a "skein"-like pattern. The pattern shape appears to be strongly
 421 related with the mushroom-like structure, especially at the ground floor (i.e.
 422 where the mushroom is closest to the floor). In order to shed some more light
 423 in such a pattern, it is colored by the modulus of the same shear stress, and
 424 the spanwise lines along which $\tau_y = 0$ and $\tau_x = 0$ (reattachment line, see also
 425 Fig. 8) are superimposed. For both lines a geometrical reading with respect to
 426 the LIC pattern can be provided: the former is the locus of points where the
 427 tangent to the streamlines are aligned with the x -axis, while the latter is the
 428 locus of points where the tangent to the streamlines are aligned with the y -axis.
 429 The mushroom spanwise characteristic length is equal to the wavelength λ of
 430 the "festoon" reattachment line. In particular, the spanwise maximum reat-
 431 tachment length correspond to the mushroom center, while the minimum value
 432 takes place in between two consecutive mushrooms.
 433 To the authors' best knowledge, analogous spanwise coherent flow structures
 434 have been previously recognized at least in two studies involving nominally 2D
 435 setups.
 436 Similar spanwise mushroom-shaped flow structures have been visualized by
 437 Schewe (2001) around an apparently different aerodynamic setup, i.e. the sep-
 438 arated flow around an airfoil at incidence in the critical regime. In fact, in
 439 his pioneering and seminal work Schewe has observed and described in detail
 440 mushroom-like flow structures (Figure 13), combined in different arrangements
 441 for different values of the airfoil aspect ratio S/L ($L = w$), and bounded by dis-
 442 turbed regions close to the end plates. On the basis of the experimental results,
 443 Schewe conjectures that: i. the occurrence and number of the mushroom-like
 444 structures depend on the inclination of the base upper surface; ii. the spanwise
 445 flow structure remains intact as $S/L \rightarrow \infty$; iii. the wavelength λ scales with the
 446 sectional dimension(s) of the airfoil; iv. preferential or more natural spanwise
 447 arrangements exist, in terms of number of cells and their wavelength. These
 448 speculations seem to hold, to a certain extent, also in the present case study.
 449 In fact: i. the downwind face of the dune and the base upper surface of the

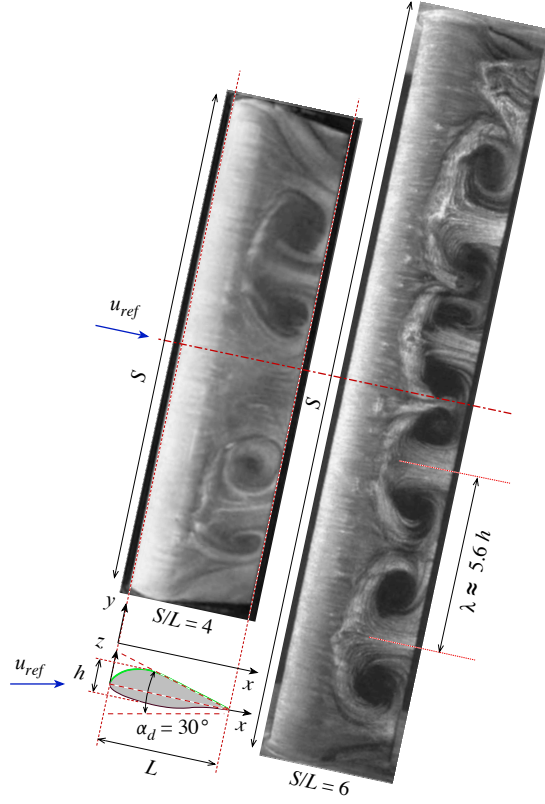


Figure 13: Oil-flow pictures of the mushroom-like flow structures at the upper surface of an airfoil, after [Schewe \(2001\)](#)

450 airfoil share the same inclination with respect to the incoming wind ($\alpha_d \approx 30^\circ$);
 451 ii. setup s3 confirms that the coherent flow structure is qualitatively unchanged
 452 by passing from s3a to s3b, where the latter mimics an infinite aspect ratio of
 453 the dune because of the periodic side b.c. and the increased spanwise length;
 454 iii. the characteristic length λ of the mushrooms found by [Schewe \(2001\)](#) is
 455 comparable to the one in s3, if both are scaled versus h ($\lambda \approx 5.75h$, Fig. 12-a,
 456 $\lambda \approx 5.6h$, Fig. 13); iv. in both Schewe and present setups, stable arrangements
 457 are characterized by a given number of spanwise aligned mushrooms. In Schewe,
 458 an even number of vortices is always observed, but the end-plate disturbances
 459 considerably extend spanwise; conversely, in s3 an odd number of mushrooms

emerges in both s3a (7) and s3b (27) setups (see Fig. 8), despite the spanwise
 length in s3b is four time the one in s3a. It is worth pointing out that the
 quasi-periodic mushroom structure is corrupted at midspan, if the dune length
 $S = w$ is not an odd multiple of λ (s3b). Despite the analogies above, it is
 worth pointing out that the flow structures in Schewe (2001) are recognized only
 in the critical regime, while the occurrence of the same condition is unlikely in
 the present case study.

More recently, analogous 3D, global, quasi-steady vortices have been simulated
 by Spalart et al. (2014) in an even more different fluid flow setup, i.e. the nom-
 inally 2D, high Reynolds number, fully developed turbulent Couette flow. The
 RANS-based simulations of Spalart et al. (2014) (including the SST $k - \omega$ one),
 successfully reproduce the same flow structures previously observed and sim-
 ulated in experiments and DNS, respectively. In the present perspective, it is
 worth pointing out that: i. the vortices are arranged in a quasi-periodic z-wise
 system of counter-rotating pairs (Fig. 1, Spalart et al. (2014)), analogously to
 the arrangement in Figure 12(a) ; ii. the distribution of the skin-friction coef-
 ficient in the z direction (Fig. 6, Spalart et al. (2014)) qualitatively matches
 the "festoon-shaped" spanwise reattachment line in Figure 8; iii. the simulated
 flow structures hold in a wide range of Reynolds numbers, and the effect of the
 vortices is only weakly dependent on Re. In their outlook, Spalart et al remark
 that there is a convincing scale separation between the simulated flow structures
 and the turbulence which is represented by the RANS model. The vortices have
 a lateral scale much smaller than the scale of the geometry (which is infinite in
 the setup), and random locations in z , giving them the nature of an instability.
 The remarks above qualitatively hold also in the present case study. Despite
 such analogies, it is worth pointing out that the flow structures in Spalart et al.
 (2014) are somewhat triggered by an initial velocity field mimicking a periodic
 system of counter-rotating vortex pairs in the $(y - z)$ plane, while in the present
 case study the mushroom-like structures spontaneously develop from uniform
 initial conditions.

491 5. Conclusions

492 The present study points out some emerging 3D coherent flow structures
493 in the wake of a transverse dune under different setup conditions by means of
494 computational simulations and compares the obtained results with a number of
495 experimental wind tunnel measurements available in literature. The comparison
496 shows a good and robust agreement of the CWE results to WT data, and it goes
497 beyond: it puts in evidence common misunderstandings in setting up computa-
498 tional and experimental models for CWE/WT validation. Some good practices
499 in dune aerodynamics CWE simulations and WT tests are recommended: i.
500 CWE-WT comparisons require the careful simulation of the WT setup, includ-
501 ing the wind tunnel geometry; ii. forcing the flow symmetry by b.c. in CWE
502 can strongly affect the results; iii. high values aspect ratio are recommended in
503 WT test to replicate external flow conditions, e.g. $w/L \gg 10$.
504 Surprisingly, emerging mushroom-like, coherent flow structures in the dune wake
505 are clearly shown by a deep analysis of the CWE results. They are compared
506 to analogous flow structures arising from rather different aerodynamic setups
507 belonging to referential literature in fluid dynamics. It follows that the studied
508 setup can be ascribed to a wider class of 3D flows occurring under 2D nominal
509 conditions. According to the authors such class of flow seems to be of high
510 relevance in modern developments of fluid dynamics, and it still remain poorly
511 understood in its general features, if any. The authors hope further indepen-
512 dent studies will appear and further develop their contribution. In particular,
513 the precise definition of the aerodynamic regime(s) at which mushrooms grow in
514 the dune near wake remain an open issue. An even wider computational study
515 would be required to discuss the permanence and/or changes of such coherent
516 flow structures from the model scale to the full scale, e.g. by varying Reynolds
517 number and/or surface roughness.

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